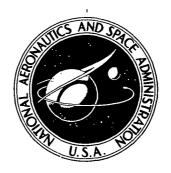
# NASA TECHNICAL MEMORANDUM



**NASA TM X-2998** 

CASE FILE

USER'S GUIDE FOR ANALYSIS
OF FINITE ELASTOPLASTIC
DEFORMATION: THE FIPDEF AND
FIPAX PROGRAMS FOR THE CDC 6600

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1. Report No. NASA TM X-2998	2. Government Accessi	on No.	3. Recipient's Catalog	No.
4. Title and Subtitle USER'S GUIDE FO	FINITE	5. Report Date		
ELASTOPLASTIC DEFORMAT			June 1974	
PROGRAMS FOR THE CDC 666			6. Performing Organiz	ation Code
7. Author(s)			8. Performing Organiz	ation Report No.
Jon R. Osias			E-7610	
			10. Work Unit No.	
9. Performing Organization Name and Address		ļ	501-21	
Lewis Research Center	A 1		11. Contract or Grant	No.
National Aeronautics and Space	Administration			
Cleveland, Ohio 44135			13. Type of Report an	d Period Covered
12. Sponsoring Agency Name and Address			Technical Me	emorandum
National Aeronautics and Space	Administration		14. Sponsoring Agency	Code
Washington, D.C. 20546				
15. Supplementary Notes	<u> </u>			
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16. Abstract				:144 f
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work hardening exceed some small positive value. The user's guide assumes familiarity with				
both finite-element analysis and FORTRAN IV programming for the CDC 6600. Sufficient infor-				
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17. Key Words (Suggested by Author(s))		18. Distribution Statement		
Finite deformation	OC 6600	Unclassified - ı	ınlimited	
Finite deformation of CDC 6600 Unclassified - unlimited  Plasticity  The last of the first of the content of th				
Elastoplastic flow	₹c *			
Finite elements			CAT	. 32
19. Security Classif. (of this report)	20. Security Classif. (or	f this page)	21. No. of Pages	22. Price*
Unclassified	1	assified	74	\$3.75

# USER'S GUIDE FOR ANALYSIS OF FINITE ELASTOPLASTIC DEFORMATION: THE FIPDEF AND FIPAX PROGRAMS FOR THE CDC 6600

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#### Lewis Research Center

#### SUMMARY

The FIPDEF and FIPAX programs provide analysis capability for problems of two-dimensional finite deformation of elastoplastic bodies. Applications are restricted to problems amenable to analysis in two spatial dimensions. Both programs, FIPDEF for problems of plane strain and plane stress, and FIPAX for axisymmetric cases, allow treatment of monotonic and cyclic loading of isotropic materials which exhibit no Bauschinger effect. Elastic unloading, as, for example, in tensile necking, is automatically treated. No restriction is placed upon deformation magnitude other than the availability of material property data. Stress - plastic strain data points are used directly, providing a piece-wise linear relation, thereby eliminating any need for curve fitting of experimental property data. The input data points must reflect a strictly positive rate of hardening.

The problem of finite elastoplastic deformation has been posed as a quasi-linear initial- and boundary-value problem (refs. 1 and 2). The subject programs perform requisite integrations of the governing equations over space and time. The analyses presume the existence of a stress-free reference configuration and require that it be modeled by an array of triangular finite elements. The initial geometry may include sharp notches. Complete problem definition requires specification of material property information, elastic constants and stress-strain data, and an incremental boundary condition history involving boundary loads and/or displacements.

The user's guide is intended to support problem solving utilization of the programs. Matters of theoretical formulation and numerical procedure are documented in references 1 to 3 and are not detailed here. Specification of problem input and output as well as sample problem input and output are provided. Summary information on program structure and auxiliary storage requirements is presented. The user is presumed to be familiar with the operational aspects of finite-element analysis as well as FORTRAN IV programming for the CDC 6600.

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#### INTRODUCTION

The FIPDEF (<u>finite planar plastic deformation</u>) and FIPAX (<u>finite plastic axisymmetric deformation</u>) computer programs perform incremental finite-element analysis of problems of elastoplastic deformation which admit modeling in two spatial dimensions. The deformation may be viewed as either infinitesimal or finite; that is, according to user specification, the analysis considers the undeformed and deformed configurations of a body to be either indistinguishable or distinct.

Should the deformation be considered finite, the numerical analysis is based on objective, complete forms of the incremental equilibrium and elastoplastic constitutive equations. Consequently the analysis is valid irrespective of deformation magnitude. This feature provides the principal distinction between the capabilities of the subject finite-element programs and other available formulations employing, for example, simple ''updating'' of nodel coordinates or ''large'' displacement - ''small'' strain kinematics appropriate to limited classes of plate and shell problems. The present analyses are considered appropriate for two-dimensional treatment of the finite deformation of bodies of arbitrary shape including those containing sharp notches.

The theoretical formulation and numerical procedures employed are detailed in references 1 to 3 and will not be reiterated here. It is appropriate, however, to review several aspects of the general finite-deformation formulation which have a direct bearing on definition and solution of particular problems.

The problem of finite elastoplastic deformation is posed in the form of an initialand boundary-value problem whose spatial domain is at all times the current configuration of a deforming solid. The adoption of this Eulerian viewpoint produces a quasilinear problem whose solution requires a sequence of spatial integrations of the instantaneously linear governing equations. Consecutive spatial integrations, accomplished
by finite-element solution, are coupled by the integration of the dependent variables over
a small increment of time. Thus, to the user, the numerical analysis appears as an incremental process producing the entire history of deformation, boundary loading, and
internal stress and strain fields. In the limit of infinitesimal deformation, the formulation and numerical implementation reduce to a conventional incremental finite-element
analysis of infinitesimal elastoplastic deformation.

The piecewise linear nature of the numerical analysis allows the solution of finite-deformation problems at no greater computational expense than is required for analysis of infinitesimal elastoplastic deformation. Furthermore, this feature allows efficient automatic treatment of elastic unloading and cyclic plasticity.

Problem definition requires specification of a finite-element map corresponding to the undeformed, stress-free state; material properties, elastic constants and equivalent stress - plastic-strain data; and an incremental boundary condition history involving boundary components of displacement, load, or admissible combinations thereof. As deformation proceeds the finite-element map deforms providing a material reference frame for tracking stress and strain field components within the Eulerian framework of the analysis. Consequently incremental boundary condition specifications must reflect conditions applied to the deformed state at each increment.

Principal features of both programs include:

- (a) User specification of either infinitesimal or finite deformation analysis
- (b) Choice of either isotropic elastic or work-hardening elastoplastic material behavior
- (c) Data point specification of the equivalent stress plastic strain relation
- (d) Automatic treatment of elastic unloading and cyclic plasticity
- (e) Program control of incremental loading history in accordance with user specification of maximum allowable incremental stress magnitude
- (f) Problem interruption and restart capability.

Additional options for both programs are defined in the input data tables of the sections dealing with the individual programs.

This user guide is divided into four sections dealing with details of program usage, including problem definition, specifics of utilization for each of the programs, and sample problem input and output. The program sections include information on input data, output data, program structure, and array dimensioning.

Before proceeding the user must be cautioned in several respects. These programs have been extensively verified and evaluated only for a limited class of displacement bounded problems of particular interest to the developer (see, e.g., refs. 1 and 2). The user is encouraged to undertake his own verification for those types of problem he intends to consider. It is assumed that the user is familiar with the operational aspects of finite-element analysis (ref. 4), FORTRAN IV programming, and the CDC SCOPE operating environment.

#### **SYMBOLS**

$$\begin{array}{ll} d_{ef}^p & \text{effective plastic strain rate,}^1 \equiv \left[ (2/3) d_{ij}^p d_{ij}^p \right]^{1/2} \\ \\ d_{ij} & \text{deformation rate,} \equiv (1/2) \left( \partial v_i / \partial x^j + \partial v_j / \partial x^i \right) \\ \\ E & \text{Young's modulus (linear elastic)} \\ \\ F_i^N & i^{th} & \text{component of load vector at node } N \\ \\ f_i & i^{th} & \text{component of lineal boundary loading density} \end{array}$$

<sup>&</sup>lt;sup>1</sup>Repeated index implies summation over i, j = 1, 2, 3.

$J_{i}$	i <sup>th</sup> component of J integral
$\theta_2$	second invariant of deviatoric stress, $= (1/2) S_{ij} S_{ij}$
K	bulk modulus (linear elastic)
<b>l</b> .	deformed tensile test specimen gage length
l <sub>o</sub> ···	initial tensile test specimen gage length
$R_{\mathbf{N}}$	radial coordinate of node N
r, z	cylindrical spatial coordinates
S <sub>ij</sub>	deviatoric Cauchy stress
$\mathbf{v_i}$	velocity field
$x_{i}^{(i=1,2,3)}$	general spatial coordinates
x, y	Cartesian spatial coordinates
$\gamma_{\mathbf{o}}^{\mathbf{p}}$	octahedral plastic strain, = $(1/\sqrt{2})\epsilon_{ef}^{p}$ .
$\epsilon_{ m ef}^{ m p}$	effective plastic strain, $\equiv \int d_{ef}^p dt$
σ .	uniaxial stress in simple tension
$\sigma_{ extbf{ef}}$	effective stress, $\equiv (3 p_2)^{1/2}$
$ au_{0}$	octahedral stress, $\left(\sqrt{2}/3\right)\sigma_{ ext{ef}}$

#### PROGRAM USAGE

#### Problem Definition

This discussion is limited to those facets of problem definition unique to the present analysis of finite deformation. Additional program-dependent specifics of input and output are given in later sections.

Independent variables of the analysis include two spatial coordinates and ''time.'' Spatial coordinates are defined in a single fixed reference frame throughout the solution of a given problem. Since application is limited to problems of quasi-static deformation of rate-insensitive elastoplastic materials, the entire analysis is independent of time scale. Thus ''time'' represents any parameter convenient as an ordering reference for the deformation process.

Geometry. - The geometry of a deforming body is always given by the instantaneous configuration of the finite-element map. The initial, stress-free configuration is specified by definition of an array of triangular elements, each defined by the positions of three vertex nodes. Nodal coordinates are defined in the fixed Cartesian (FIPDEF) or cylindrical (FIPAX) coordinate system of the analysis. Nodes are assigned numerical identification in the order of specification of their coordinates. Elements are numbered in the order of specification of triplets of node numbers, each triplet defining a single element. Within each triplet nodes must be specified in counterclockwise order around the element. As deformation proceeds, the element map is deformed by updating of the nodal coordinates.

Material properties. - Elastic and elastoplastic material properties must be supplied. Elastic properties required are the Young's modulus and Poisson's ratio of linear elasticity. It is assumed that stress levels considered are sufficiently low  $(\sigma_{ij}/E << 1)$  that the elastic portion of the deformation is adequately represented by linear elasticity. Incompressible elastic material behavior in plane strain or of axisymmetric bodies may be approximated by specification of a bulk modulus considerably greater than the Young's modulus (K/E > 1000) for the material. In plane stress such behavior is treated exactly by prescribing a Poisson's ratio of 0.5.

Plastic deformation is governed by a discrete input relation between an equivalent stress and an equivalent plastic strain. The relation is supplied in the form of data point pairs. Equivalent stress-strain data may be supplied in terms of either effective  $\left(\sigma_{\rm ef}, \epsilon_{\rm ef}^{\rm p}\right)$  or octahedral  $\left(\tau_{\rm o}, \gamma_{\rm o}^{\rm p}\right)$  quantities. Thus, if property data are available from uniaxial tensile testing, the stress-strain relation input data are found as

$$\sigma_{\text{ef}} = \frac{3}{\sqrt{2}} \quad \tau_{\text{o}} = \sigma$$

$$\epsilon_{\text{ef}}^{\text{p}} = \sqrt{2} \gamma_{\text{o}}^{\text{p}} = \ln \frac{l}{l_{\text{o}}} - \frac{\sigma}{E}$$

The present formulation and numerical implementation are restricted to the consideration of work-hardening materials. The slope of the stress-plastic strain curve must be strictly positive.

Boundary conditions. - The principal unknowns of the analysis are nodal displacement and force vectors. Coordinate components of nodal vector quantities, position, displacement, and force are identified by index numbers derived from the node numbers. At node N the  $\mathbf{x}_1$  component of a vector quantity is indexed as number (2N - 1) and the  $\mathbf{x}_2$  component as (2N) in a matrix vector containing components at all nodes. In planar analysis (FIPDEF),  $\mathbf{x}_1 = \mathbf{x}$  and  $\mathbf{x}_2 = \mathbf{y}$ ; while in axisymmetric analysis,  $\mathbf{x}_1 = \mathbf{r}$  and  $\mathbf{x}_2 = \mathbf{z}$ .

Boundary conditions are set by prescribing a sequence of incremental values for appropriate nodal forces and/or displacements. The default condition at all nodes is null valued force components. This condition is automatically removed at any node by specification of nonzero incremental force components or of incremental displacement components. All incremental nodal boundary values are applied to the instantaneous configuration of a deforming body. Nodal force components represent loads not tractions. Thus in a plane stress analysis where thinning is considered nodal force components are loads on present thickness not load per unit thickness; the initial thickness is assumed to be unity but subsequently may vary. In axisymmetric analysis nodal force components are of the form

$$F_{i}^{N} = 2\pi R_{N}^{f_{i}}$$
 (i = 1, 2)

where  $R_N$  is the present radial coordinate of node N and  $f_i$  is a ring loading density. For further discussion of nodal force boundary conditions see references 1 and 2.

Incremental values of nodal force and displacement components may be specified individually for each increment (nonuniform conditions) or by providing a single value at each increment which is to be applied to a number of components (uniform conditions). Uniform and nonuniform boundary condition specification modes for displacements or for forces may not both be used in a single problem.

The total number of integration steps comprising a complete analysis is determined by two factors. The number of increments is user determined by the manner of boundary condition specification as discussed previously. Each increment may be divided into a number of smaller integration steps, or substeps, by invoking an 'autoload' option that restricts element stress variation within any substep. The autoload option requires user specification of maximum values for yield stress overshoot (applied to both initial yield and secondary yielding in cyclic loading) and octahedral stress variation over any integration step. The programs will divide user prescribed increments into a number of substeps to insure compliance with these stress-variation tolerances. The user may thereby obtain controlled accuracy but loses precise control over the amount of computing required.

### Restart Capability

Problems involving uniform displacement boundary conditions may be restarted at preselected integration steps of the analysis. After each such integration step a restart data block containing sufficient data for restart of the analysis is written into a user declared file. The user must specify the interval between integration steps from which restart data blocks are filed. Program response to the restart data interval specification

will involve counting of increments or of substeps as the autoload option is suppressed or activated. Restart data blocks filed for a particular problem are identified by number in their order of generation. A restarted problem may employ an additional number of uniform incremental boundary displacements and/or a revised or extended stress-strain curve.

The FIPDEF program allows restart data to be stored on either cards or tape files. The FIPAX program uses only tape.

#### Program Considerations

Program array dimensions are problem dependent and must be user specified by source code modification. Detailed requirements are given in sections discussing the FIPDEF and FIPAX programs.

If restart data blocks are to be written into or retrieved from tape files, the tape must be declared as logical file TAPE1.

ASCII formatting conventions (ref. 5) are employed and must be declared when the programs are compiled on the CDC RUN compiler.

#### THE FIPDEF PROGRAM

Analysis capability is provided for problems of planar deformation under conditions of either plane strain or plane stress. Either infinitesimal or finite-deformation analysis may be performed. Plane stress finite-deformation analysis may consider or neglect the effects of local thinning from an initial unit thickness. If thinning is considered, boundary force vectors are total loads on present thickness; if thinning is neglected, force vectors are to be interpreted as load per unit thickness.

Restart data blocks generated from intermediate integration steps may be stored on tape. A restart block from the final step of an analysis may be retained on either tape files or cards.

In the following sections information is provided on input/output data, program structure, and array variable minimum dimensions.

#### Input Data

In this section the complete FIPDEF input card stream for both initialization and restart problems is defined. Note that not all input cards defined will be present for a given problem.

Data

1 16(I4, 1x)

NINC: Number of loading increments.

NINF: Deformation mode control.

NINF = 1: full finite deformation analysis.

= 2: thinning suppressed (valid only for NZZ = 1 (CD. 8)).

= 3: infinitesimal deformation analysis.

NOUTP: Output print interval (default value, 1).

NPT: Input source key.

NPT = 0: initial card input; no restart data to be generated.

= 1: restart problem or initial problem card input with restart data to be generated.

Note: NPT = 1 is admissible only for NDIS = 0 on CD.8 and

NFC = 0 on CD. 12.

NPRNT: Increment number for initial output printing (default value, 1).

NITER: Maximum allowed cyclic loading evaluation iterations (default value-no limit).

INCP: Nodal data output control.

INCP = 0: partial output.

= 1: full output.

(See output block 14.)

If NPT = 0, skip to CD. 7.

2 16(I4, 1x)

NPTR: Restart data control.

NPTR = 1: restart data on tape.

= 2: restart data on cards.

= 3: initial problem from card data with restart data to be generated.

NEXT: Restart problem extension key.

NEXT = 0: no problem extension.

= 1: initial problem extended by increasing the number of loading increments.

Note: NEXT is ignored for NPTR = 3.

NTBLK: Number of the restart block on file TAPE1 from which problem data is to be retrieved.

NTMAX: Total number of restart record blocks on TAPE1.

CD	Format	Data
2	16(I4, 1x)	Notes: (a) Analysis will restart from block NTBLK and additional restart record blocks will be placed following block NTMAX.  (b) NTBLK, NTMAX are ignored for NPTR = 2.
		NOUTR: Increment/substep interval for tape restart data generation (default is no data generation).
		NPTG: Final increment restart data generation control.  For ISC = 0 (no ''autoload, '' see CD.27) -  NPTG = 0: no restart card data produced.  = 1: restart card data produced after the last substep of increment NINC.  For ISC = 1 (''autoload'' increment control, see CD.27) -  NPTG = 0: no restart data generation from last increment/  substep analysis.  = 1: restart data on TAPE1 and output print from last increment/substep analysis so long as NOUTR ≠ 0 on CD.2.
	•	NPROP: Restart problem stress-strain curve key.  NPROP = 0: use original curve.
		= 1: new curve to be supplied.
If NP	TR = 1, 2 and	estart card block is placed here.  NEXT = NPROP = 0, skip to CD. 27.  XT = 0, and NPROP = 1, skip to CD. 5.
3	<b>I</b> 4	NINC: New maximum number of loading increments.
4	10F8.1	$\frac{\text{TD(I)}\colon \ \text{K1} \leq \text{I} \leq \text{K2 (see CD. 14)}.}{\text{K1 = first increment number of restarted problem.}}$ $\text{K2 = NINC on CD. 3.}$
If NP	ROP = 0, skip	to CD.27.
5	<b>I4</b>	NPSS: Number of data points on revised stress-strain curve (see CD. 22); NPSS $\geq 3$ .
6	2E20.10	SS(I): $1 \le I \le 2$ (NPSS). Stress-strain curve data point vector; one ordered pair $(\sigma_{eq}, \epsilon_q^p)$ per card; data may be either octahedral or effective (see CD. 22).

Skip to CD. 27.

CD	Format	Data
7	A1, 7A10	NCAR: Output carriage control character.
		TITLE: Alphanumeric, up to 70 characters.
8	16(I4, 1x)	<u>IBD</u> : Bandwidth = (2) ( $ N2 - N1  + 1$ ) where $ N2 - N1  = maximum difference in numbers assigned to adjacent nodes.$
		NRD: Number of degrees of freedom associated with complete problem before application of boundary conditions.
		NEL: Number of elements.
		NXY: Nodal coordinate input format key for CD. 10.  NXY = 1: five nodal coordinate pairs per card.  = 2: one nodal coordinate pair per card.
	-	NDIS: Incremental displacement boundary condition mode:  NDIS = 0: uniform.  = 1: nonuniform.
		NF: Incremental force boundary condition mode.  NF = 0: uniform.  = 1: nonuniform.
		$\frac{NZZ}{NZZ}$ : Planar analysis mode control. $\frac{NZZ}{NZZ} = 1$ : plane stress. = 2: plane strain.
9	8(3I3, 1x)	$\underline{\text{NM}(I)} \colon \ 1 \leq I \leq 3 \ (\text{NEL}); \ \text{element definition, node identification in counterclockwise order around each element.}$
10	10F8.5	$\underline{XYMO(I)} \colon \ 1 \leq I \leq NRD; \ nodal \ coordinates \ in \ (x,y) \ pairs \ (see \ NXY, \ CD. \ 8).$
11	4E10.5	SFX: x-coordinate scale factor.
		SFY: y-coordinate scale factor.
		DX: x-coordinate shift after scaling.
		DY: y-coordinate shift after scaling.
12	16(I4, 1x)	NDC: Number of degrees of freedom eliminated by nonzero incremental displacement conditions.
		NZC: Number of degrees of freedom eliminated by zero incremental displacement conditions.

CD	Format	Data
12	16(I4, 1x)	NFC: Number of degrees of freedom eliminated by nonzero incremental force conditions.
		<u>IDBC</u> : Incremental nodal displacement boundary condition array input order (see CD.15) (ignored for NDIS = 0 on CD.8).
		<u>IFBC</u> : Incremental nodal force boundary condition array input order (see CD. 19) (ignored for NF = 0 on CD. 8).
		NNF: Number of boundary nodal force components included in boundary load summation (see CD. 23).
If ND	C = 0, skip to $0$	CD. 16.
13	16(I4, 1x)	$\underline{\text{NDP(I)}}\text{: }1 \leq I \leq \text{NDC; identification of boundary incremental nodal} \\ \text{displacement components set to nonzero values.}$
If ND	IS = 1, skip to	CD. 15.
14	10F8.1	$\underline{\mathrm{TD}(I)}$ : $1 \leq I \leq \mathrm{NINC}$ ; values of uniform incremental boundary nodal displacement.
If ND	IS = 0, skip to	CD. 16.
15	10F8.1	$\begin{array}{lll} \underline{DBC(I,J)} \colon \ 1 \leq I \leq \text{NINC array (NINC rows, NDC columns)} \\ 1 \leq J \leq \text{NDC} \\ \\ \text{Incremental displacement boundary condition value array. Input order is governed by IDBC (CD.12) as} \\ \underline{\text{IDBC}} = 0 \colon \text{input DBC by columns.} \\ &= 1 \colon \text{input DBC by rows.} \\ \\ \text{Note: Values are assigned to particular boundary displacements in the order of specification of the NDP(I) on CD.13;} \\ \underline{\text{e.g., DBC(I, J)}} = \text{incremental value assigned to displacement} \\ \underline{\text{NDP(J)}} \text{ at increment I.} \\ \end{array}$
16	16(I4, 1x)	$\frac{NZP(I)}{\text{set to zero values for all increments.}}$
If NF	C = 0, skip to	CD. 20.
17	16(I4, 1x)	$\frac{\text{NFP(I):}}{\text{force components set to nonzero values.}} \ 1 \leq I \leq \text{NFC; identification of boundary nodal incremental}$
If NF	= 1, skip to Cl	D. 19.

 $\underline{TF(I)} \colon\ 1 \leq I \leq NINC;$  values of uniform incremental boundary

nodal forces.

18

10F8.1

CD	Format	Data
If NF	= 0, skip to C	ED. 20.
19	10F8.1	FBC(I, J): Nonuniform boundary nodal incremental force boundary condition value array; defined analogously to DBC(I, J), CD. 15, in terms of NINC, NFC, IFBC, NFP.
20	3E20.8	PRT: Poisson's ratio, elastic.
		YMD: Young's modulus, elastic.
		RKAP: Bulk modulus, elastic.  Note: In plane strain, for PRT < 0.5 the input value of RKAP is ignored and RKAP = YMD/[3(1-2PRT)] is used. In plane stress the input value of RKAP is ignored.
21	16(I4, 1x)	IPSS: Stress - plastic-strain data point pair input order key.  IPSS = 0  = 1  the input order is $\begin{cases} \sigma_{eq}, \epsilon_{eq}^p \\ \epsilon_{eq}^p, \sigma_{eq} \end{cases}$
		NPSS: Number of stress - plastic-strain curve input points; NPSS $\geq 3$ .
		Note: If NPSS = 0, an elastic analysis will be performed; the maximum octahedral stress must be less than $10^{10}$ lb/in. <sup>2</sup> .
If NP	SS = 0, skip to	CD. 23.
22	2E20.10	$SS(I)$ : $1 \le I \le 2(NPSS)$ ; stress - plastic-strain curve data point pairs are read one pair per card (pair order set by IPSS on
	·	CD. 21) for NPSS cards.  Note: (a) The first point must be the proportional limit stress
		corresponding to $\epsilon_{\rm eq}^{\rm p}=0.0$ . (b) The first strain value is assumed to be 0.0. If the first strain input value is $\geq 0.0$ , the stress-strain data are assumed to be in terms of octahedral quantities. If the first value is $< 0.0$ , the data are assumed to be effective quantities. (c) The data must relate stress and logarithmic plastic strain.
23	16(I4, 1x)	$\underline{\text{NSF}(I)} \colon \ 1 \leq I \leq \text{NNF}; \ \text{boundary nodal force components which are} \\ \text{to be summed and output as total applied load.}$
24	16(I4, 1x)	NPATH: Number of contours in the x-y plane on which the J integral is to be computed.

16(I4, 1x)	Note: If NPATH = 0; no J integral computation is performed. (For J integral definition, see refs. 6 and 7.)
ATH = 0, skip to (	CD. 27.
	Note: The J integral is computed as a contour integral on piecewise continuous paths defined in terms of segments each of which is finite-element boundary. Thus a single path is defined by N segments involving $N+1$ nodes. An internal segment is bounded by two elements, a boundary segment by one.
16(I4, 1x)	NPSEG(I): $1 \le I \le NPATH$ ; number of segments for each of the NPATH paths.
16(I4, 1x)	$\frac{2_{\underline{NDSEG(I)}:}}{\text{specified in counterclockwise order along the path.}}$
16(I4, 1x)	$\frac{^{2}\text{NELSEG(I):}}{\text{1} \leq \text{I} \leq 2[\text{NPSEG(K)}];} \text{ elements bounding each of the segments defining path K. For internal segments two elements are identified by number;}^{3}$ for boundary segments the second number specified <u>must</u> be zero.
I4, 1x, 2F10.0	ISC: "Autoload" load substep scaling option key.
÷	<ul><li>ISC = 0: no scaling.</li><li>= 1: prescribed loading increments will be divided into substeps within which EYP, ETO are satisfied.</li></ul>
	ETO: Maximum fractional incremental variation of octahedral stress in any element undergoing plastic flow.
	EYP: Maximum fractional overshoot of specified proportional limit stress in any element; or maximum overshoot of yield stress for yielding subsequent to elastic unloading.
	16(I4, 1x) 16(I4, 1x) 16(I4, 1x)

<sup>&</sup>lt;sup>2</sup>A pair of consecutive cards 26(a), 26(b) are needed for each of the NPATH paths being defined.

being defined.  $^3$  Elements are assigned numbers according to their order of definition in the NM(I), CD.9.

CD	Format	Data
27	I4, 1x, 2F10.0	Note: "Autoload" substeps will be counted in determining
		output printing and tape restart data generation points but
	•	are not considered in setting NINC on CDS. 1 and 3; K1,
		K2 on CD. 4 or in response to NPRNT on CD. 1.

# Output Data

Specific output data from the FIPDEF program are dependent on the type of analysis performed and details of problem definition. All possible output messages and quantities are defined in this section.

Block	Generated for -	Contents, [generating subprogram], and OUTPUT MESSAGE
1	(see footnote 4)	Image of CD. 1. [IOPT].
2	NPT = 1	Image of CD. 2. [IOPT].
3	NPT = 0 or	-
	NPT = 1; $NPTR = 3$	START FROM CARDS. [IOPT].
		One of the following:
		PLANE STRAIN FINITE DEFORMATION ANALYSIS
		PLANE STRAIN INFINITESIMAL DEFORMATION
		ANALYSIS
		PLANE STRESS FINITE DEFORMATION ANALYSIS
		PLANE STRESS FINITE DEFORMATION ANALYSIS
		THINNING SUPPRESSED
		PLANE STRESS INFINITESIMAL DEFORMATION
		ANALYSIS
•		FOR ELEMENT THE BANDWIDTH HAS BEEN
	£	CHANGED FROM TO
		(If this message appears, a programmed stop
		follows immediately, indicating that IBD on CD. 8
		must be increased).
		Image <sup>5</sup> of CDS. 7 to 26. [SETUPP].
		Image of CD. 27. [IOPT].

<sup>&</sup>lt;sup>4</sup>Output produced for all problems.
<sup>5</sup>Initial nodal coordinates are printed after scaling and shifting according to input CD.11.

Block	Generated for -	Contents, [generating subprogram], and OUTPUT MESSAGE
4	NPT = 1	
	NPTR = 1	RESTART FROM TAPE. [IOPT].
	<b>= 2</b>	RESTART FROM CARDS.
5	NPT = 1	PROBLEM EXTENDED FROM K1 TO K2 STEPS.
•	NPTR = 1, 2	K1 = increment number from restart data block.
	NEXT = 1	K2 = new final increment number NINC from CD.3.
		TD VECTOR IS TD(I) $1 \le I \le K2$ . [IOPT].
6	NPT = 1	NUMBER OF SS POINTS IS NPSS.
	NPTR = 1, 2	SS(I) $1 \le I \le 2(NPSS)$ . [IOPT].
	NPROP = 1	
7(a)	footnote 4	STATE MAP STEP N-NAUTO. [PRNTIT].
		Indicates successful completion of analysis for substep NAUTO of increment N.
7(b)	footnote 4	PROGRAM IS ITERATING ON STEP N-NAUTO LOAD-
.(2)	10041000 1	ING REVERSAL FOR ITOT ELEMENTS THESE
		ELEMENTS ARE NREV(I) $1 \le I \le ITOT$ . [PRNTIT].
8	footnote 4	Element loading state key:
Ū	10041000	generated for all iterations; integer display of IRV
	•	vector indicating state of each element; IRV(I) takes
	•	the values 1, , 6; display FORMAT is labeled
		4000. [PRNTIT].
		IRV Significance
		1 elastic state
		2 yield has occurred on this increment
		3 continuing plastic flow
		64 elastic unloading detected
		5 elastic unloading continues
		6 false detection of elastic unloading, plastic
		flow resumes.

<sup>&</sup>lt;sup>6</sup>Detection of any element in this state causes its flow behavior to be appropriately modified and the incremental analysis to be repeated.

Block	Generated for -	Contents, [generating subprogram], and OUTPUT MESSAGE
9	Step 1 for	Problem definition data:
	NPRNT = 0, 1	NEL, NRD, IBD
		NZC, NDC, NFC
		YMD, GMD, PRT
		RKAP, SIGEQ YIELD
	•	NZP, NDP, NFP
		TD(1) or DBC $(1, J)$
		TD(1) or DBC $(1,J)$ see footnote 7.
		[OUTPUP].
10	Step N = PT	TAPE RESTART GENERATION (IOPT)
	for $NPT = 1$	
•	NOUTR ≠ 0	Binary write of restart data on logical file TAPE1.
		PT = N1 + (K) (NOUTR) - 1
		N1 = first increment of present run
		$K = 1, 2, 3, \ldots$
11	$^{8}$ Step N = P*	THE APPLIED LOAD AT STEP N-NAUTO IS FT
		THE INCREMENTAL LOAD IS FI. [OUTPUT].
	•	FT and FI are found as sums of nodal force compo-
		nents $NSF(I)$ . $1 \le I \le NNF$ .
12	ISC = 1	SCALED STEP. [OUTPUP].
13	Step 1 for	
	NPRNT = 0,1	Element map data: element-node key undeformed nodal coordinates. [OUTPUP].
14(a)	$^{8}$ Step N = P*	Current nodal coordinates
	INCP = 0	Current nodal forces
		Current element centroid coordinates. [OUTPUP].
14(b)	$^{8}$ Step N = P*	Nodal output:
	INCP = 1	current coordinates
		total displacements
		incremental displacements
		total forces
		incremental forces. [OUTPUP].

Only those quantities appropriate to a particular problem will be printed.  $^{8}P^{*} = NPRNT + (K) (NOUTP); K = 0, 1, 2, ....$ 

Block	Generated for -	Contents, [generating subprogram], and OUTPUT MESSAGE
15	<sup>8</sup> Step N = P*	Element output:  IRV (see block 8)  Almansi strains - EPSX, EPSXY  principal stresses in x-y plane - S1, S2  maximum shear stress - TM  principal stress in radians from +x axis - THET  Cauchy stresses - SIGY, SIGXY, SIGZ <sup>9</sup> equivalent stress - SIGEQ  equivalent plastic strain - EP  thickness stretch 10 - LZ. [OUTPUT].
16	<sup>8</sup> Step N = P*	Element output:  elastic energy density  plastic work density  total work density  hydrostatic tension.
17	<sup>8</sup> Step N = P*	THE ELASTIC ENERGY IS WE THE PLASTIC ENERGY IS WP
18	<sup>8</sup> Step N = P* NPATH ≠ 0	THE TOTAL ENERGY IS WT FOR A LOAD OF FT $J1 = RJ1(I)$ ; $1 \le I \le NPATH$ $J2 = RJ2(I)$ ; $1 \le I \le NPATH$ FOR NPATH PATHS $J1 \text{ BAR} =$ WITH STD. DEV. OF $J2 \text{ BAR} =$ WITH STD. DEV. OF $J2 \text{ BAR} =$ WITH STD. $J2 \text{ ACC} =$ WITH STD. $J2 \text{ BAR} =$ WITH STD. $J2 \text{ BAR} =$ WITH STD. $J2 \text{ BAR} =$
		STD. DEV. = $\sqrt{\frac{1}{\text{NPATH}}} \left[ \sum_{k=1}^{\text{NPATH}} (JI_k - JIBAR)^2 \right]$

<sup>&</sup>lt;sup>9</sup>Printed only from plane strain analysis.
<sup>10</sup>Printed only from plane stress analysis.

Block	Generated for -	Contents, [generating subprogram], and OUTPUT MESSAGE
18	<sup>8</sup> Step N = P* NPATH ≠ 0	$J1 = J_x$ ; $J2 = J_y$ The J integral is computed in accordance with reference 7. In a hyperelastic body it provides the energy release rate per unit translation of a cavity in a stressed body; deriving its vector sense from the direction of translation. Its physical significance, if any, for elastoplastic bodies is a matter of conjecture.

# Program Structure

The FIPDEF program consists of a main program and 24 subprograms. The logical connection between these program units is shown in figure 1. The function of each subprogram is as follows:

Subprogram	Function
FIPDEF	program execution control
PROCES	data flow control
IOPT	input-output control
SETUPP	card input processor
SETRST	restart data processor
OUTPUP	printed output
KGEN	stiffness matrix generation control
CNSTT1/2	element property matrix generation
GKT1/2	upper triangular stiffness matrix generation
GKB1/2	lower triangular stiffness matrix generation
PROG	incremental results processor
DGRADP	element displacement gradient evaluation
STRESP	element stress evaluation
MODEP	element loading state evaluation and autoload increment scaling

 $<sup>^{8}</sup>P^{*} = NPRNT + (K)(NOUTP); K = 0,1,2,...$ 

Subprogram	Function ————
TMODP	element loading state evaluation and autoload increment scaling
STRANP	element strain evaluation
PRNTIT	element loading state map print
JCOMP	J integral and element energy evaluation
SOLVE	stiffness equation solution control
STBC	boundary condition processor
SLVQ2	nodal incremental displacement solution
FRCMP	nodal incremental force evaluation

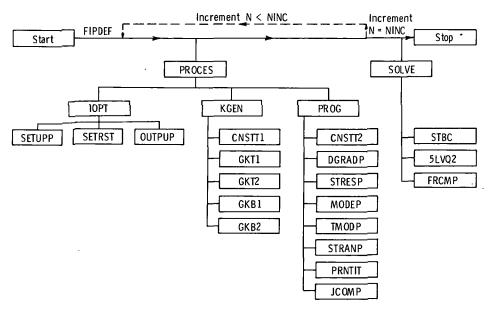


Figure 1. - FIPDEF subprogram flow.

The program executes in overlay form. There are six overlays at three levels of core which are loaded in one of four combinations, or links, at various times during execution:

Link	Overlays loaded	Function
1	(0,0),(1,0),(1,1)	Input/output
2	(0,0),(1,0),(1,2)	Stiffness matrix generation
3	(0,0),(2,0)	Displacement solution
4	(0,0),(1,0),(1,3)	Result processing

The overlay structure is given in figure 2. Logical files employed are identified as follows:

File	Usage	Used by subprograms
TAPE1	Restart data	SETRST
TAPE5	Input	IOPT, SETUPP
TAPE6	Output	IOPT, SETUPP, OUTPUP, PRNTIT
TAPE7	Punch	SETRST
TAPE17	Temporary storage	SETRST
TAPE18	Temporary storage	KGEN, SOLVE
TAPE19	Temporary storage	KGEN, SOLVE
TAPE25	Temporary storage	KGEN, PROG

(0,0): FIPDEF Labeled common blocks  CONST1 CONST2 KEY ARRAY1 BOUND BOUNDR			
(1, 0): PROCES Labeled common blocks  ARRAY2  ARRAY3  GEOMET  MATDAT  JCAL  PLAST			(2, 0): SOLVE Labeled common blocks ARRAY4 Subprograms STBC
(1, 1): IOPT Subprograms SETUPP SETRST OUTPUP	(1,2): KGEN Subprograms CNSTT1 GKT1 GKT2 GKB1 GKB2	(1,3): PROG Subprograms CNSTT2 DGRADP STRESP MODEP TMOD P STRANP PRNTIT JCOMP	SLVQ2 FRCMP

Figure 2. - FIPDEF overlay structure.

#### Array Dimensions

All array variables are dimensioned in labeled common block declarations. The labeled common blocks, their array contents, and problem dependent minimum array dimensions are given in this section. The content of common block ARRAY3 varies between overlays. Overlay locations for each form of the block are indicated in figure 2. Array dimensions are given in terms of problem input parameters defined in the FIPDEF input section.

Block	Variable	Dimensions
ARRAY1	FO	NRD
	DIS	NRD
	TITL	8
ARRAY2	SE	7 (NEL)
	FT	NRD
	TDYX33	NEL
ARRAY3	A(I, J)	$1 \le I \le IBD$
		$1 \leq J \leq NRD$
Overlays:		
(1,0),(1,2)	WASTE1	KK1 <sup>11</sup>
ARRAY3	RPT	NEL
	EOT	NEL
Overlays:	TO	NEL
(1,1),(1,3)	DIST	NRD
	DISI	NRD
•	EA	4(NEL)
	ST	7(NEL)
	IRV	NEL
	NREV	NEL
	SP	4(NEL)
	DGD	4(NEL)
	WE	NEL
	WPT	NEL
	WASTE2	KK2 <sup>11</sup>

 $<sup>^{11}</sup> K$  = (IBD)(NRD) - 26 (NEL) - (2NRD). When  $\, K > 0 \, , \, \, KK2$  =  $\left| \, K \, \right| \, , \, \, KK1$  = 0; when  $\, K < 0 \, , \, \, KK1$  =  $\left| \, K \, \right| \, , \, \, KK2$  = 0.

Block	Variable	Dimensions
ARRAY4	A(I, J)	$1 \le I \le [2(IBD) - 1]$ $1 \le J \le NRD$
BOUND	TF <sup>12</sup> TD NSF	NINC NINC NNF
BOUNDR	NDP NFP NZP DBC(I, J) <sup>12</sup> FBC(I, J) <sup>12</sup>	NDC NFC NZC $1 \le I \le NINC$ $1 \le J \le NDC$ $1 \le I \le NINC$ $1 \le J \le NFC$
GEOMET	NM XYM XYMO	3(NEL) NRD NRD
MATDAT	SS RP TO1 IDB EO	2(NPSS) NEL NEL NEL NEL
JCAL	NPSEG RJ1 RJ2 NDSEG NELSEG WP	NPATH NPATH NPATH NNODE <sup>13</sup> NELEM <sup>14</sup>

 $<sup>^{12}</sup>$ Dimensions shown are maximum possible; e.g., if NDIS = 0, TD is dimensioned to NINC, but DBC may be set to (1,1) as it is not used.

<sup>13</sup> NNODE is the total number of nodes required to define the NPATH paths.

 $<sup>^{14}\</sup>mathrm{NELEM}$  is the twice the total number of segments comprising the NPATH paths.

#### THE FIPAX PROGRAM

Analysis capability is provided for problems of either infinitesimal or finite axisymmetric deformation. The analysis is restricted to consideration of problems involving axisymmetric geometry and loading.

Restart data blocks drawn from any integration step of an analysis may be retained on tape.

In the following sections information is provided on input/output data, program structure, and array variable dimensions.

#### Input Data

In this section the complete FIPAX input card stream for both initialization and restart problems is defined. Note that not all input cards defined will be present for a given problem.

CD	Format	Data
1	16(I4, 1x)	NINC: Number of loading increments.  NPRNT: Increment number for initial output printing (default value, 1).
		NPT: Input source key.  NPT = 0: initial card input; no restart data to be generated.  = 1: restart problem or initial problem card input with restart data to be generated.  Note: NPT = 1 is admissible only for NDIS = 0 on CD. 9 and NFC = 0 on CD. 13.
		NPRNTI: Increment/substep output print interval (default value,  1).  ISC: Autoload substep scaling option key.  ISC = 0: no scaling.  = 1: prescribed loading increments will be divided into substeps within which EYP and ETO are satisfied.
		EYP: Maximum percentage overshoot of specified proportional limit stress in any element; or maximum overshoot of yield stress for yield subsequent to elastic unloading.
	•	ETO Maximum percentage variation of octahedral stress over a

substep in any element undergoing plastic flow.

1 16(I4, 1x)

Note: ''Autoload'' substeps will be counted in determining output printing and tape restart data generation points but are not considered in setting NINC on CDS. 1,4; K1,K2 on CD.5 or in response to NPRNT on CD.1.

NINF: Deformation mode key.

NINF = 0: finite deformation analysis.

= 1: infinitesimal deformation analysis.

If NPT = 0, skip to CD. 8.

2 16(I4, 1x) NPT1: Restart data control.

NPT1 = 1: initial problem from card data with restart data to be generated.

= 2: restart problem from tape data with problem modification.

= 3: restart problem from tape with no problem modification.

NRSTI: Increment/substep interval for tape restart data generation (default is no data generation).

NTBLK: Number of restart data block on file TAPE1 from which problem data are to be obtained.

NTMAX: Total number of restart data blocks on file TAPE1.

Note: (a) Analysis will restart from block NTBLK and further restart blocks will be placed following block NTMAX.

(b) NTBLK, NTMAX are ignored for NPT1 = 1.

NFINT: Final increment/substep restart data generation for ISC = 1 (ignored for ISC = 0).

NFINT = 0: Final increment/substep analysis restart data generation is not guaranteed.

= 1: Final increment/substep analysis results will be printed and restart data placed on file TAPE1.

If NPT1 = 1, skip to CD. 8.

If NPT1 = 3, END OF INPUT.

3 16(I4, 1x) NEXT: Restart problem extension key (ignored for NPT1 = 1).

NEXT = 0: no problem extension.

= 1: problem extended by increasing the number of loading increments.

CD	Format	Data
3	16(I4, 1x)	NPROP: Restart problem stress-strain curve key (ignored for NPT1 = 1).  NPROP = 0: use original curve.  = 1: new curve to be supplied.
If NEX	KT = 0, skip to	o CD. 6.
4	<b>I</b> 4	NINC: New maximum number of loading increments.
5	10F8.5	$\frac{\text{TD(I)}}{\text{K1}}: \text{ K1} \leq \text{I} \leq \text{K2 (see CD. 15)}.$ $\text{K1 = First increment number of restarted problem}.$ $\text{K2 = NINC on CD. 4}.$
If NPF	ROP = 0, END	OF INPUT.
6	16(I4, 1x)	<u>IPSS</u> : Input order for revised stress-strain curve (see CD. 22).
7	2E20.10	$\underline{SS(I)}$ : $1 \le I \le 2 \text{(NPSS)}$ . Revised stress-strain curve data point vector (see CD. 23).
END C	OF RESTART	PROBLEM INPUT.
8	A1, 7A10	NCAR: Output carriage control character.
		TITLE: Alphanumeric, up to 70 characters.
9	16(I4, 1x)	<u>IBD</u> : Bandwidth = $2( N2 - N1  + 1)$ , where $ N2 - N1  = maximum$ difference in numbers assigned to adjacent nodes.
		NRD: Number of degrees of freedom associated with complete problem before application of boundary conditions.
		NEL: Number of elements.
		NRZ: Nodal coordinate input format key for CD.11.  NRZ = 1: five nodal coordinate pairs per card.  = 2: one nodal coordinate pair per card.
		NDIS: Incremental displacement boundary condition mode.  NDIS = 0: uniform.
	·	$\underline{NF}$ : Incremental force boundary condition mode. NF = 0: uniform.

= 1: nonuniform.

CD	Format	Data
10	8(3I3, 1x)	$\underline{\mathrm{NM}(\mathrm{I})}$ : $1 \leq \mathrm{I} \leq 3 (\mathrm{NEL});$ element definition, node identification in counterclockwise order around each element.
11	10F8.5	
12	4E10.5	SFR: r coordinate scale factor.
	٠	SFZ: z coordinate scale factor.
		DR: r coordinate shift after scaling.
		<u>DZ</u> : z coordinate shift after scaling.
13	16(I4, 1x)	NDC: Number of degrees of freedom eliminated by nonzero incremental displacement conditions.
		$\underline{NZC} \colon \text{ Number of degrees of freedom eliminated by zero incremental displacement conditions.}$
		NFC: Number of degrees of freedom eliminated by nonzero incremental force conditions.
		<u>IDBC</u> : Incremental nodal displacement boundary condition array input order (see CD. 16) (ignored for NDIS = 0 on CD. 9).
		<u>IFBC</u> : Incremental nodal force boundary condition array input order (see CD. 20) (ignored for NF = 0 on CD. 9).
		NNF: Number of boundary nodal force components included in boundary load summation (see CD. 24).
If ND	C = 0, skip to	CD. 17.
14	16(I4, 1x)	$\underline{NDP(I)} \colon \ 1 \leq I \leq NDC; \ identification \ of \ boundary \ incremental \ nodal \\ displacement \ components \ set \ to \ nonzero \ values.$
If ND	IS = 1, skip to	CD. 16.
15	10F8.3	$\underline{TD(I)} \hbox{:} \ 1 \leq I \leq NINC; \ values \ of \ uniform \ boundary \ incremental \ nodal \\ displacement.$
If ND	IS = 0, skip to	CD. 17.
16	10F8.3	$\begin{array}{l} \underline{DBC(I,J)} \colon \\ 1 \leq I \leq \text{NINC array (NINC rows, NDC columns)} \\ 1 \leq J \leq \text{NDC} \\ \text{Incremental nodal displacement boundary condition value array.} \\ \text{Input order is governed by IDBC (CD. 13) as} \end{array}$

CD	Format	Data
16	10F8.3	IDBC = 0: input DBC by columns.  = 1: input DBC by rows.  Values are assigned to particular boundary displacements in the order of specification of the NDP(I) on CD.14; e.g., DBC(I, J) = incremental value assigned to displacement NDP(J) at increment I.
17	16(I4, 1x)	$\underline{NZP(I)} {:}  1 < I < NZC; \text{ nodal incremental displacement components} \\ \text{set to zero value for } \underline{all} \text{ increments}.$
If NF	C = 0, skip to	CD. 21.
18	16(I4, 1x)	
If NF	= 1, skip to 0	CD. 20.
19	10F8.2	$\underline{\mathrm{TF}(I)}$ : $1 \leq I \leq \mathrm{NINC}$ ; values of uniform incremental nodal forces.
If NF	= 0, skip to	CD. 21.
20	10F8.2	FBC(I, J): Nonuniform boundary nodal incremental force boundary condition value array; defined analogously to DBC(I, J) (CD. 16) in terms of NINC, NFC, IFBC, NFP.
21	3E20.8	PRT: Poisson's ratio, elastic.
		YMD: Young's modulus, elastic.
		<u>RKAP</u> : Bulk modulus, elastic. Note: For PRT $< 0.5$ , input value of RKAP is ignored and RKAP = YMD/[3(1 - 2PRT)] is used.
22	16(I4, 1x)	
		NPSS: Number of stress - plastic-strain curve input points; NPSS $\geq 3$ .  Note: If NPSS = 0, an elastic analysis will be performed; the maximum octahedral stress must be less than $10^{10}$ lb/in. $^2$ .

If NPSS = 0, skip to CD. 24.

CD	Format	Data	
23	2E20.10	<ul> <li>SS(I): 1 &lt; I &lt; 2(NPSS); stress - plastic-strain curve data point pairs are read one pair per card (pair order set by IPSS on CD. 22) for NPSS cards.</li> <li>Note: (a) The first point must be the proportional limit stress corresponding to ϵ<sup>p</sup><sub>eq</sub> = 0.0.</li> <li>(b) The first plastic-strain value is assumed to be 0.0. If the input strain value is ≥0.0, the stress - plastic-strain data are assumed to be in terms of octahedral quantities. If the first value is &lt;0.0, the data are assumed to be effective quantities.</li> <li>(c) The data must relate stress and logarithmic plastic strain.</li> </ul>	
24	16(I4, 1x)		
25	16(I4, 1x)	NPATH: Number of loci in r-z plane of axisymmetric closed surfaces on which J integral is to be computed.  Note: If NPATH = 0; no J integral computation is performed.	
If NPA	ATH = 0, end	of input.	
, ·		Note: The J integral is computed as an integral on a cylindrical surface whose locus in the r-z plane is a piecewise continuous path defined in terms of segments, each of which is a finite-element boundary. Thus a single path is defined by N segments involving N + 1 nodes. An internal segment is bounded by two elements; a boundary segment by one.	
26	16(I4, 1x)	$\frac{\text{NPSEG(I)}: \ 1 \leq I \leq \text{NPATH; number of segments for each of the}}{\text{NPATH paths.}}$	
<b>27</b> (a)	16(I4, 1x)	NDSEG(I): $15 \le I \le NPSEG(K) + 1$ ; nodes defining path K, specified in counterclockwise order along path.	
27(b)	16(I4, 1x)	$\frac{\text{NELSEG(I):}^{15}}{\text{ment defining path K. For internal segments two}} \\ = \frac{1 \leq I \leq 2[\text{NPSEG(K)}]; \text{ elements bounding each segment two}}{\text{ment defining path K. For internal segments two}} \\ = \frac{1 \leq I \leq 2[\text{NPSEG(K)}]; \text{ elements bounding each segments two}}{\text{elements are identified by number; for boundary segments the second element number specified must be zero.}$	

<sup>&</sup>lt;sup>15</sup>A pair of consecutive cards 27(a) and 27(b) are required for each of the NPATH paths being defined.

# Output Data

Specific data from the FIPAX program are dependent on the type of analysis performed and on the details of problem definition. All possible output messages and data are defined in this section.

Block	Generated for -	Contents [generating subprogram] and OUTPUT MESSAGE
1	(See footnote 4)	Image of CD.1. [PROCES].
2	NPT = 1	Image of CD. 2. [PROCES].
3	NPT = 1 NPT1 = 2,3	RESTART FROM TAPE. [PROCES].
4	$ NPT = 1 \\ NPT1 = 2 $	Image of CD.3. [PROCES].
5	NPT = 1 NPT1 = 2, NEXT = 1	Image of CD.4. [PROCES].
		PROBLEM EXTENDED FROM K1 TO K2 STEPS
		<ul><li>K1 = increment number from restart data block.</li><li>K2 = new final increment number from CD. 4.</li></ul>
		THE NEW TD VECTOR IS
6	NPT = 1, NPT1 = 2 NPROP = 1	Image of CD.6. [PROCES].
		THE NEW SS CURVE IS
7	NPT = 0 or NPT = 1, NPT1 = 1	FOR ELEMENT THE BANDWIDTH MUST BE CHANGED FROM TO (SETC)  (If this message appears, a programmed stop follows immediately, indicating that IBD on CD.9 must be increased).
8	NPT = 0 or NPT = 1, NPT1 = 0	Image <sup>16</sup> of CD. 8 to 27. [SETC].
		START FROM CARDS. [PROCES].

<sup>&</sup>lt;sup>4</sup>Output produced for all problems.

<sup>&</sup>lt;sup>16</sup>Initial nodal coordinates are printed after scaling and shifting according to input CD.12.

Block	Generated for -	Contents [generating subprogram] and OUTPUT MESSAGE
9(a)	See footnote 4	STATE MAP STEP N-NAUTO. [PRNTA]. Indicates successful completion of substep NAUTO of increment N.
9(b)	See footnote 4	PROGRAM IS ITERATING ON STEP N-NAUTO. LOADING REVERSAL FOR ITOT ELEMENTS THESE ELEMENTS ARE [PRNTA].
increment, of IRV vec IRV(I) take		Element loading state key: generated for all increment/substep iterations; integer display of IRV vector indicating state of each element. IRV(I) takes values 1, , 6. Display FORMAT is labeled 4000. [PRNTA].
		IRV Significance
		1 elastic state
		2 yield has occurred on this increment/ substep
		3 continuing plastic flow
		17 <sub>4</sub> elastic unloading detected
•		5 elastic unloading continues
		false detection of elastic unloading, plastic flow resumes.
11	Increment 1, substep 1 for	Element map data: Element-node key undeformed nodal coordinates. [OUTPT].
	NPRNT = 0	Problem definition data: NEL, NRD, IBD, NINC NZC, NDC, NFG YMD, GMD, PRT, RKAP $(\sigma_{eq})$ yield (either octahedral of effective, depending on SS input form; see CD. 23).

<sup>&</sup>lt;sup>4</sup>Output produced for all problems.

17Detection of any element in this state causes its flow behavior to be appropriately modified and the increment/substep analysis to be repeated.

Block	Generated for -	Contents [generating subprogram] and OUTPUT MESSAGE
12	Increment/substep N = K(NPRNTI) K = 1, 2, 3, for increments N* > NPRNT	Nodal data:  total displacements incremental displacements incremental forces total forces nodal coordinates. [OUTPT].  Element stress data: IRV (see block 10) Cauchy stress - SR, ST, SZ, SRZ principal stress in r-z plane - S1, S2 maximum shear stress principal stress in r-z plane in radians from +z axis - TS octahedral or effective stress - SIGEO hydrostatic stress invariants - J2, J3.
13	<pre>Increment/substep N = K(NPRNTI) K = 1, 2, 3, for increments N* &gt; NPRNT</pre>	Element deformation data:  element centroid coordinates - RC, ZC  Almansi strains - ER, ET, EZ, ERZ  coordinate direction stretches - LR, LZ, LT  principal stretches (in r-z plane) - L1, L2  principal stretch axis orientation in radians  from +z axis - TL  r-z plane shear angle - TS  r-z plane element rotation - TR  octahedral or effective plastic strain -  EPSEQP. [OUTPT].
14	<pre>Increment/substep N = K(NPRNTI) K = 1, 2, 3, for increments N* &gt; NPRNT</pre>	Element energy data: elastic energy density plastic energy density total energy density hydrostatic stress. [OUTPT].

15

Increment/substep
N = K(NPRNTI)
K = 1, 2, 3, . . .
for increments

 $N^* > NPRNT$ 

Problem energy summary [OUTPT]:

THE ELASTIC ENERGY IS --THE PLASTIC ENERGY IS --THE TOTAL ENERGY IS --FOR A LOAD OF ---

J1 = RJ1(I)  $1 \le I \le NPATH$ J2 = RJ2(I)  $1 \le I \le NPATH$ 

FOR --- PATHS

J1BAR = --- WITH STD. DEV. OF ---J2BAR = --- WITH STD. DEV. OF ---

JIBAR = 
$$\frac{1}{\text{NPATH}} \left( \sum_{k=1}^{\text{NPATH}} JI_k \right)$$
; I = 1, 2

STD. DEV. = 
$$\sqrt{\frac{1}{\text{NPATH}} \left[ \sum_{k=1}^{\text{NPATH}} (JI_k - JIBAR)^2 \right]}$$

$$J1 = J_r$$
;  $J2 = J_z$ 

The J integral is computed in accordance with reference 7. In a hyperelastic body it provides the energy release rate per unit translation of a cavity in a stressed body deriving its vector sense from the direction of translation. Its physical significance, if any, for elastoplastic bodies is a matter of conjecture.

THIS IS INCREMENT N-NAUTO OF NINC THE APPLIED LOAD IS FT THE INCREMENTAL LOAD IS FI. [OUTPT].

Block	Generated for -	Contents [generating subprogram] and OUTPUT MESSAGE
17	Increment/substep	SCALED STEP. [OUTPT]
	N = K(NPRNTI)	Message printed if autoload defined substep has
	$K = 1, 2, 3, \dots$ for increments	been introduced.
	N* > NPRNT	
	and $ISC = 1$	
18	NRSTI ≠ 0	TAPE RESTART GENERATION STEP
	for increment/substep N = K(NRSTI)	N-NAUTO OF NINC
	$K = 1, 2, 3, \dots$	

# Program Structure

The FIPAX program consists of a main program and 23 subprograms. The logical connection between these program units is given in figure 3. The function of each subprogram is as follows:

Subprogram	Function	
FIPAX	program execution control	
PROCES	incremental analysis setup and result evaluation control	
SETC	input processor	
SETRST	restart data processor	
OUTPT	printed output	
PSET	stiffness matrix generation control	
PMAT1 element property matrix generation		
INTEGR	element geometry integral evaluation	
GKT1/2	upper triangular stiffness matrix generation	
GKB1/2	lower triangular stiffness matrix generation	
CEVAL incremental result processor		
VGRD	element displacement gradient evaluation	
STRSA	element stress evaluation	

Subprogram	<u>Function</u>
MDA	element loading state evaluation and autoload increment scaling
TMDA	element plastic modulus evaluation
STRNA	element deformation evaluation
PRNTA element loading state map print	
JCOMP	J integral evaluation
PSLV	stiffness equation solution control
STBC	boundary condition processor
SLVQ	nodal incremental displacement solution
FRCMP	nodal incremental force evaluation

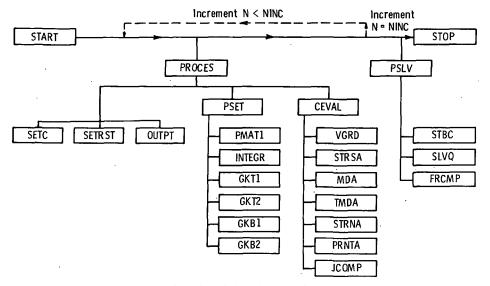


Figure 3. - FIPAX subprogram flow.

The program executes in overlay form. There are three overlays at two levels of core that are loaded in one of two combinations, or links, at different stages of execution:

Link	Overlays loaded	Function
1	(0,0), (1,0)	Input/output, stiffness matrix generation, and result
	(0,0), (2,0)	processing
2	(0,0), (2,0)	Displacement solution

(0, 0): F1PAX	Labeled of CONST KEY BOUND ARRAY2	ommon blocks	
(1, 0): PROCES Subprograms SETC - SETR ST- OUTPT+ PSET- PMAT1- INTEGR- GKT1- GKE1- GKB2- CEVAL+ VGRD+ STR SA+ MDA+ TMDA+ TMDA+ STRNA+ PRNTA+ JCOMP+	Labeled common blocks ARRAY4	(2, 0): PSLV Subprograms STBC SLVQ FRCMP	Labeled common blocks ARRAY5

<sup>&</sup>lt;sup>1</sup>Use ARRAY1 form 1 in subprograms marked -; use ARRAY 1 form 2 in subprograms marked +

Figure 4. - FIPAX overlay structure.

### Overlay structure is given in figure 4. Logical files used are identified as follows:

File	Usage	Used by subprograms
TAPE1	Restart data;	SETRST
	temporary storage	PROCES
TAPE5	Input	PROCES
		SETC
TAPE6	Output	PROCES
•		OUTPT
a de la companya de		PRNTA
TAPE18	Temporary storage	PSET
TAPE19	Temporary storage	PSET
		PSLV
TAPE25	Temporary storage	PROCES
		SETRST

### Array Dimensions

All array variables are dimensioned in labeled common block declarations. Labeled common blocks, their array contents, and problem dependent minimum array dimensions are given in this section.

The array content of common block ARRAY1 varies between subprograms of overlay (1,0). Subprogram locations for each form of the block are indicated in figure 4. Array dimensions are given in terms of problem input parameters defined in figure 3.

Block	Variable	Dimensions
ARRAY1, form 1 <sup>18</sup>	T(I, J)	$1 \leq I \leq IBD$
		$1 \le J \le NRD$
	WASTE2	кк2 <sup>19</sup>
ARRAY1, form 2 <sup>18</sup>	RPT	NEL
	EOT	NEL
	TO	NEL
	IRV	NEL
	NREV	NEL
	THTL	NEL
	SHR	NEL
	ROT	NEL
	EA	4(NEL)
	ST	4(NEL)
	DGD	5(NEL)
	STR	3(NEL)
	STRP	3(NEL)
	DIST	NRD
	WE	NEL
	WPT	NEL
	WASTE1	KK1 <sup>19</sup>
ARRAY2	DIS	NRD
	FO	NRD
	TITL	8
ARRAY4	SE	4(NEL)
	FT.	NRD
ARRAY5	<b>A</b> (I, J)	$\begin{aligned} &1 \leq I \leq [2(IBD) - 1] \\ &1 \leq J \leq NRD \end{aligned}$

<sup>&</sup>lt;sup>18</sup>See fig. 4.

 $<sup>^{19}{\</sup>rm K}=({\rm IBD})({\rm NRD})$  - 29(NEL) - NRD. If K > 0, KK1 + |K| and KK2 = 0. If K < 0, KK1 = 0 and KK2 = |K|.

Block	Variable	Dimensions
GEOMET	NM	2(NEL)
	XYMO	NRD
	XYM	NRD
	E(I, J)	$1 \le I \le 3$
		$1 \leq J \leq \mathtt{NEL}$
MATDAT	SS+	2(NPSS)
	RP	NEL
	TO1	
	IDB	
	EO	
JACAL	NPSEG	NPATH
	RJ1	
	RJ2	
	NDSEG	NNODE <sup>20</sup>
	NELSEG	NELEM <sup>21</sup>
	WP	NEL
BOUND	$\mathrm{TF}^{22}$	NINC
	${ m TD}^{22}$	NINC
	DBC(I, J)	$1 \le I \le NINC, 1 \le J \le NDC$
	FBC(I, J)	$1 \le I \le NINC$ , $1 \le J \le NFC$
	NSF	NNF
	NDP	NDC
	NFP	NFC
	NZP	NZC

### SAMPLE PROBLEMS

Input and output are presented for four simple sample problems: two for each of the FIPDEF and FIPAX programs. The problems are not intended to indicate the scope of application of the analysis but rather to provide an input preparation and output interpretation exercise for the user. Consequently, the examples are restricted to displacement

 $<sup>^{20}</sup>$ NNODE = total number of nodes required to define the NPATH paths.

 $<sup>^{21}</sup>$ NELEM = twice the total number of segments comprising the NPATH paths.

 $<sup>^{22}</sup>$ Dimensions shown are maximum possible, e.g., if NDIS = 0, then TD is dimensioned to NINC but DBC may be set to (1,1) as it is not used.

bounded problems involving bilinear elastoplastic materials and simple geometries. Since the program input data provide a complete problem definition, no additional discussion is necessary.

The four problems are as follows: For FIPDEF

- (1) Tables I and II simple tension of a rectangular bar under conditions of plane strain; two-element map (fig. 5).
- (2) Tables III and IV biaxial tension of a rectangular bar under conditions of plane stress; two-element map (fig. 5).
  and for FIPAX
- (3) Tables V and VI expansion of a thick-walled cylinder under zero axial load with restart data generation; 40-element map (fig. 6).
- (4) Tables VII and VIII restart from problem (3) and continue expansion of the cylinder.

All problems use finite deformation analysis. The autoload integration step scaling is used in problems (2) to (4).

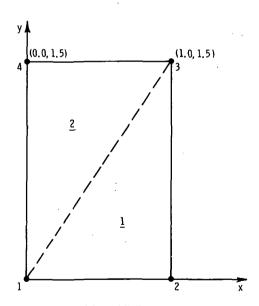


Figure 5. - Undeformed finite-element model sample problems (1) and (2). Node numbers, i; element numbers,  $\underline{i}$ .

TABLE I. - SAMPLE PROBLEM (1) - INPUT

STATEMENT ZE FORTRAN STATE	AN STATEMENT
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 35 30 40 41 42 43	23 34 35 36 37 38 39 40 41 42 42 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80
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9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41	77 38 39 40 41 42 41 42 46 47 48 49 50 51 52 53 54 55 50 57 38 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80
NASA-C-836 (REV 9-14-59)	(Ztra):

### Table II. - Sample problem (1) - output

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STATE WAP STEP

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### TABLE II. - Concluded. SAMPLE PROBLEM (1) - OUTPUT

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TABLE III. - SAMPLE PROBLEM (2) - INPUT

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### TABLE IV. - SAMPLE PROBLEM (2) - OUTPUT

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## TABLE IV. - Continued. SAMPLE PROBLEM (2) - OUTPUT

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NOUAL DATA

TABLE IV. - Continued. SAMPLE PROBLEM (2) - OUTPUT

TABLE IV. - Continued. SAMPLE PROBLEM (2) - OUTPUT

ELE N 18V	E AL	ALMAWSI STRAIN EPSY EPS	FRA IN EPSXY	77	51	PHINC1PAL S2	AL STRESS	THET	× els	Y 518	CAUCHY STRESS SIG AY S	STRESS AY SIGEO	Ä	
1 3 0 2 3 0 -PLANE	-0100 0 -0100 0 STRESS-	1 3 0.0100 0.3070 0.0070 2 3 0.0105 0.0090 0.0030 PLANE STRESSPLANE STRESS	.0000 .0000 .0000 STRESS	9892 0. 9892 0. PLANE S	1 3 0.0100 0.3090 0.0000 0.9897 0.1094245 0.11 2 3 0.0100 0.0090 0.0030 0.9892 0.10942405 0.11 -PLANE STPESSPLANE STPESSPLANE STPESSPLANE	0.1015E+09 0.1015E+09 ANE STRESS	0.3948E+0 0.3948E+0 5PLANE ST	U.*HY/ 0.1094E+05 0.1015E+05 0.394BE+03 0.0000 0.1094E+05 0.9892 0.1094E+05 0.1015E+05 0.394BE+03 0.0000 0.1094E+05 0PLANE SIPESSPLANE SIRESSPLANE SIR	1094E+05 1094E+05 STKESS-	0.1015E+ 0.1015E+ -PLANE ST	05 0.E+00 05 0.7032E-1 RESSPLANE	.094E+05 0.1015E+05 0.E+00 0.44981E+04 0.3298E-02.094E+05 0.1015E+05 0.7034E+11 0.4981E+04 0.3298E-02. STRESSPLANE STRESSPLANE STRESSPLANE STRESS-	4 0.3298E 4 0.3298E 16 STRESS	-05 -05.
ELE E 1 00	EL. EN. DEN 10.73027E+02	7*00 26*.	EL. EN. DEN PLS EN. DEN 00.73027E+02 00.47122E+02		EN. DEN F	TOT EN. DEN HYDHO. IENS. 00.12515E+03 00.70294E+04	• •	ELE EL. 2 00.78	EL. EN. DEN 0.78027E+02	PLS EN.	DEN _TOT EN +02 00.12515	EL. EN. DEN PLS EN. UEN TOT EN. UEN HYDRO. TENS. 00.78027E+02 00.47122E+02 00.12515E+03 00.70244E+04	• TENS•	
THE ELASTIC ENEMRY IN THE MLASTIC ENERGY IN THE TOTAL ENERGY IS	STIC EN STIC EN AL ENERA	EMGY 15 ERGY IS GY 15	000	00.1 00.7 89298E+	00.11HU22E.03 00.712762E.02 00.1H929HE.03FUK A LOAD OF	OAD OF	00.5d2077E-10	76-10						
STATE MAP	IAP STEP	~	۰											
3 THE APP THE INC SCALEU SAMPLE	3 3 THE APPLIED LOA THE INC. LOAD I SCALEU STEP SAMPLE PROBLEY	0 W V	T STEP 2- ; 0.11359E-10 PLANE STRESS	2 15 10 55 81AX1AL		0.87311E-10 Extension	NOUAL	S NUUAL UATA	STEP 2-	2 OF	~			
3,00E	COUR	COURDINATES			PISE	DISPLACEMENTS				-	FORCES			
2	4 C.00×U	₹ C00PB	אט טא	×	Ų	XVU	¥00	<b>&gt;</b>	FX	F	× in		Ur Y	z
1 2 3 -PLANE SAMPLE	0.0090 1.0137 1.0137 0.0030 ST-ESS-	0.0000 0.0000 1.5172 1.5172 	0 0.00300 0 0.013645 0 0.013845 0 0.00000 2 0.000000 STHESS-PLAN	*000000 *013645 *013645 *000000 \$PLANE S	0.0000 0.0000 0.00000 0.000000 0.00 1.0137 0.0000 0.013695 0.000000 0.00 1.0137 1.3172 0.013695 0.017195 0.00 0.000 1.5172 0.000000 0.017195 0.00 57-ESSPLAVE STHESSPLANE STHESSPLANE PROBLEM 2 PLANE STHESS HIAXIAL EXTENSION	0.000000 0.003544 0.003544 0.000000 AME STRESS	0.00000 0.003544 0.003544 	0000 -0.46965E+04 0000 0.86965E+04 3544 -0.86965E+04 3544 -0.86965E+04 NE STRESSPLANE S ELEMENT DATA	+04 -0.5 +04 -0.5 +04 0.5 +04 0.5 E STRESS-	-0.51894E+04 0.51894E+04 0.51894E+04 0.51894E+04 ESSPLANE STI	0.000000 0.000000 0.000000 -0.86965E+04 -0.51894E+04 -0.51235E+03 0.000000 0.00354 0.000000 0.86965E+04 -0.51894E+04 0.51235E+03 0.017195 0.003344 0.86965E+04 0.51894E+04 0.51235E+03 0.017195 0.000000 0.00354 0.86965E+04 0.51894E+04 0.51235E+04 0	3 -0.12332403 3 -0.12332403 3 0.12332403 3 0.12334403 5TRÈSSPLANE	E+03 E+03 E+03 E+03 E+03 E+03 E+03	- N m + 1
ELE	ΑL	ALMA 151 STRAIN	THAIN			PHINCIPAL	AL STRESS				CAUCHY	STRESS		
2	N INV FPSK	FPSY	EPSXY	77	7.	ž	Ξ	THET	S16 X	S16 Y	516 A	AY SIGEU	J.	
1 3 0 2 3 0 -rla:4	.0134 0 .0134 0 statss-	1 3 0.6134 0.9113 0.0600 2 3 0.0134 0.9113 0.0000 -LANE STAESSPLANE STRESS	.0000 0.0 .0000 0.1	9839 0. 9839 0. PLANE S	1166E+05 1166E+05 TPESSPL	0.9839 0.1166E+05 0.1042E+05 0.9839 0.1166E+05 0.1042E+05 iPLANE STRESSPLANE STRESS-	0.62076+0 0.62076+0	0.6407E+03 0.0000 0.1165E+05 0.6407E+03 0.0000 0.1165E+05 PLANE STRESSPLANE STRESS	1166E+05 1166E+05 STRESS-	0.1042E+ 0.1042E+ -PLANE ST	05 0.4.00 05 0.3062E-1 4ESSPLANE	1 3 0.0134 0.0113 0.0000 0.9439 0.1166E+05 0.1042E+05 0.6407E+03 0.0000 0.1166E+05 0.1042E+05 0.2400 0.5427E+04 (2 3 0.0134 0.0134 0.0113 0.0000 0.9439 0.1166E+05 0.1042E+05 0.5427E+03 0.0000 0.1166E+05 0.1042E+05 0.3642E-11 0.5427E+04 (2 3 0.0134 0.0134 0.0133 0.0000 0.9439 0.1166E+05 0.1042E+05 0.1042E+05 0.3642E-11 0.5427E+04 (2 3 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.	. 0.6998E-02 . 0.6998E-02 ME STRESS-	-05

# TABLE IV. - Concluded. SAMPLE PROBLEM (2) - OUTPUT

LE CL. E 1. UEH PLS EH. DEM TOT EM. DEM HYDMO. TENS. 1 00.85770E+02 00.10240E+03 00.18H17E+03 00.73574E+04

ELE EL. EN. UEN PLS EN. UEN 101 EN. UEN HYUHO. TENS. 2 00,85770E+02 00,10240E+03 00,18817E+03 00,73579E+04

Ŗ 00.129782E+03 00.154948E+03 00.284730E+03F0K A LOAD FLASTIC ENERGY IS PLASTIC ENFRGY IS TUTAL EVERGY 15 YYY

æ STEP STATE MAP

^ P 5 STEP NUUAL DATA THE APPLIEU LOAN AT STEP 2- 3 IS 0.14552E-( THE INC. LOWN IS 0.29104E-10 SAMPLE PHYBLEM ? PLANE STRESS HIAXIAL EXTENSION

JF.X FUNCES ř ĭ ELEMENT DATA Ϋ́ ň DISPLACEMENTS Ξ š Y COURD COURDINATES x C0:0-0 -PLANE SAMPLE HOUSE z

S16E0 CAUCHY STRESS SIG AY 516 Y SIG X THET PRINCIPAL STRESS Σ SS 7 7 EPSXY ALMANSI STRAIN N IRV EP X EP Y EL.

ELE EL. EN. DEN PLS EN. DEN 101 EN. DEN HYDHO. TENS. 2 00.93532E+02 00.1574BE+03 00.251U1E+03 00.76777E+04 EL. E1. DEN PLS EN. DEN TOT EN. DEN HYDHO. TENS. 00.93512E+02 00.15748E+03 00.25101E+03 00.76777E+04 00.141578E+03 00.238378E+03 ELASTIC EVERGY IS PLASTIC ENERGY IS TOTAL EVERGY IS 里里里

ELE 1

00.379956E+03FOR A LUAD UF

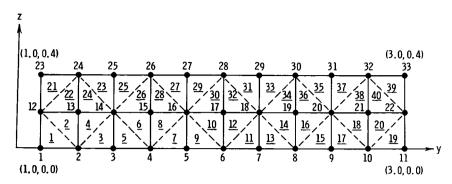


Figure 6. - Undeformed finite-element model sample problems (3) and (4). (Node numbers, i; element numbers,  $\underline{i}$ .)

TABLE V. - SAMPLE PROBLEM (3) - INPUT

TATEMENT NUMBER					FORTR	RAN STAT	EMENT					IDENTIFICATION
2 3 4 5 6	7 8 9 10 II	12 13 14 15 16 17 11	19 20 21 22 23 2	25-26 27 28 29 30	31 32 33 34 35 36	37 38 39 40 41 42	43 64 45 46 67 41	8 49 50 51 52 53 54	55 56 57 58 59 60	61 62 63 64 65 66	67 68 69 70 71 72	13 14 75 76 77 78 79
2	0	1	0 1	1	5	0						
1	3	0	0 1									
FIPAX	SAMP	LE PROB	LEM 3	EXP AN	SIONO	F A TH	ICK WA	LL TUB	E			
2,6	6,6	4.0	10	1								
1 2	1.2	2 13 1	2 2	3 14	2. 1.4	13	3 4 1	4 4	15 14	4 5	1.6	4 1 6 1 5
56		6. 1.7.1	6 6	7. 1.8	6. 1.8	17	7. 8. 1	8 8	19 18	8 9	2.0	8 2 0 1 9
9 10		10. 21. 2	0. 1.0	1,1, 2,2,	_1.02.2	21 1	2 24 2	31.2_	13. 24	14 25	24 1	3 1 4 2
4 2 6	2.5	14 15 2	6 1.6	2.7. 2.6	1,5_1,6	261	6 28 2	7 16	17 28	18 29	28 1	7 18 2
8 30	2.9	18, 19, 3	0 20	3 1 3 0	1.9 2.0	3.02	0_32_3	120_	21 32	22 33	3.2 2	1 2 2 3
1	. 0.	00	12		.,0,	1.4		1	6	0. 0.	18	
2	. 0	0.0	2.2			2.4	0.0	1	. 6	0.0	2.8	0.
3	-0	00	1.0		. 2	1.2	0, 2	1	. 4	0.2	1.6	0.
1	8,	0. 2	2.0	) o	2	2.2	02		. 4	0.2	2,6	0
2	8,,	02	30	0	. , 2,	10	04	1	. 2	04	14	0
1	. 6, , , ,	0.4	1.8	0	. 4	2.0	0.4	2	. 2	0.4	, 2,,4	0.
2	. 6	0.4	2.8	, , , , , , , , , 0	. 4	3.0	0,.,4	 				
_,,_	_10	1	J. 0	0.0	 	0.0		<u> </u>		<u> </u>	<del></del>	· · · · · · · · · · · · · · · · · · ·
3	1,1,	0	00	3			<u> </u>	ļ.,		<u> </u>		<u> </u>
. 1	2.3	4.5	I	ļ.,,.,.,.	· · · · · · · · · · · · · · · · · · ·	<u> </u>	<u> </u>	<u> </u>			, , , , ,	
0.0	0.5,,	0.005	<u> </u>	<u></u>	L	<u> </u>	,	<u> </u>			_,_,_,	
2	4	6,	8 1.0	1.2	1,4, ,	1,6,	1,8,,,,2	0, , , ,2,2	1 -1 -1 1	<u> </u>	<del>, , , , , , , , , , , , , , , , , , , </del>	<del>                                     </del>
			3	<b></b>	1,0,0,0,0	0,0,0,	<b>, , , , , ,</b>	<u> </u>				ļ
0	3	<u> </u>		ļ		<b></b>	ļ	<u> </u>				ļ <del> </del>
		1.0 0 0 . 0				0,1	<u> </u>	<del> </del>	<u> </u>	! <del>!</del>		<u> </u>
_,		110000	0.0			1.0	<b> </b>	<b> </b>	<del> </del>	<b> </b> i		
		210000	<u> </u>		<u> </u>	2.0	<del> </del>	<b> </b>	<b></b>	L		<del></del>
1	23	4.5	<u> </u>			<del> </del>	<u> </u>	<del> </del>	<del></del>	<del> </del>		<del></del>
0	<u> </u>		<u> </u>				<u> </u>	L				73 74 75 76 77 78 79

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### TABLE VI. - SAMPLE PROBLEM (3) - OUTPUT

2 0 1 0 1 1 3 0 0 1 FINITE DEFORMATION ANALYSIS ·AAISYNMETHIC··AAISYNMETHIC··AAISYNMETHIC··AAISYMMETHIC··AAISYMMETRIC··AAISYNMETHIC··AAISYNMETHIC··AAISYNMETHIC FOR REFERENCE. THE INPUT DECK IS REPRODUCED IN ITS ENTIRETY 3 EXPANSION OF A THICK WALL TUBE SAMPLE PROBLEM 6n s 4 8 24 15 19 13 4 8 14 -- -13 15 19 24 15 6 7 14 10 11 22 16 27 26 20 31 30 50 10 55 18 17 21 26 30 20 24 28 32 . 17 53 12 18 ---20 20 20 14 724 18 28 10 12 10 14 26 25 14 15 26 18 19 30 15 50 10 35 / 59 27 \ 31 16 17 21 28 32 18 29 33 1.2000 0.0000 1.4000 0.0000 1.6000 0.0000 1.6000 0.0000 2.0000 0.0000 2.2000 0.0000 2-4000 U-000U 1.0000 0.0000 0.2000 0.2000 2.6000 0.0000 2.8000 0.0000 3.0000 0.0000 1.0000 0.2000 1.2000 1.0000 1.8000 0.2000 0.2000 1.4000 2.0000 0.2300 2.2000 0.2000 1.6000 0.4000 2.6000 0.2000 2.4000 0.2000 2.5000 0-2000 3.0000 0.2000 1.0000 3.4000 1.2000 0-4000 1.8000 0.4000 <.2000 0.4000 2.4000 00.10000000E+01 3.0000 0.4000 00.10000000E+01 0 45 \_0.5000E-02\_0.5000E-02\_6 \_16 ----10 12 14 16 20 -- 00,3000000E+00 U0.10000000E+07 -0.E+00 00.10000000000E+05 -0.1000000000E+00 45 53 n AXISYMMETTIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMMETRIC++AXISYMIC++AXISYMETRIC++AXISYMETRIC++AXISYMMETRIC++AXISYMETRIC++AXISYMETRIC++AXISYMETRIC++AXISYMETRIC++AXISYMETRIC++AXISYMETRIC++AXISYMETRIC++AXISYMETRIC++AXISYMETRIC++AXI START FROM CARDS STATE MAP STEP 1 --EXPANSION WALL TUBE STEP 1 -GEOMETRY ELE NODES COORDINATES N2 ZN3 N3 1.00000 1.20000 1.00000 0.20000 0.00000 0.00000 1.20000 0.20000 0.00000 1.20000 0.20000 1.00000 3 0.00000 1.40000 0.00000 1.40000 14 0.20000 1.20000 13 1.20000 0.00000 1.40000 0.20000 1.40000 0.00000 1.60000 0.20000 15 14 1-60000 0.00000 1.60000 0.20000 1.40000 0.20000 1.00000 1.80000 0.00000 1.80000 1.60000 1.60000 0.00000 1.80000 0.20000 0.20000 1.80000 0.00000 2.00000 0.00000 0.20000 1.80000 17 10 16 2.00000 0.00000 2.00000 0.20000 1.80000 0.20000 2.00000 2.20000 0.00000 2.20000 2.00000 0.00000 2.20000 0.20000 2.00000 0.20000 0.00000 2.40000 0.00000 2.20000 19 19 2.40000 18 0.20000 0.20000 2.40000 0.00000 2.60000 0.00000 2.60000 20 0.20000 0.20000 19 17 10 20 2.60000 0.00000 2.80000 0.00000 2.60000 0.20000 21 2.00000 0.60000 2.80000 0.20000 0.20060 2.60000 2-60000 0.00000 3.00000 0.00000 3-00000 0.20000 2.00000 0.00000 3.00000 2.00000 0.20000 53 51 24 13 0.40000 12 23 1.40000 0.20000 1.20000 1.00000 0.40000 1.00000 0.20000 1.20000 0.40000 24 0.20000 14 25 1.40000 1.40000 0.40000 1.20000 0.40000 1.20000 24 0.20000 1.40000 0.20000 1.20000 0.40000 25 26 15 25 1-40000 0.20000 1.60000 0.40000 1.40000 0.40000 1.00000 14 0.20000 1.50000 0.20000 0.40060 27 27 26 16 1.00000 0.20000 1.60000 0.40000 1.60000 0.40000 26 0.20000 1.40000 0.20000 0.40000 28 29 16 2H 1.00000 1.60000 16 1.00000 1.80000 28 28 2.00000 30 17 1.50000 0.20000 0.20000 2.00000 0.40000 2.20000 0.20000 2.00060 0.40000 0.40000 54 58 32 2.00000 0.20000 2.20000 0.20000 2.00000 0.40000 .13 30 2.20000 0.20000 0.40000 2.20000 0.40000 14 2.40000 14 14 30 2.20000 0.20000 2.40000 0.20000 0.40000 30 0.20000 20 2.00000 2.60000 0.40000 0.40000 2.40000 2-40000 0.20000 2.40000 36 14 20 30 0.20000 2.50000 0.40000 31 32 2.40000 U.20000 0.40060 2.40000 51 55 50 36 21 2.60000 0.20000 2-40000 0.20000 2.00000 0.40000 3.00000 3.00000 0.40000 2.40000 0.40000 34 2.00000 0.20000 3.00000 0.20000 Z. H000U 0.40000

### TABLE VI. - Continued. SAMPLE PROBLEM (3) - OUTPUT

SAMPLE PROBLEM & EXPANSION OF A THICK WALL TUBE

.....

ZENO DISPLACEMENT DEGREES OF FREEDOM ARE

PROHLEM SUMMARY

STEP 1 - 1 OF 2

2 4 6 8 10 12 14 16 18 20 22

NEL= 40 N/C= 11 NINC= 2 YMD=10.00000E+05 PKAP= 25.00000E+05 NRD= 66 NDC= 3 GMU=36.40154E+04 PRT=0.30000 SIGEO YIELD= 10000.00

		DISPLACE	MENT HOUNDED	DEGREES OF FRE	EEDOM ARE	<del></del>			·
		N= DU= 0.0	00500 1	45					
				TOTAL	DISPLACEMENTS				
2.00500000	0.00000000	0.00-25183	0.00000000	0.00377409	0.00000000	76046600.0	0.00000000	0.00313603	0.00000000
0.00242355	0.00000000	0.00277101	0.00000000	0.00264478	0.00000000	0.00255317	0.00000000	0.00247751	0.00000000
0.0024237H	0.00000000	0.00500000	00005279	0.00429385	00004698	0.00376076	00034830	0.00340974	000004801
0.00312825	00004#68	0.00292979	00004871	0.00276652	00004458	0.00264632	00004859	0.002550+3	00004852
3.3024797H	00004860	0.00242190	00004875	0.00500000	00010895	0.00425163	00009199	0.00377480	00009713
0.00339692	00009731	0.00313627	00009720	0.00292359	00009747	0.00277099	00009711	0.00264477	00009721
0.00255323	00009705	0.00247767	00009718	0.00242401 A*TMQ.IQUBMI	00009758 CH/UK+BOLDMT/				
~c.00500000	0.0000000	0.00425183	0.0000000	0.00377409	0.00000000	0.00339637	0.0000000	0.00313603	0.00000000
0.00292355	0.00000000	0.00277101	0.00000000	0.00264478	0.00000000	0.00255317	0.00000000	0.00247751	0.00000000
0.00242378	0.0000000	0.00500000	00005279	0.00429385	00004698	0.00376076	00004830	0.003409/4	UU004851
3.00312825	00004568	0.00292979	00004671	0.00276652	00004858	0.00264832	00004859	0.002550+3	00004852
0.00247978	00004460	0.00242190	00004875	0.00500000	00010895	0.00425163	00009199	0.00377480	00009713
3.00339692	00009731	0.00313627	00009720	0.00292359	00009747	0.00277099		0.0026+477	
0.00255323	00009705	0.00247767	00009718	0.00242401	00009758				
			1	NCREMENTAL	FORCES	• •	• "	• •	
1917.3	-37.5	-0.0	49.0	-0.0	-12.3	0.0	-0.8	-0.0	1.7
-0.0	-1.8	-0.0	2.1	-0.0	-1.5	-0.0	1.4	-0.0	6.00
00.0	-1.1	4282.0	-0.0	-0.0	-0.0	-0.0	00.0	00.0	-0.0
U.0	00.0	-0.0	-0.0	00.0		-0.0	-0.0	00.0	00.0
-0.0	-0.0	00.0	00.0	1940.2	+0.0	-0.0	-0.0	-0.0	-0.0
0.0	-0.0	00.0	-0.0	00.0	00.0	00.0	-0.0	00.0	00.0
00.0	-0.0		00.0	00.0	00.0				
				TOTAL	FORCES				=
1917.3	-37.5	-0.0	49.0	-0.0	-12-3	0.0	-0.8	-0.0	<sup>-</sup> 1'.7
-0.0	-1.8	-0.0	2.1	-0.0	-1.5		1.4	-0.0	00.8
00.0	-1.1	4262.0	-0.0	-0.0	-0.0	-0.0	00.0	00.0	-0.0
0.0	00.0	-0.0	-0.0	00.0	00.0	-0.0	-0.0		00.0
-0.0	-0.0	00.0	00.0	1940.2	-0.0	-0.0	-0.0	-0.0	-0.0
0.0	-0.0	00.0	-0.0	00.0	00.0	.00.0	-0.0	00.0	_00.0
00.0	-0.0	00.0	00.0	00.0	00.0				
				NODAL	COORDINATES				
1.005000	0.000000	1.204252	0.00000	1.403774	· · · · · · · · · · · · · · · · · · ·	1.603396	T 5.000000	1.803136	0.000000
2.002424	0.000000	2.202771	0.000000	2.402645	0.00000	2.602553	0.000000	2.802478	0.000000
3.002424	0.000000 -	1.005000	00.199947	1.204294	00.199953	1.403761	00.199952	1.603410	00.199951
1.803128	00.199951	2.002930	00.199951	2.202767	00.199951	2.402648	00.199951	2.602550	00.199951
2.802480	00.199951	3.002422	00.199951	1.005000	00.399891	1.204252	00.399908	1.403775	00.399903
2.602480	00.199951 00.399903	3.002422 1.803136	00.199951	1.005000	00.399891 00.399903				
2.802480 1.603397 2.602553	00.199951 00.399903 00.399903	3.002422 1.803136 2.802478	00.199951 00.399903 00.399903	1.005000	00.399891	1.204252	00.399908	1.403775 2.402645	00.399903 00.399903
2.802480 1.603397 2.602553	00.199951 00.399903	3.002422 1.803136 2.802478	00.199951 00.399903 00.399903	1.005000 2.002924 3.002424	00.399891 00.399903 00.399902	1.204252	00.399908	1.403775	00.399903 00.399903
2.802480 1.603397 2.602553	00.199951 00.399903 00.399903	3.002422 1.803136 2.802478	00.199951 00.399903 00.399903	1.005000	00.399891 00.399903 00.399902	1.204252	00.399908	1.403775 2.402645	00.399903 00.399903
2.802480 1.603397 2.602553	00.199951 00.399903 00.399903	3.002422 1.803136 2.802478	00.199951 00.399903 00.399903	1.005000 2.002924 3.002424	00.399891 00.399903 00.399902	1.204252	00.399908	1.403775 2.402645	00.399903 00.399903
2.802480 1.603397 2.602553	00.199951 00.399903 00.399903	3.002422 1.803136 2.802478	00.199951 00.399903 00.399903	1.005000 2.002924 3.002424	00.399891 00.399903 00.399902	1.204252	00.399908 00.399903 SIEP	1.403775 2.402645	00.399903
2.602480 1.603397 2.602553 SAMPLE PROB	00.199951 00.399903 00.399903 ILEM 3 EXPANS	3.002422 1.803136 2.802478 ION OF A THIC	00.19951 00.399903 00.399903 K WALL TUBE	1.005000 2.002924 3.002424 STRESS ELE	00.399891 00.399903 00.399902 EMENT DATA	1.204252	00.399908 00.399903 SIEP	1.403775 2.402645 1 - 1 OF	00.399903 00.399903
2.802480 1.603397 2.60253 SAMPLE PROB	00.194951 00.394903 00.394903 LEM 3 EXPANS	3.002422 1.803136 2.802478 ION OF A THIC	00.199951 00.399903 00.399903 K WALL TUBE	1.005000 2.002424 3.002424 STRESS ELE	00.399891 00.399903 00.399902 EMENT DATA	1.204252 2.202771	00.399903 00.399903 SIEP	1.403775 2.402645 1 - 1 OF	2
2.602480 1.603397 2.602553 SAMPLE PROB	00.194951 00.349403 00.394403 EEM 3 EXPANS SR ST	3.002422 1.803136 2.802478 ION OF A IHIC	00.199951 00.399903 00.399903 K WALL TUBE SRZ	1.005000 2.002724 3.002424 STRESS ELE 51 S2	00.399891 00.399403 00.399402 EMENT DATA S12	1.204252 2.202771 TS SIGE	00.399903 00.399903 SIEP 0 S	1.+03775 2.402645 1 - 1 OF J2	00.399903 00.399903 2 2
2.002480 1.603397 2.602553 SAMPLE PROB NEL IRV	00.194951 00.394903 00.394903 BLEM 3 EXPANS SR ST 9E+04 0.3085E+0 0E+04 0.3141E+	3.002422 1.803136 2.302473 ION OF A INIC	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02-	1.005000 2.002424 3.002424 STRESS ELE 51 S2	00.399891 00.399903 00.399902 EMENT DATA \$12	1.204252 2.202771 TS SIGE E+040.00 0.546 E+040.04 0.502	00.399903 00.399903 SIEP 0 S 0E+04 0.3741E 1E+04 0.1d2UE	1.+03775 2.402645 1 - 1 0F J2 +03 0.1001E+08 +03 0.8396E+07	00.399903 00.399903 2 2 0.3152E+10 0.1974E+10
2.602480 1.603397 2.602553 SAMPLE PROB NEL IRV 1 1-0.261 2 1-0.259 3 1-0.165	00.194951 00.399903 00.399903 ILEM 3 EXPANS: SR ST 9E+04 0.3685E+0 0E+04 0.3161E+1 0E+04 0.3449E+1	3.002422 1.803136 2.802473 ION OF A THIC SZ 04-0.5595E+02 04-0.5471E+02 04-0.3206E+01	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02-	1.005000 2.002724 3.002424 STRESS ELE 51 S2 0.5595E+02-0.24 6.5138E+02-0.25	00.399891 00.399902 00.399902 EMENT DATA \$12 519E-04 0.1337 953E-04 0.1271	1.204252 2.202771 TS SIGE E-040.00 0.546 E-040.04 0.502 E-030.02 0.357	00.399908 00.399903 SIEP 0 S	1.403775 2.402645 1 - 1 0F J2 •03 0.1001E•06 •03 0.8396E•07 •03 0.4264E•07	00.399903 00.399903 2 J3 0.3152E+10 0.1174E+10 0.1174E+10
2.002480 1.603397 2.602553 SAMPLE PROB NEL IRV 1 1-0.261 2 1-0.259 3 1-0.155 4 1-0.155	00.194951 00.399903 00.399903 ILEM 3 EXPANS SR ST 98*04 0.36856*( 108+04 0.31916*( 108+04 0.3498*( 108+04 0.24498*(	3.002422 1.803136 2.802478 ION OF A INIC 5Z 04-0.5471E+02 04-0.5471E+02 04-0.3206E+02	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02- -0.2564E+02-	1.005000 2.002724 3.002424 3.002424 STRESS ELE 51 52 0.5595E+02-0.26 0.5595E+02-0.26 0.2608E+01-0.16 0.1767E+02-0.11	00.399891 00.399902 00.399902 EMENT DATA 512 5196+04 0.1237 593E+04 0.1271 555E+04 0.1271 255E+04 0.9381	1.204252 2.202771 TS SIGE E+040.00 0.548 E+040.04 0.502 E+030.02 0.357 E+030.04 0.395	00.399903 00.399903 SIEP 0 S 0E+04 0.3741E 1E+04 0.1020E 7E+04 0.2026 6E+04 0.2018E	1.+03775 2.402645 1 1 0F J2  *03 0.1001E*08 *03 0.4396E*07 *03 0.4264E*07 *03 0.4264E*07 *03 0.5210E*07	0.399903 0.399903 2 J3 0.3152E+10 0.1174E+10 0.1119E+10 0.1174E+10
2.002480 1.603397 2.602553 SAMPLE PROB NEL IRV 1 1-0.259 3 1-0.155 5 1-0.124	00.194951 00.399903 00.399903 ILEM 3 EXPANS SR ST 98-04 0.36856+ 105-04 0.31916+ 105-04 0.31916+ 105-04 0.24496+ 105-10 0.21156+	3.002422 1.803136 2.802478 ION OF A INIC SZ 04-0.5471E-02 04-0.3206E-01 04-0.3206E-01 01440E-01	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02- 0.2564E+02- 0.7827E-02- 0.7827E-02-	1.005000 2.002924 3.002424 STRESS ELE 51 S2 0.5595E+02-0.27 6.5138E+02-0.25 0.2608E+01-0.16 0.1767E+02-0.13	00.399891 00.399902 00.399902 EMENT DATA 512 5196-04 0.1337 5936-04 0.1271 5556-04 0.8262 596-04 0.9340	1.204252 2.202771 TS SIGE E+040.00 0.548 E+040.04 0.502 E+030.02 0.357 E+030.04 0.395 E+030.02 0.294	00.399908 00.399903 SIEP 0 S 0E+04 0.3741E 1E+04 0.1820E 7E+04 0.2037E 6E+04 0.2037E 6E+04 0.2038E	1.403775 2.402645 1 - 1 0F J2  •03 0.1001E•08 •03 0.4396E•07 •03 0.4264E•07 •03 0.5210E•07	00.399903 00.399903 2 J3 0.3152E+10 0.1474E+10 0.1174E+10 0.7772E+09
2.002480 1.603397 2.602553 SAMPLE PROB NEL IRV 1 1-0.261 2 1-0.259 3 1-0.155 4 1-0.155 5 1-0.124 6 1-0.117	00.194951 00.399903 00.399903 ILEM 3 EXPANS: SR ST 9E+04 0.3685E+(05+04 0.3191E+(05+04 0.3191E+(05+04 0.4495E+(05+04 0.4495E+(	3.002422 1.803136 2.802478 ION OF A THIC 5Z 04-0.54716-02 04-0.54716-02 04-0.34066-01 04-0.34066-01 04-0.34716-02	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02- 0.7927E+02 0.2554E+02- 0.2554E+02	1.005000 2.002724 3.002424 3.002424 STRESS ELE 51 S2 0.5595E-02-0.26 0.5138E-02-0.26 0.2608E-01-0.11 0.1767E-02-0.12	00.399891 00.399902 00.399902 EMENT DATA \$12 \$19E+04 0.1337 593E+04 0.1271 555E+04 0.1262 359E+04 0.9381 249E+04 0.53821	1.204252 2.202771 TS SIGE E.040.00 0.548 E.040.04 0.502 E.030.02 0.357 E.030.02 0.357 E.030.02 0.202	00.399903 00.399903 SIEP 0 S 0E+04 0.3741E 1E+04 0.1620E 7E+04 0.2037E 6E+04 0.2037E 6E+04 0.2038E 6E+04 0.2038E 9E+04 0.2038E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E*08 *03 0.83965*07 *03 0.42646*07 *03 0.5210E*07 *03 0.5246E*07 *03 0.2466E*07	00.399903 00.399903 2 2 0.3152E+10 0.177+E+10 0.1174E+10 0.1772E+09 0.5356E+09
2.002480 1.603397 2.602553 SAMPLE PROB NEL IRV 1 1-0.261 2 1-0.259 3 1-0.155 4 1-0.155 5 1-0.124 6 1-0.117 7 1-0.820	00.194951 00.399903 00.399903 BLEM 3 EXPANS SR ST 9E+04 0.3685E+ 10E+04 0.3191E+ 10E+04 0.3191E+ 10E+04 0.215E+ 10E+04 0.215E+ 10E+04 0.1940E+ 10E+03 0.1610E+	3.002422 1.803136 2.802478 ION OF A INIC SZ 04-0.5471E+02 04-0.5206E+02 04-0.1259E+02 04-0.1459E+02 04-0.1447E+02	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02- -0.2564E+02 -0.2564E+02 -0.2564E+02 -0.2574E+02	1.005000 2.002424 3.002424 STRESS ELE 51 S2 0.5595E+02-0.25 0.5138E+02-0.25 0.2008E+01-0.16 0.1767E+02-0.17 0.1911E+02-0.17	00.399891 00.399902 00.399902 EMENT DATA 512 5196+04 0.1337 5936+04 0.1271 5556-04 0.9361 2496-04 0.9361 2496-04 0.5321 1126-03 0.4073	TS SIGE  E+040.00 0.548 E+040.04 0.502 E+030.02 0.357 E+030.02 0.272 E+030.02 0.272 E+030.02 0.272	00.399903 00.399903 SIEP 0 S 0E+04 0.3741E 1E+04 0.1420E 7E+04 0.2037E 6+04 0.2037E 3E+04 0.2952E 9E+04 0.2952E 3E+04 0.2056E	1.+03775 2.402645 1	00.399903 00.399903 2 0.3152E+10 0.147+E+10 0.1114E+10 0.7772E+09 0.6358E+09 0.3961E+09
2.602480 1.603397 2.602553 SAMPLE PROB NEL 1RV 1 1-0.261 2 1-0.259 3 1-0.155 4 1-0.177 7 1-0.826 8 1-0.888	00.194951 00.399903 00.399903 ILEM 3 EXPANS SR ST 9E+04 0.3685E+ 10E+04 0.3191E+ 10E+04 0.3191E+ 10E+04 0.215E+ 10E+04 0.215E+ 10E+04 0.11940E+ 10E+04 0.11960E+ 10E+04 0.11960E+ 10E+03 0.1172E+ 10E+03 0.172E+	3.002422 1.803136 2.802473 ION OF A THIC SZ 04 0.5595E+02 04-0.547IE+02 04-0.3205E+01 04-0.1440E+02 04-0.1447E+02 04-0.417E+02 04-0.417E+02	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.4198E+02- 0.2564E+02- 0.2564E+02- 0.2564E+02- 0.2512E+02- 0.2512E+02- 0.2554E+02	1.005000 2.002724 3.002424 STRESS ELE S1 S2 0.5595E+02-0.26 0.5130E+02-0.26 0.2608E+01-0.16 0.1767E+02-0.16 0.1911E+02-0.17 0.1393E+02-0.17	00.399891 00.399902 00.399902 EMENT DATA S12 519E-04 0.1337 593E-04 0.8262 559E-04 0.9381 249E-04 0.5340 176E-04 0.5340 176E-04 0.5421 212E-03 0.4073	TS SIGE  E-040.00 0.546 E-040.04 0.502 E-030.02 0.357 E-030.04 0.395 E-030.02 0.272 E-030.02 0.272 E-030.02 0.272 E-030.03 0.20	00.399903 00.399903 SIEP 0 S 0E-04 0.3741E 1E-04 0.2037E 6E-04 0.2037E 6E-04 0.203E 9E-04 0.243E 9E-04 0.243E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E •08 *03 0.8396E •07 *03 0.4264E •07 *03 0.5210E •07 *03 0.2461E •07 *03 0.2461E •07 *03 0.1530E •07 *03 0.1530E •07	00.399903 00.399903 2 2 0.3152E+10 0.1174E+10 0.1174E+10 0.1374E+10 0.556E+09 0.5772E+09 0.596E+09 0.406E+09
2.002480 1.603397 2.602553 SAMPLE PROB NEL IRV 1 1-0.261 2 1-0.299 3 1-0.155 4 1-0.177 7 1-0.826 8 1-0.898 9 1-0.624	00.194951 00.399903 00.399903 ILEM 3 EXPANS: SR ST	3.002422 1.803136 2.802478 ION OF A INIC 5Z 04 0.5595E+02 04-0.5471E+02 04-0.3406E+01 04-0.1440E+02 04-0.1459E+02 04-0.417E+01 04-0.417E+01 04-0.417E+01	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02- 0.7527E+02 -0.7527E+02 -0.2554E+02- 0.2512E+02- -0.1497E+02- 0.2559E+02- 0.1497E+02-	1.005000 2.002724 3.002424 3.002424 5TRESS ELE 51 S2 0.5595E+02-0.26 0.5138E+02-0.16 0.1767E+02-0.16 0.1911E+02-0.16 0.193E+02-0.16 0.77775E+01-0.66 0.77775E+01-0.66	00.399891 00.399902 00.399902 EMENT DATA 512 519E+04 0.1337 593E+04 0.1271 555E+04 0.9361 247E+04 0.5342 178E+04 0.5342 178E+04 0.5342 178E+04 0.5421 212E+03 0.4073 194E+03 0.3454	1.204252 2.202771 TS SIGE E.040.00 0.548 E.040.04 0.502 E.030.02 0.357 E.030.02 0.357 E.030.02 0.272 E.030.02 0.272 E.030.03 0.229 E.030.03 0.229 E.030.03 0.229	00.399908 00.399903 SIEP 0 S 0E+04 0.3741E 1E+04 0.1020E 7E+04 0.2037E 6E+04 0.203E 6E+04 0.203E 6E+04 0.203E 6E+04 0.203E 6E+04 0.203E 6E+04 0.203E 6E+04 0.203E	1.403775 2.402645  1	00.399903 00.399903 2 2 0.3152E+10 0.177+E+10 0.1175E+10 0.1772E+01 0.7772E+01 0.5356E+01 0.3901E+01 0.406E+01 0.2901E+01
2.002480 1.603397 2.602553 SAMPLE PROB NEL IRV 1 1-0.259 3 1-0.155 5 1-0.124 6 1-0.117 7 1-0.820 8 1-0.828 9 1-0.624 10 1-0.502	00.194951 00.399303 00.399303 ILEM 3 EXPANS  SR ST	3.002422 1.803133 2.802473 ION OF A INIC SZ 04-0.5471E-02 04-0.5471E-02 04-0.3206E-01 04-0.1440E-02 04-0.1447E-02 04-0.7045E-01 04-0.5490E-01 04-0.5490E-01	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.9198E+02- 0.2564E+02- 0.7527E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.1194E+02-	1.005000 2.002724 3.002424 STRESS ELE 51 S2 0.5595E+02-0.29 0.5138E+02-0.29 0.2008E+01-0.19 0.1716-02-0.19 0.1911E+02-0.19 0.1911E+02-0.19 0.1925+01-0.89 0.7775E+01-0.89	00.399891 00.399902 00.399902 EMENT DATA 512 519E+04 0.1337 593E+04 0.1271 555E+04 0.936 178E+04 0.936 178E+04 0.5821 12E+03 0.4485 12E+03 0.4485 14E+03 0.4485	1.204252 2.202771 TS SIGE E+040.00 0.548 E+040.04 0.502 E+030.02 0.357 E+030.02 0.294 E+030.02 0.274 E+030.03 0.229 E+030.03 0.214 E+030.03 0.229 E+030.03 0.214	00.399908 00.399903 SIEP 0 S 0E+04 0.3741E 1E+04 0.2037E 6E+04 0.2037E 6E+04 0.2038E 9E+04 0.2038E 9E+04 0.2038 9E+04 0.2038 9E+04 0.2038 9E+04 0.2038	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E*08 *03 0.4396E*07 *03 0.4264E*07 *03 0.5210E*07 *03 0.1530E*07 *03 0.1700E*07 *03 0.1700E*07 *03 0.1137E*01	00.399903 00.399903 2 2 33 0.3152E+10 0.1474E+10 0.1474E+10 0.1374E+10 0.1374E+10 0.7772E+09 0.3901E+09 0.3901E+09 0.3901E+09 0.4006E+09 0.2901E+09 0.2901E+09
NEL IRV  1 1-0.261 2 1-0.262 3 1-0.155 4 1-0.155 5 1-0.164 6 1-0.117 7 1-0.826 8 1-0.888 9 1-0.624 10 1-0.624	00.194951 00.399903 00.399903 ILEM 3 EXPANS: SR ST 9E+04 0.3085E+( 0E+04 0.3191E+( 0E+04 0.3191E+( 0E+04 0.2415E+( 0E+04 0.2415E+( 0E+04 0.2415E+( 0E+04 0.1940E+( 0E+03 0.1610E+( 0E+03 0.172E+( 0E+03 0.172E+( 0E+03 0.172E+( 0E+03 0.172E+( 0E+03 0.172E+( 0E+03 0.172E+( 0E+03 0.172E+( 0E+03 0.172E+(	3.002422 1.803136 2.802473 ION OF A THIC SZ 04 0.5595E+02 04-0.5471E+02 04-0.1440E+02 04-0.1459E+02 04-0.147E+01 04-0.47E+01 04-0.543E+01 04-0.543E+01 04-0.543E+01	0.194951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.4198E+02- 0.7527E+02- 0.7512E+02- 0.2512E+02- 0.2512E+02- 0.2512E+02- 0.1447E+02 0.1144E+02- 0.1144E+02-	1.005000 2.002724 3.002424 3.002424 5TRESS ELE 51 S2 0.5595E-02-0.24 6.5138E+02-0.25 0.2608E+01-0.16 0.1911E+02-0.17 0.1911E+02-0.17 0.5542E+01-0.92 0.7775E-01-0.98 0.7775E-01-0.90	00.399891 00.399902 00.399902 EMENT DATA 512 5196:04 0.1337 5938:04 0.1271 5556:04 0.1271 5496:04 0.9361 746:04 0.5421 126:03 0.4073 146:03 0.4666 2446:03 0.3154 3946:03 0.4656	TS SIGE  E-040.00 0.548 E-040.04 0.502 E-030.02 0.357 E-030.02 0.294 E-030.02 0.272 E-030.02 0.272 E-030.02 0.284 E-030.02 0.184 E-030.02 0.184 E-030.02 0.184 E-030.02 0.184	00.399908 00.399903 SIEP 0 S 0E-04 0.3741E 1E-04 0.1620E 7E-04 0.2037E 6E-04 0.2037E 6E-04 0.2038E 9E-04 0.2048E 9E-04 0.2058E 9E-04 0.2058E 9E-04 0.2791E 0E-04 0.2791E 0E-04 0.2791E	1.403775 2.402645  1 - 1 0F  J2  -03 0.10016-08 +03 0.8396-07 +03 0.4266-07 +03 0.52106-07 +03 0.52106-07 +03 0.1376-07 +03 0.1376-07 +03 0.11376-07 +03 0.11376-07 +03 0.10096-07 +03 0.10096-07 +03 0.5966-07	J3  0.3152E+10 0.1774E+10 0.1774E+10 0.7772E+09 0.0556E+09 0.3901E+09 0.2901E+09 0.2901E+09 0.2901E+09 0.2901E+09
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NEL 1RV  1 1-0.261 2 1-0.259 3 1-0.155 5 1-0.17 7 1-0.826 9 1-0.624 10 1-0.502	00.199951 00.399903 00.399903 ILEM 3 EXPANS SR ST 9E+04 0.3685E+ 10E+04 0.3191E+ 10E+04 0.3191E+ 10E+04 0.215E+ 10E+04 0.215E+ 10E+04 0.1196E+ 10E+03 0.1172E+ 10E+03 0.172E+ 10E+03 0.172E+	3.002422 1.803136 2.802473 ION OF A THIC SZ 04 0.5595E+02 04-0.5205E+01 04-0.3205E+01 04-0.3205E+01 04-0.417E+02 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.4198E+02- 0.2564E+02- 0.2564E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.1194E+02- 0.1194E+02- 0.1194E+02- 0.1255E+02- 0.1255E+02- 0.1255E+02- 0.1255E+02-	1.005000 2.002924 3.002424 5TRESS ELE 51 S2 0.5595E+02-0.26 0.5130E+02-0.26 0.2008E+01-0.16 0.1715E+02-0.16 0.1393E+02-0.11 0.1393E+02-0.11 0.1393E+01-0.50 0.7775E+01-0.50 0.6770E+01-0.50 0.6770E+01-0.50 0.6770E+01-0.50	00.399891 00.399902 00.399902 EMENT DATA S12 519E-04 0.1337 593E-04 0.8262 559E-04 0.9361 249E-04 0.5340 176E-04 0.5340 176E-04 0.5340 176E-04 0.5340 176E-03 0.4073 344E-03 0.2040 177E-03 0.2040 177E-03 0.2040 177E-03 0.2040	TS SIGE  E-040.00 0.546 E-040.04 0.502 E-030.02 0.357 E-030.02 0.272 E-030.02 0.272 E-030.02 0.272 E-030.02 0.274 E-030.03 0.229 E-030.03 0.229 E-030.03 0.124 E-030.03 0.154 E-030.03 0.154	00.399908 00.399903 STEP 0 S 0E-04 0.3741E 1E-04 0.2037E 6E-04 0.203E 7E-04 0.203E 9E-04 0.203E 9E-04 0.203E 9E-04 0.203E 0E-04 0.203E 0E-04 0.203E 0E-04 0.203E 0E-04 0.203E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E •08 *03 0.8396E •07 *03 0.84264E •07 *03 0.5210E •07 *03 0.5210E •07 *03 0.1530E •07 *03 0.1137E •07 *03 0.1137E •07 *03 0.696E •00 *05 0.775ach •00 *05 0.75530E •00	00.399903 00.399903 2 2 33 0.3152E+10 0.1174E+10 0.1174E+10 0.1374E+10 0.1374E+09 0.5056E+09 0.5056E+09 0.5056E+09 0.5056E+09 0.5056E+09 0.1075E+09 0.1075E+09 0.1075E+09
NEL 1RV  1 1-0.261 2 1-0.259 3 1-0.155 5 1-0.17 7 1-0.826 9 1-0.624 10 1-0.502	00.199951 00.399903 00.399903 ILEM 3 EXPANS SR ST 9E+04 0.3685E+ 10E+04 0.3191E+ 10E+04 0.3191E+ 10E+04 0.215E+ 10E+04 0.215E+ 10E+04 0.1196E+ 10E+03 0.1172E+ 10E+03 0.172E+ 10E+03 0.172E+	3.002422 1.803136 2.802473 ION OF A THIC SZ 04 0.5595E+02 04-0.5205E+01 04-0.3205E+01 04-0.3205E+01 04-0.417E+02 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01 04-0.417E+01	00.199951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.4198E+02- 0.2564E+02- 0.2564E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.2554E+02- 0.1194E+02- 0.1194E+02- 0.1194E+02- 0.1255E+02- 0.1255E+02- 0.1255E+02- 0.1255E+02-	1.005000 2.002924 3.002424 3.002424 5TRESS ELE 51 52 0.5595E+02-0.26 0.5138E+02-0.26 0.2408E+01-0.16 0.1767E+02-0.17 0.1911E+02-0.17 0.1931E+02-0.17 0.6542E+01-0.87 0.621E+01-0.87 0.621E+01-0.87	00.399891 00.399902 00.399902 EMENT DATA S12 519E-04 0.1337 593E-04 0.8262 559E-04 0.9361 249E-04 0.5340 176E-04 0.5340 176E-04 0.5340 176E-04 0.5340 176E-03 0.4073 344E-03 0.2040 177E-03 0.2040 177E-03 0.2040 177E-03 0.2040	TS SIGE  E-040.00 0.546 E-040.04 0.502 E-030.02 0.357 E-030.02 0.272 E-030.02 0.272 E-030.02 0.272 E-030.02 0.274 E-030.03 0.229 E-030.03 0.229 E-030.03 0.124 E-030.03 0.154 E-030.03 0.154	00.399908 00.399903 STEP 0 S 0E-04 0.3741E 1E-04 0.2037E 6E-04 0.203E 7E-04 0.203E 9E-04 0.203E 9E-04 0.203E 9E-04 0.203E 0E-04 0.203E 0E-04 0.203E 0E-04 0.203E 0E-04 0.203E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E •08 *03 0.8396E •07 *03 0.84264E •07 *03 0.5210E •07 *03 0.5210E •07 *03 0.1530E •07 *03 0.1137E •07 *03 0.1137E •07 *03 0.696E •00 *05 0.775ach •00 *05 0.75530E •00	00.399903 00.399903 2 2 33 0.3152E+10 0.1174E+10 0.1174E+10 0.1374E+10 0.1374E+09 0.5056E+09 0.5056E+09 0.5056E+09 0.5056E+09 0.5056E+09 0.1075E+09 0.1075E+09 0.1075E+09
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NEL IRV  1 1-0.261 2 1-0.262 3 1-0.165 4 1-0.176 6 1-0.117 7 1-0.860 8 1-0.888 9 1-0.624 10 1-0.502 11 1-0.404 12 1-0.407 13 1-0.271 15 1-0.168	00.194951 00.399903 00.399903 ILEM 3 EXPANS  SR ST  9E+04 0.3685E+0 0.2649E+0 0.215E+0 0.215E	3.002422 1.803136 2.802473 10N OF A THIC  SZ  04 0.5595E+02 04-0.5471E+02 04-0.3206E+01 04-0.1440E+02 04-0.4671E+02 04-0.5471E+02 04-0.5471E+02 04-0.5471E+02 04-0.5471E+02 04-0.5471E+02 04-0.5471E+02 04-0.5471E+01 04-0.3769E+01 04-0.3769E+01 04-0.3769E+01 04-0.3769E+01 04-0.3760E+01 04-0.3760E+01 04-0.3760E+01	0.194951 00.399903 00.399903 K WALL TUBE SRZ 0.E+00 0.4198E+02- 0.7527E+02 0.2512E+02- 0.2512E+02- 0.1194F+02- 0.1194E+02- 0.1194E+01- 0.11285E+02 0.66742E+01- 0.6742E+01- 0.574E+01- 0.574E+01- 0.574E+01-	1.005000 2.002924 3.002424 5TRESS ELE 51 S2 0.5595E+02-0.24 6.5138E+02-0.17 0.1911E+02-0.17 0.1911E+02-0.17 0.193E+01-0.06 0.7775E+01-0.08 0.5321E+01-0.06 0.5705E+01-0.08 0.5321E+01-0.06 0.509E+01-0.09 0.509E+01-0.09 0.333E+01-0.09 0.3308E+01-0.09 0.3308E+01-0.09 0.2311E+01-0.19	00.399891 00.399902 00.399902 EMENT DATA 512 519E-04 0.1337 593E-04 0.1271 555E-04 0.8262 259E-04 0.9361 212E-03 0.4073 176E-04 0.5321 212E-03 0.4073 174E-03 0.4456 244E-03 0.3154 245E-03 0.4073 377E-03 0.2462 245E-03 0.2462	TS SIGE  E-040.00 0.546 E-040.04 0.502 E-030.02 0.357 E-030.02 0.272 E-030.02 0.272 E-030.02 0.272 E-030.02 0.174 E-030.03 0.229 E-030.03 0.128	00.399908 00.399903 SIEP  0 S  0E+04 0.3741E 1E+04 0.1420E 6E+04 0.243E 6E+04 0.243E 9E+04 0.2492E 3E+04 0.2403E 7E+04 0.2505E 6E+04 0.2505E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E*08 *03 0.8396E*07 *03 0.4264E*07 *03 0.4264E*07 *03 0.5210E*07 *03 0.2461E*07 *03 0.2461E*07 *03 0.1376E*07 *03 0.1376E*07 *03 0.77536*06 *03 0.57536*06 *03 0.57536*06 *03 0.57536*06 *03 0.57536*06 *03 0.57536*06 *03 0.57536*06 *03 0.57536*06	J3  0.3152E+10 0.3152E+10 0.3152E+10 0.1717+E+10 0.1717E+09 0.3154E+09 0.3961E+09 0.3961E+09 0.3961E+09 0.2507E+09 0.1507E+09 0.1505E+09
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NEL IRV  1 1-0.261 2 1-0.255 3 1-0.155 5 1-0.156 6 1-0.117 7 1-0.820 8 1-0.888 9 1-0.624 10 1-0.522 11 1-0.437 13 1-0.255 14 1-0.717 15 1-0.166 16 1-0.117 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 17 1-0.166 18 1-0.17 19 1-0.27 19 1-0.27	00.199951 00.399903 00.399903 ILEM 3 EXPANS  SR ST	3.002422 1.803136 2.802478 10N OF A THIC  SZ  04-0.54718-02 04-0.54718-02 04-0.32068-01 04-0.14408-02 04-0.14478-02 04-0.14478-02 04-0.418-01 04-0.408-01 04-0.408-01 04-0.408-01 04-0.408-01 04-0.408-01 04-0.408-01 04-0.308-01 04-0.308-01 04-0.308-01 04-0.308-01 04-0.308-01 03-0.20958-01 03-0.20958-01 03-0.20988-01	00.199951 00.399903 00.399903 K WALL TUBE SRZ  0.E+00 0.9198E+02- 0.2554E+02- 0.7527E+02- 0.2554E+02- 0.2554E+02- 0.1194E+02- 0.1194E+02- 0.1194E+02- 0.6024E+01- 0.125E+02- 0.6024E+01- 0.5274E+01- 0.4015E+01- 0.4015E+01-	1.005000 2.002924 3.002424 3.002424 STRESS ELE 51 S2 0.5595E+02-0.26 0.5138E+02-0.25 0.2608E+01-0.26 0.17167E+02-0.13 0.1911E+02-0.13 0.1912E+01-0.26 0.7775E+01-0.26 0.5321E+01-0.26 0.4706E+01-0.26 0.3333E+01-0.26 0.3333E+01-0.26 0.340E+01-0.26 0.340E+01-0.26 0.240E+01-0.41 0.2311E+01-0.11 0.2431E+01-0.12 0.2431E+01-0.12 0.2431E+01-0.13 0.24370E+01-0.26	00.399891 00.399902 00.399902 EMENT DATA  S12  519E+04 0.1337 593E+04 0.1271 555E+04 0.2622 159E+04 0.9380 178E+04 0.5821 122E+03 0.4486 124E+03 0.3482 124E+03 0.3482 124E+03 0.2486 125E+03 0.2486	1.204252 2.202771  TS SIGE  E+040.00 0.548 E+040.04 0.502 E+030.02 0.357 E+030.02 0.294 E+030.02 0.214 E+030.03 0.229 E+030.02 0.174 E+030.03 0.128	00.399908 00.399903 SIEP  0 S  0E+04 0.3741E 1E+04 0.207E 6E+04 0.203E 7E+04 0.203E 9E+04 0.203E 9E+04 0.203E 9E+04 0.203E 9E+04 0.203E 9E+04 0.2753E 8E+04 0.2753E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E*08 *03 0.4396E*07 *03 0.4264E*07 *03 0.5210E*07 *03 0.5210E*07 *03 0.1137E*07 *03 0.13770E*06 *03 0.5531E*00 *03 0.23770E*00 *03 0.2325*00 *03 0.2325*00 *03 0.2325*00 *03 0.2325*00	00.399903 00.399903 2 2 33 0.3152E+10 0.1474E+10
NEL 1RV  1 1-0.261 2 1-0.2553 SAMPLE PROB  NEL 1RV  1 1-0.261 2 1-0.259 3 1-0.155 4 1-0.155 6 1-0.17 7 1-0.826 9 1-0.624 10 1-0.528 11 1-0.464 12 1-0.452 14 1-0.271 15 1-0.166 16 1-0.17 17 1-0.166 16 1-0.17 17 1-0.166 18 1-0.295 14 1-0.272 15 1-0.166 16 1-0.17 17 1-0.166 18 1-0.17 17 1-0.166 19 1-0.273	00.199951 00.399903 00.399903 ILEM 3 EXPANS  SR ST  9E+04 0.3685E+ 05E+04 0.3191E+ 05E+04 0.3191E+ 05E+04 0.3191E+ 05E+04 0.3191E+ 05E+04 0.7245E+ 05E+04 0.7245E+ 05E+04 0.1792E+ 05E+03 0.1610E+ 07E+03 0.1792E+ 07E+03 0.17	3.002422 1.803136 2.802473 10N OF A THIC  SZ  04 0.5595E+02 04-0.5471E+02 04-0.5471E+02 04-0.3206E+01 04-0.447E+02 04-0.447E+02 04-0.447E+02 04-0.447E+01	00.199951 00.399903 00.399903 K WALL TUBE  SRZ  0.E+00 0.4198E+02- 0.7527E+02- 0.2534E+02- 0.1194E+02- 0.1194E+02- 0.1194E+02- 0.1194E+02- 0.1624E+01- 0.1225E+02 0.15274E+01- 0.5274E+01- 0.6274E+01- 0.6274E+01- 0.6274E+01- 0.6274E+01- 0.6317E+01- 0.4213E+01- 0.4213E+01- 0.4213E+01- 0.4213E+01- 0.4213E+01- 0.4213E+01- 0.4213E+01- 0.4213E+01- 0.4213E+01-	1.005000 2.002924 3.002424 5.002424 5.002424 5.102424 5.102424 5.102424 5.102424 6.5138E.02-0.25 6.5138E.02-0.25 6.5138E.02-0.25 6.2608E.01-0.16 6.1705E.01-0.19 6.5042E.01-0.26 6.5042E.01-0.	00.399891 00.399902 00.399902 EMENT DATA  S12 519E-04 0.1337 955E-04 0.1271 955E-04 0.1271 955E-04 0.5321 112E-03 0.4073 94E-03 0.4073 94E-03 0.4456 94E-03 0.2466 94E-03 0.2466 94E-03 0.2526 94E-03 0.5246 94E-03 0.5246 94E-03 0.5246 94E-03 0.5246 95E-03 0.5246	TS SIGE  E-040.00 0.546 E-040.00 0.546 E-040.00 0.546 E-030.02 0.357 E-030.02 0.272 E-030.02 0.272 E-030.02 0.272 E-030.02 0.174 E-030.03 0.122 E-030.03 0.128	00.399908 00.399903 SIEP  0 S  0E-04 0.3741E 7E-04 0.1620E 7E-04 0.2037E 6E-04 0.2038 7E-04 0.2048 7E-04 0.2048 7E-04 0.2058	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E •08 *03 0.8396E •07 *03 0.8396E •07 *03 0.5210E •07 *03 0.5210E •07 *03 0.5210E •07 *03 0.1376E •07 *03 0.1376E •07 *03 0.1377E •06 *03 0.3770E •06 *03 0.3770E •06 *03 0.349E •06 *03 0.349E •06 *03 0.337E •06 *03 0.337E •06 *03 0.337E •06 *03 0.2337E •06 *0	00.399903 00.399903 2 2 0.3152E+10 0.3152E+10 0.1774E+10 0.1774E+10 0.1374E+10 0.1374E+10 0.4046E+09 0.3961E+09 0.3961E+09 0.207E+09 0.207E+09 0.1306E+09 0.326E+08 0.326E+08
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NEL IRV  1 1-0.261 2 1-0.255 SAMPLE PROB  NEL IRV  1 1-0.261 2 1-0.256 3 1-0.155 6 1-0.17 7 1-0.826 8 1-0.124 6 1-0.17 7 1-0.826 10 1-0.582 11 1-0.404 12 1-0.437 13 1-0.271 15 1-0.168 16 1-0.17 17 1-0.102 16 1-0.17 17 1-0.102 18 1-0.271 20 1-0.374 21 1-0.271 22 1-0.258 23 1-0.155 24 1-0.155	00.199951 00.399903 00.399903 00.399903 00.399903 00.399903 00.899606 SR ST  9E+04 0.3085E+0 0.8495E+0 0.8485E+0 0.8	3.002422 1.803136 2.802473 10N OF A THIC  SZ  04 0.5595E+02 04-0.5471E+02 04-0.5471E+02 04-0.1440E+02 04-0.1447E+01 04-0.4571E+01 03-0.4571E+01 03-0.4571E+01 03-0.4571E+01 03-0.4571E+01 03-0.4571E+01 03-0.4571E+01 03-0.4571E+01 03-0.4571E+01	0.194951 00.399903 00.399903 K WALL TUBE  SRZ  0.E+00 0.4198E+02- 0.254E+02- 0.2512E+02- 0.2512E+02- 0.2512E+02- 0.2512E+02- 0.1497E+02 0.1194E+02- 0.1497E+02 0.1194E+01- 0.5274E+01- 0.5274E+01- 0.5274E+01- 0.6674E+01- 0.674E+01- 0.476E+01- 0.4776E+01- 0.4776E-01- 0.	1.005000 2.002924 3.002424 STRESS ELE S1 S2 0.5595E+02-0.24 0.5595E+02-0.25 0.2008E+01-0.16 0.1767E+02-0.17 0.1911E+02-0.17 0.1932E+01-0.20 0.7775E+01-0.20 0.333E+01-0.26 0.309E+01-0.40 0.333E+01-0.26 0.335E+01-0.36 0.335E+01-0.36	00.399891 00.399902 00.399902 EMENT DATA  \$12  \$19E+04 0.1337 \$93E+04 0.1271 \$55E+04 0.1271 \$12E+03 0.4070 \$14E+04 0.5421 \$12E+03 0.4073 \$14E+04 0.4460 \$17E+03 0.2960 \$17E+03 0.2960 \$17E+03 0.1496 \$17E+03 0.2960 \$12E+03 0.4960 \$17E+03 0.2960 \$12E+03 0.4960	TS SIGE  E-040.00 0.548 E-040.04 0.502 E-030.02 0.377 E-030.04 0.392 E-030.02 0.294 E-030.02 0.294 E-030.03 0.299 E-030.03 0.292 E-030.03 0.128 E-030.03 0.138	00.399908 00.379903 SIEP  0 S  0E-04 0.3741E 1E-04 0.1420E 1E-04 0.243E 6E-04 0.243E 9E-04 0.243E 9E-04 0.249E 3E-04 0.263E 9E-04 0.263E 9E-04 0.263E 9E-04 0.263E 9E-04 0.273E 8E-04 0.274E 9E-04 0.274E 9E-03 0.274E 9E-04 0.274E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E*08 *03 0.3706E*07 *03 0.4396E*07 *03 0.5210E*07 *03 0.5210E*07 *03 0.5210E*07 *03 0.5210E*07 *03 0.1376E*07 *03 0.5530E*00 *03 0.5530E*00 *03 0.5531E*00 *03 0.5531E*00 *03 0.5531E*00 *03 0.5531E*00 *03 0.3772E*00 *03 0.372E*00 *03 0.372E*00 *03 0.372E*00 *03 0.372E*00 *03 0.492E*00 *03 0.2496E*00 *03 0.496E*00	J3  0.3152E+10 0.1774E+10 0.1774E+10 0.1772E+09 0.3761E+09
NEL IRV  1 1-0.261 2 1-0.255 3 3 1-0.155 5 1-0.124 6 1-0.117 7 1-0.820 8 1-0.888 9 1-0.624 10 1-0.522 11 1-0.437 13 1-0.255 14 1-0.271 15 1-0.166 16 1-0.17 17 1-0.162 16 1-0.17 17 1-0.162 16 1-0.17 17 1-0.162 18 1-0.27 18 1-0.27 19 1-0.27 19 1-0.27 19 1-0.27 19 1-0.27 20 1-0.367 21 1-0.25 22 1-0.25 23 1-0.155 24 1-0.155 25 1-0.155	00.199951 00.399903 00.399903 ILEM 3 EXPANS  SR ST	3.002422 1.803136 2.802478 10N OF A THIC  SZ  04 0.5595E+02 04-0.5471E+02 04-0.3205E+01 04-0.1440E+02 04-0.1447E+02 04-0.447E+02 04-0.4176-01 04-0.47045E+01 04-0.47045E+01 04-0.47045E+01 04-0.47045E+01 04-0.47045E+01 04-0.47045E+01 04-0.47045E+01 03-0.2055E+01	00.199951 00.399903 00.399903 K WALL TUBE SRZ  0.E+00 0.9198E+02- 0.2554E+02- 0.7527E+02- 0.2554E+02- 0.2554E+02- 0.1194E+02- 0.1194E+02- 0.1194E+02- 0.6624E+01 0.16742E+01 0.16742E+01 0.5274E+01- 0.5274E+01- 0.5274E+01- 0.5274E+01- 0.5274E+01- 0.5274E+01- 0.5274E+01- 0.5274E+01- 0.9262E+02- 0.1712E+02-	1.005000 2.002924 3.002424 5.002424 5.002424 5.102424 5.102424 5.102424 6.5138E+02-0.25 6.5138E+02-0.12 6.1912E+02-0.12 6.1932E+01-0.25 6.5042E+01-0.25 6.50441E+01-0.44 6.5043E+01-0.25 6.5045E+01-0.25 6.5045E+01-0.25 6.5045E+01-0.25 6.5045E+01-0.35 6.504	00.399891 00.399902 00.399902 EMENT DATA  \$12  \$12  \$19E+04 0.1337 593E+04 0.1271 555E+04 0.2626 159E+04 0.9366 178E+04 0.5821 122E+03 0.4456 124E+03 0.4456 124E+03 0.2466 125E+03 0.2466 125E+04 0.4260	1.204252 2.202771  TS SIGE  E+040.00 0.548 E+040.00 0.548 E+040.00 0.598 E+030.02 0.357 E+030.02 0.294 E+030.02 0.174 E+030.03 0.128 E+030.03 0.502 E+030.03 0.502 E+030.04 0.502 E+030.04 0.502	00.399908 00.399903 SIEP  0 S  0E+04 0.3741E 1E+04 0.3741E 1E+04 0.2037E 6E+04 0.2037E 6E+04 0.2038 3E+04 0.2738	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E*08 *03 0.4396E*07 *03 0.4264E*07 *03 0.5210E*07 *03 0.5210E*07 *03 0.1137E*07 *03 0.1376E*07 *03 0.150E*07 *03 0.13770E*06 *03 0.5531E*00 *03 0.5531E*00 *03 0.5531E*00 *03 0.33770E*06 *03 0.33770E*06 *03 0.33770E*06 *03 0.33770E*06 *03 0.33770E*06 *03 0.49428*07 *03 0.4948*06 *04 0.4948*07 *05 0.4948*07 *07 0.4948*07 *08 0.4948*07 *09 0.4948*07 *09 0.4948*07 *09 0.4948*07	00.399903 00.399903 2 2 33 0.3152E+10 0.1374E+10 0.1374E+10 0.1374E+10 0.1374E+10 0.1374E+10 0.3961E-09 0.3961E-09 0.3961E-09 0.3961E-09 0.1306E-09 0.1306E-09 0.1306E-09 0.1306E-09 0.1306E-09 0.14074E-09 0.14074E-10 0.14074E-10
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*03 0.420E 07 *03 0.1326E 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 07 *03 0.11376 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00.4198E+02-0.2564E+02-0.2564E+02-0.2564E+02-0.2564E+01-0.2574E+01-0.2574E+01-0.3762E+01-0.3762E+01-0.3762E+01-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762E+02-0.3762	1.005000 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TS SIGE  E-040.00 0.546 E-040.00 0.546 E-030.02 0.357 E-030.02 0.272 E-030.02 0.272 E-030.02 0.174 E-030.03 0.126	00.399908 00.399903 STEP  0 S  0E-04 0.3741E 7E-04 0.1620E 7E-04 0.203E	1.403775 2.402645  1 - 1 0F  J2  *03 0.1001E •08 *03 0.8396E •07 *03 0.8396E •07 *03 0.5210E •07 *03 0.5210E •07 *03 0.5210E •07 *03 0.1009E •08 *04 0.1530E •07 *05 0.1530E •07 *05 0.1530E •06 *05 0.7750E •06 *06 0.7750E •06 *07 0.750E •06 *08 0.750E •06 *09 0.750E •07 *09 0.75	00.399903 00.399903 2 33 0.3152E+10 0.3152E+10 0.1774E+10 0.2076E+09 0.2076E+09 0.2076E+09 0.2076E+09 0.2076E+09 0.2076E+09 0.2076E+09 0.320E+09 0.1157E+09 0.4076E+08 0.4342E+08 0.4342E+10 0.1344E+10 0.1344E+10 0.1345E+10 0.1345E+10 0.1345E+10 0.1345E+10 0.1345E+10 0.1546E+09 0.3456E+09 0.3456E+0
NEL IRV  1 1-0.261 2 1-0.259 3 1-0.155 5 1-0.166 6 1-0.117 7 1-0.820 8 1-0.888 9 1-0.682 10 1-0.592 11 1-0.437 13 1-0.295 14 1-0.271 15 1-0.166 16 1-0.17 17 1-0.162 18 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 19 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820 20 1-0.820	00.199951 00.399903 00.399903 ILEM 3 EXPANS:  SR ST	3.002422 1.803136 2.802478 10N OF A THIC  SZ  04 0.5595E+02 04-0.3205E+01 14-00.3205E+01 14-0.3205E+01 13-0.3205E+01 13-0.3205E+	00.199951 00.399903 00.399903 00.399903 00.399903 00.399903 00.49986+02- 00.491986+02- 00.25546+02- 00.76276+02- 00.25546+02- 00.11946+02- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01- 00.4046+01-	1.005000 2.002924 3.002424 5.002424 5.002424 5.102424 5.102424 5.102424 5.102424 6.5138E.02-0.25 6.5138E.02-0.25 6.5138E.02-0.25 6.5138E.02-0.25 6.2608E.01-0.16 6.1715E.01-0.19 6.1393E.02-0.11 6.1393E.02-0.11 6.1393E.02-0.11 6.1393E.02-0.11 6.1393E.01-0.25 6.406E.01-0.56 6.406E.01-0.56 6.2411E.01-0.46 6.3313E.01-0.26 6.2411E.01-0.46 6.2311E.01-0.47 6.2431E.01-0.47	00.399891 00.399902 00.399902 EMENT DATA  S12  519E+04 0.1337 593E+04 0.1327 593E+04 0.8262 159E+04 0.8262 159E+04 0.5821 12E+03 0.4676 14E+03 0.4666 14E+03 0.2966 17E+03 0.1496	1.204252 2.202771  TS SIGE  E+040.00 0.548 E+040.00 0.548 E+040.00 0.598 E+030.02 0.357 E+030.02 0.294 E+030.03 0.229 E+030.02 0.148 E+030.03 0.128 E+030.03 0.108	00.399908 00.399908 00.399908 SIEP  0 S  0E+04 0.3741E 1E+04 0.18206 7E+04 0.2037E 6E+04 0.2031E 9E+04 0.2032E	1.403775 2.402645  1 1 0F  J2  *03 0.1001E*08 *03 0.4396E*07 *03 0.4264E*07 *03 0.5210E*07 *03 0.5210E*07 *03 0.1760E*07 *03 0.1760E*07 *03 0.1776E*06 *03 0.5031E*00 *03 0.7776E*06 *03 0.37776E*06 *03 0.3776E*06 *03 0.3776E*06 *03 0.3776E*06 *03 0.3776E*06 *03 0.397E*06 *03 0.293E*06 *03 0.397E*06 *03 0.2946E*07 *03 0.1002E*07 *03 0.1004E*07 *03 0.1004E*07 *03 0.1004E*07 *03 0.1137E*07 *03 0.1137E*07 *03 0.1137E*07	00.399903  00.399903  2  0.3152E+10 0.1374E+10 0.1174E+10 0.1174E+10 0.1374E+10 0.1374E+10 0.3958E+09 0.3961E+09 0.3961E+09 0.3961E+09 0.1306E+09 0.1306E+09 0.1306E+09 0.1316E+08 0.7172E+08 0.7172E+09 0.7174E+09

### TABLE VI. - Continued. SAMPLE PROBLEM (3) - OUTPUT

34 1-0.271nf+0.0 0.10nvf+04-0.3v54E+01-0.6dr1E+01-0.3774E+01-0.2718E+03 0.1340E+030.03 0.1229E+04 0.2644E+03 0.5031E+06 0.1157E+04 35 1-0.1674E+03 0.464E+03-0.2521E+01 0.5701E+01-0.2325E+01-0.1681E+03 0.8240E+020.03 0.1063E+04 0.2660E+03 0.3769E+06 0.8184E+08 36 1-0.1476:03 0.1004:00 0.148/2:01-0.66812:01 0.21182:01-0.14742:03 0.44442:020.04 0.11042:06 0.27282:03 0.41022:06 0.412242:08 0.412242:08 0.412242:08 0.412242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 0.41242:08 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00.00 0.00000 3.12 -0.00 00.13330 -0.00141 0.00 00.00 00.00 0.00000 3.12 1.86973 00.06665 -0.00106 00.00 0.00000 -0.00 2.13615 00.03665 -0.00099 2.13615 00.03665 -0.00076 2.00954 00.13330 -0.00082 00.00 0.00000 0.00 00.00 3.12 -0.00 2.00974 00.00 0.00000 0.00 00.00 2.26939 00.06665 -0.00063 00.13330 -0.0005+ 3.11 -0.00 13 13 2.33602 0.00 00.00 00-00 0-00000 00.0665 -0.08046 3.11 -0.00 00.00 0.00000 2.53542 2.46926 0.00 00.00 00.00 -0.00000 0.00095.-0.00024 -0.00001 0.9946 0.9998 0.00091 -0.00024 0.00001 0.9946 0.9998 1.0009 0.9998 00.00 0.00000 00.0665 -0.0003A 0.9995 -0.00 2.65919 3.09 7 1504 0.00 00.06665 -0.00027 00.13330 -0.00024 00.33325 -0.00376 2.96 0.00 00.00 0.00000 00.00 0.00000 20 2.86913 00.00 20 \_\_\_00.00 00.00 U.00JJO 00.00 0.00JJO 00.00 0.00JJO 1.13785 00.26660 -0.00355 22 3.11 -0.00 ZŹ 1.33726 00.33325 -0.0023+ 1.27077 00.26660 -0.0026H 00.00 3.10 -0.00 -0.00 25 1.47031 00.33325 -0.00189 0.00 00.00 0.00000 00.26660 -0.00176 00.33325 -0.00131 00.26660 -0.00141 00.33325 -0.00107 00.26660 -0.00049 00.00 0,00000 26 1.53636 3.12 20 \_\_00.00 1.73655 0.00 00.00 0.00030 00.00 0.00030 00.00 0.00030 28 1.66998 3.11 -0.00 23 1.93633 0.00 00.00 -0.00 3.12 30 2.13615 00.33325 -0.00076 2.06954 00.26660 -0.00082 0.00132 -0.00024 0.00001 0.9992 0.9998 0.00139 -0.00024 -0.0002 0.9998 1.0013 0.9998 0.9992 00.00 0.00000 0.00 00.00 32 3.12 -0.00 2.26939 00.33325 -0.00063 2.33632 00.26660 -0.00059 0.00120 -0.00024 0.00001 0.9994 0.9998 1.0012 0.9998 0.9994 0.00115 -0.00024 -0.00001 0.9994 0.9998 1.0012 0.9998 0.9994 0.00 00.00 0.00000 00.00 34 3.12 -0.00 2.53592 00.33325 -0.00046 2.46928 00.26660 -0.00049 0.00102 -0.00024 0.00001 0.9995 0.9998 1.0010 0.9998 0.9995 0.00106 -0.00024 -0.00001 0.9995 0.9998 1.0011 0.9998 0.9995 0.00 00.00 00.00\_0.00000 35 36 00.00 0.00000 Зь. 3.11 -0.00 2.56919 00.33325 -0.00038 0.00095 -0.00024 0.00001 0.9996 0.9998 1.0009 0.9998 0.9995 2.3557 00.33325 -0.00027 0.00018 -0.00024 0.00001 0.9996 0.9998 1.0009 0.9998 0.9995 2.3557 00.33325 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TABLE VI. - Continued SAMPLE PROBLEM (3) - OUTPUT

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0.00526424 0.00526424	0.0000				46546		000000 008761		0.00000000 00007511	0.0045		.00000000	0.00443668	0.0000000 00007942
0.00565014	0000	8057		0.005	27785	000	008185	0.00497118	0000H273	0.0047	024	19660000	0.00455747	00003475
0.00443697 0.00615074	0000				33064 663333		008405 016090		00017533 00016364	0.0077		00014560	0.00685741 0.00474070	0001565/ 0001o753
0.00457041					45455		11/055	0.00433108	00016972					
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0.00234574	0.0000	0000		0.002	51147	0.000	00000	0.00510140	0.00000000	0.0020	2294 0.	,00000000	0.00145918	0.0000000
C.00191424 U.00252194	0.0000				34806		)03482 )03313		00002812 00003415	0.0030		00002956	0.0027686→ 0.002017Q4	+.00003081 00003624
0.00175714	0000	3641		0.001	90874	000	003530	0.00414392	00000634	0.0034	9543 <u>-</u> ,	00005361	0.00303460	00005744
0.00275382	0000				52705 95155		)06370 )0730 <i>1</i>		00006617	0.00220	1642 -	,00006805	0.00204543	00007032
		31.0						INCREMENTAL	FORCES					3.0
1684.7		21.9 00.5	-		-0.0		59.8 4.6		-6.5 3.4		0.0 -0.0	3.1 3.1	-0.0 -0.0	3.0 -8.1
00.0		41.0		3	763.0		-0.0	-0.0	-0.0	•	0.0	-0.0	00.0	-0.0
00.0		-0.0		•	00.0		00.0		-0.0		0.0	-0.0	0.0	-0.0
00.0		~0.0 ~			00.0		-0.0		-0.0		0.0	-0.0	00.0	00.0
00.0		-0.0			00.0	·- ·	00.0	TOTAL	FORCES					
3602.0		59.4			-0.0		108.7	0.0	-18.8 1.9		0.0	2.4	-0.0	4.7 -7.3
00.0		42.1		8	045.0		-0.0		-0.0		0.0	00.0	00.0	-0.0
00.0		-0.0			0.0		-0.0	00.0 3685.5	00.0 -0.0		0.0	-0.0 -0.0	-0.0	-0.0
- 00.0		-0.0			00.0		0.0	00.0	-0.0		0.0	-0.0		. 00.0
00.0		-0.0			00.0		00.0	00.0	COORDINATES				<del></del>	
1,009144	0.00				07757		00000	1.406864	0.000000	1.606		0.000000	1.805668	0.000000
2.005269 3.004336	0.00				04983 09144		00000 199912		0.000000 00.199925	2.604		0.000000	2.804437 1.600179	0.000000
1.805650	00.19				05278	00.1	94918	2.204971	00.199917	2.404	750 0	0.199916	2.60+567	60.199915
2.804437	00.19				04331 05663		199839 199916		00.399825_ 00.399836	1.207 2.204	747 C	0.399854	1.40od59 2.404741	00.399843 00.399832
2.604570	00.39	9831		2.8	04429	00.3	199830	3.004331	00.399830					
SAMPLE PROB	SLEM. 3	FXPAN	15 I O I	M OF	A THIC	K WALL	. TUHE					STEP	2 - 1 OF	7 2
		CAT A							MENT DATA				2 - 10	_
				-				STRESS ELE	MENT DATA					
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	<u> </u>	s1			SZ	\$RZ	·	STRESS ELE	215			5	JS .	J3
1 2-0.491	3E+94 0	S1	•04	0.84	52 53E+02	SR2	0	\$1 \$2 0.8853E+02-0.45	\$12 18E+04 0.2503	E+040.00 (	.1007E+	05 0.6146	J2 E+03 0.3386E+08	J3 5 0.1764E+11
1 2-0.491 2 1-0.487 3 1-0.314	3E+04 0	51 ,66748 ,57648	+04	0.88 -0.11 -0.10	52 53E+02 00E+03 98E+02	SR2	0 0 0E+03	51 52 0.8853E+02-0.49 -0.1041E+03-0.48 -0.1002E+02-0.31	\$12 18E+04 0.2503 85E+04 0.2340 49E+04 0.1570	8E+040.00 0 E+040.03 0 E+040.02 0	.1007E+	5 05 0.6146 04 0.25d5	J2 E+03 0.3386E+08 E+03 0.2842E+08 E+03 0.1442E+08	J3 5 0.1704E+11 5 0.1042t+11 5 0.0088E+10
1 2-0.491 2 1-0.487 3 1-0.314 4 1-0.352	3E+04 0 4E+04 0 6E+04 0	51 ,6674E ,5764E ,4409E	+04 +04- +04-	0.88 -0.11 -0.10 0.19	52 53E+02 00E+03 98E+02 78E+02	SR2	00 0E+03 7E+02	\$1 \$2 0.8853E+02-0.45 -0.1041E+03-0.46 -0.1002E+02-0.31 0.2511E+02-0.3	\$12 18E+04 0,2503 85E+04 0,2390 49E+04 0,1570 29E+04 0,1777	8E+040.00 0 1E+040.03 0 1E+040.02 0 1E+040.04 0	.1007E+ .9239E+ .6577E+	5 05 0.6146 04 0.25d5 04 0.4167 04 0.4459	J2 E+03 0.338GE+0a b+03 0.2842E+0a E+03 0.1763E+0a E+03 0.1763E+0a	J3 5 0.1764E+11 5 0.104Zt+11 5 0.768E+10 5 0.7434E+10
1 2-0.491 2 1-0.497 3 1-0.314 4 1-0.352 5 1-0.236 6 1-0.225	3E+04 0 3E+04 0 3E+04 0 3E+04 0 7E+34 0 5E+04 0	57646 57646 44096 48416 38036	•04 •04 •04 •04 •04	0.88 -0.11 -0.10 0.19 0.35	52 53E+02 00E+03 98E+02 78E+02 28E+02 22E+02	SRZ 0.E+0 0.167 -0.544 0.137 -0.544 0.330	00 00E+03 07E+02 05E+03 05E+02	\$1RESS ELE \$1 \$2 0.8853E+02-0.45 -0.1041E+03-0.46 -0.1002E+0c-0.31 0.2511E+02-0.32 0.3653E+02-0.23 -0.2957E+02-0.23	\$12 18E+04 0.2503 85E+04 0.2340 49E+04 0.1570 29E+04 0.1777 8HE+04 0.1212 56E+04 0.1113	BE+040.00 0 BE+040.03 0 BE+040.02 0 BE+040.04 0 BE+040.02 0 BE+040.02 0	.1007E+ .9239E+ .6577E+ .7276E+ .5403E+	5 05 0.6146 04 0.2585 04 0.4167 04 0.4459 04 0.4836 04 0.3976	J2 E+03 0.3386E+06 E+03 0.2842E+06 E+03 0.1763E+06 E+03 0.1763E+06 E+03 0.9729E+06	J3  5 0.1704E+11  1 0.104Ze+11  5 0.208E+10  5 0.434E+10  0.427E+10  0.3496E+10
1 2-0.491 2 1-0.487 3 1-0.314 4 1-0.352 5 1-0.236 6 1-0.252 7 1-0.158	3E+04 0 3E+04 0 3E+04 0 3E+04 0 3F+04 0 3F+04 0	51 .66748 .57648 .44098 .48418 .38038 .34788	+04 +04- +04 +04 +04-	0.88 -0.11 -0.10 -0.19 0.35 -0.30	52 53E+02 00E+03 98E+02 78E+02 28E+02 22E+02 24E+02	\$R2 0.E+0 0.167 -0.544 0.137 -0.544 0.380	00 00E+03 7E+03 5E+03 15E+02 11E+02	\$1 \$2 0.8853E+02-0.45 -0.1041E+03-0.46 -0.1002E+02-0.31 0.2511E+02-0.35 0.3653E+02-0.22	\$12 118F+04 0.2503 85E+04 0.2390 29E+04 0.1777 88E+04 0.1712 56E+04 0.1113 89E+04 0.7466	BE+040.00 C E+040.03 C E+040.02 C E+040.02 C E+040.02 C E+040.02 C	.1007E+ .9239E+ .6577E+ .7276E+ .5403E+ .5007E+	5 05 0.6146 04 0.2565 04 0.4167 04 0.4459 04 0.3976 04 0.4242	J2 E+03 0.3386E+08 E+03 0.2842E+08 E+03 0.1442E+08 E+03 0.1763E+08 E+03 0.452E+07 E+03 0.452E+07	J3 3 0.1704E+11 3 0.104Zt+11 3 0.2088E+10 9 0.424SE+10 7 0.424SE+10 0.2173E+10
1 2-0.441 2 1-0.467 3 1-0.314 4 1-0.355 5 1-0.236 6 1-0.225 7 1-0.158 8 1-0.171 9 1-0.121	3E+04 0 9E+04 0 05E+04 0 3E+04 0 17E+04 0 06E+04 0 4E+04 0 2E+04 0	51 .66748 .57648 .44098 .48418 .38788 .34788 .30348	+04 +04 +04 +04 +04 +04 +04	0.88 -0.11 -0.10 0.19 0.35 -0.30 -0.13 0.13	53E+02 00E+03 98E+02 78E+02 28E+02 24E+02 63E+02 63E+02	SR2  0.E+0  0.167  -0.54n  0.13/ -0.54n  0.330  0.34n  -0.350	00 00 00 00 00 00 00 00 00 00	\$1 \$2 0.8853E+02-0.46 -0.1041E+03-0.46 -0.1002E+02-0.31 0.2511E+02-0.32 0.3653E+02-0.22 -0.2957E+02-0.22 -0.1546E+02-0.12 0.1451E+02-0.17	\$12 118E+04 0.2503 85E+04 0.2390 29E+04 0.1570 29E+04 0.1777 88E+04 0.1212 56E+04 0.7466 115E+04 0.6139 113E+04 0.6139	BE+040.00 C E+040.03 C E+040.02 C E+040.04 C E+040.02 C E+040.02 C E+040.02 C E+030.02 C E+030.03 C	.1007E+ .9239E+ .6577E+ .7276E+ .5403E+ .5007E+ .3423E+ .34210E+	5 05 0.6146 04 0.2535 04 0.4167 04 0.4459 04 0.4370 04 0.4242 04 0.4010 04 0.4010	J2 E+03 0.3386E+06 t+03 0.2842E+06 t+03 0.1442E+06 t+03 0.1763E+06 t+03 0.9729E+01 t+03 0.435-E+07 t+03 0.5127E+07 t+03 0.5378E+06	J3 3 0.1704E+11 1 0.1042E+11 3 0.404E+10 3 0.7434E+10 7 0.4271E+10 7 0.3496E+10 7 0.2173E+10 0.4252E+10 0.1525E+10
1 2-0.491 2 1-0.497 3 1-0.314 4 1-0.352 5 1-0.225 7 1-0.158 6 1-0.171 9 1-0.121 10 1-0.113	3E+94 0 YE+04 0 3E+94 0 3E+94 0 0FE+04 0 0EE+04 0 4E+04 0 0SE+04 0 0SE+04 0 0SE+04 0	51 66748 57648 44098 48418 38038 34768 38778 30448 26408 24468	• 04 • 04 • 04 • 04 • 04 • 04 • 04 • 04	0.88 -0.11 -0.10 0.19 0.35 -0.30 0.13 0.13 0.13 -0.15 -0.15	53E+02 53E+02 98E+02 78E+02 28E+02 24E+02 63E+02 46E+02 46E+02	\$R2 0.E+0 1.67 -0.54n 0.330 -0.350 0.34s -0.350	00 00E+03 75E+03 75E+03 15E+02 11E+02 11E+02 11E+02	\$1 \$2  0.8853E+02-0.49  -0.1041E+03-0.46  -0.1002E+02-0.31 0.2511E+02-0.35 0.3653E+02-0.22  -0.2957E+02-0.22  -0.1546E+02-0.12 0.1451E+02-0.17 0.1457E+02-0.12  -0.1528E+02-0.11	\$12 118E+04 0.2503 49E+04 0.1570 29E+04 0.1777 80E+04 0.1212 56E+04 0.1113 89E+04 0.7666 115E+04 0.6649 13E+04 0.6139 34E+04 0.53	8E+040.00 0 E+040.03 0 E+040.02 0 E+040.02 0 E+040.02 0 E+030.02 0 E+030.03 0 E+030.03 0 E+030.03 0	.1007E+ .9239E+ .6577E+ .7276E+ .5403E+ .5007E+ .3923E+ .4210E+ .3372E+ .3172E+	5 05 0.6146 04 0.2535 04 0.4167 04 0.4459 04 0.4242 04 0.4510 04 0.4610 04 0.4610 04 0.4610	J2  E+03 0.3386E+06 E+03 0.2442E+06 E+03 0.1442E+06 E+03 0.1763E+06 E+03 0.835-E+07 E+03 0.5127E+07 E+03 0.3786E+01 E+03 0.3786E+01 E+03 0.3302E+01	J3 3 0.1704E+11 3 0.1042+11 5 0.008E+10 5 0.434E+10 7 0.4271E+10 7 0.4271E+10 7 0.4252+10 7 0.4252+10 7 0.4025E+10 7 0.4025E+10 7 0.4025E+10
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9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 9E+04+0 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.547 0 .54	00 - 03 - 05 - 05 - 05 - 05 - 05 - 05 -	\$18ESS ELE  \$1  \$2  0.8853E+02-0.46  -0.1041E+03-0.48  -0.1002E+02-0.31  0.2511E+02-0.32  0.3653E+02-0.22  -0.1546E+02-0.17  0.1451E+02-0.17  0.1457E+02-0.17  0.1457E+02-0.17  0.1457E+02-0.17  0.1457E+02-0.17  0.1452E+01-0.32  0.7461E+01-0.35  0.7461E+01-0.35  0.7452E+01-0.37  0.7458E+01-0.37  0.7458E+01-0.37  0.7458E+01-0.37  0.7458E+01-0.37  0.4476E+01-0.37  0.4476E+01-0.37  0.4476E+01-0.37  0.4476E+01-0.37  0.4476E+01-0.37	\$12  \$18E-04 0.2503  85E-04 0.2390  49E-04 0.1570  88E-04 0.1777  88E-04 0.1670  89E-04 0.7466  15E-04 0.3699  34E-04 0.5591  15E-03 0.3924  16E-03 0.4639  16E-03 0.1656  63E-03 0.1904  16SE-04 0.5591  16SE-04 0.1539  16SE-04 0.1539  16SE-05 0.4109  16SE-06 0.1548  16SE-07 0.1548  16SE-08 0.1558  16SE-08 0.1548  16SE-08 0.1558  16SE	1E+040.00 (1E+040.00 (	.1007E+ .9239E+ .6577E+ .7276E+ .55007E+ .55007E+ .3923E+ .3172E+ .3172E+ .3172E+ .32628E+ .2775E+ .2628E+ .2775E+ .2638E+ .2738E+ .2638E+ .2746E+ .1682E+ 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0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4514 04 0.4511	## 1386 ## 10	J3  3 0.176=11  3 0.10+2:+11  3 0.10+2:+11  3 0.743=10  0.743=10  0.271:10  0.271:10  0.271:10  0.271:10  0.271:10  0.1025:10  0.1025:10  0.1025:10  0.1025:10  0.1025:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.1075:10  0.107

STATE MAP STEP

TABLE VI. - Continued. SAMPLE PROBLEM (3) - OUTPUT

SAMPL	E PROBLEM	3 EXPA	NSION OF A	THICK W	ALL TUBE	STR	IN ELEM	ENT DAT	<b>A</b>			STEP	s <b>-</b>	1 OF	F 2	
NEL	нс	žC.	Ен	ET	ΕZ	EHZ	LK	LZ	LT	LI 1	L2	TL	TS	TH	FLF	NEL
1	1.075.15	00.00664	-0.00701		-0.00044							0.00	-0.00	00.00	0.00000	1
5	1.1-158		-0.00nn3		-0.00038							0.00	00.00	00.00	0.0000	è.
3	1.34049		-0.00444		-0.00039							3.15	-0.00		0.00000	j
. 4	1.27414		-0.00501		-0.00038							0.00	00.00		0.00000	4
5	1.47329		-0.00355		-0.00039							3,12	-0.00		0.00000	Ġ
6	1.53972		-0.00330		-0.00040							0.00	00.00		0.00000	0
?	1.73916		-0.00245		-0.00040							3.12	-0.00		0.00000	7
8	1.67256		-0.00265		-0.00040							0.00	00.00		0.00000	
. 9	1.87220		-0.00200		-0.00040							3.11	-0.00		0.00000	٠
- 10 - 11	1.938/3 2.13b-1		-0.00187 -0.00143		-0.00041							0.00	00.00		0.00000	10
15	2.07164		-0.00154		-0.00041							3.11	-0.00		0.00000	
13	2.27157		-0.00114		-0.00041							3.10	00.00		0.00000	12
14	5.23816		-0.00111		-0.00042							0.00	-0.00		0.00000	ذ ا • ا
15	2.53746		-0.00085		-0.00042							3.09	-0.00		0.00000	15
16	2.47135		-0.00042		-0.00042							0.00	00.00		0.00000	16
17	-2.67119		-0.00070									3.06	-0.00-			
18	2.73791		-0.00065		-0.00043							0.00	00.00		0.00000	Î.
19	2.43770	00.06664	-0.00049	0.00144	-0.00042	-0.00002	0.9995	0.9996	1.0015	0.9996	0.9995	2.91	-0.00		0.00000	ī,
20	2.87137	00.13324	-0.00053	0.00153	-0.00043	0.00000	0.9995	0.9996	1.0015	0.9990	0.9995	0.00	00.00		0.00000	20
21	1.07534	00.33320	-0.00706	0.00804	-0.00044	0.00007	0.9930	0.9996	1.0081	0.9996	0.9930	0.00	00.00	00.00	0.00000	21
22	1.14157		-0.00663		0.00035							3.11	-0.00	00.00	0.00000	22
23	1.34048		-0.00447		-0.00034							0.00	.00.00	00.00	0.00000	ڏِج
24	1.27414		-0.00501		-0.00035							3.09	-0.00	00.00	0.00000	24
25	1.47328		-0.00356		-0.00039		0.9965					0.00	00.00		0.00000	25
26	1.53972		-0.00330		-0.00040							3.12	-0.00		0.00000	26
27	1.73915		-0.00245		-0.00040		0.9976					0.00	00.00		0.00000	27
- 28	1.67206		-0.00265		-0.00040							3.11	-0.00		0.00000	26
29	1.87219		-0.00591		-0.00040		0.9980					0.00	00.00		0.00000	24
30 _	1.93073		-0.00187		-0.00041							3.11	+0.00		0.00000	نو
31	2.138-0		-0.00143		-0.00041							0.00	00.00		0.00000	31
32	2.07134		-0.00154		-0.00041							3.11	-0.00		0.00000	32
33	2.27156		-0.00119		-0.00041							0.00	00.00		0.00000	د 3
34	2.33815		-0.00111		-0.00042							3.10	0.00		0.00000_	_ 34
35	2.53746		-0.00085		-0.00042							0.00	-0.00		0.00000	
36 37	2.47135		-0.00092		-0.00042							0.00	00.00		0.00000	3e 37
38	2.73751		-0.00071		-0.00042							3.05	-0.00		0.00000	3 / 3 ė
39	2.93770		-0.00049		-0.00043							0.00	00.00		0.00000	39
40	2.87107		-0.00053		-0.00043							2.99	-0.00		0.00000	40
		-0,2000				7,000,00	- 33.747.75		600 43		• <u> </u>					

ELE EL. EN. DEN PLS	EN. DEN TOT EN. DEN	HYDRO. TENS. EL	E EL. EN. DEN	PLS EN. DE	N TOT EN. DE	N HYURO. TENS.
1 00.44170E+02 0.E+	00.44170E+02	00.61464E+03 2	00.37026E+02	0.E+00	00.37026E+02	00.25847E+v3 -
3 00.18850E+02 0.E+	00.18850E+02	00.41674E+03 4	00.23061E+02	0.E+00	00.230p1E+02	00.44588E+03
5 00.127+1E+02 0.E+	00.12791E+02	00.48357E+03 6	00.10957E+02	0.E+00	00.109576+02	00.397638+33
7 00.67769E+01 0.E+	00 00.67769E+01	00.4241dE+03 8	00.7807ZE+01	0.E+00	00.78072E+01	00.+607E+03
9 00.505745+J1 0.E+	00 00.50574E+01	00.46725E+03 10	00.44721E+01	0.E+00	00.44721E+01	00.432426+63
11 00.31105E+01 0.E+	00.311056+01	00.4427/E+03 12	00.34662E+01	0.E+00	00.346622+01	00.465176+63
13 00.24917E+01 U.E+	00 00.24917E+01	00.47071E+03 14	10+3SE65S.00	0.E+00	00.22632E+01	00.45143E+03
15 00.17149E+01 0.E+	0000.17199E+01	00.45896E+0316	00.18695E+01	0.E+00	00.18695E+01	00.47211E+03
17 00.145-5E+01 0.E+		00.47961E+03 18	00.13566E+01	0.E+00	"00.13566E+01	00.467336+03
19 00.110+6E+01 0.E+			00.11606E+01	0.E+00	00,118UbE+01	00.48162E+CJ
21 00.443-9E+02 0.E+				0.E+00		00.27530E+03
23 00.14754E+02 0.E+			00.23061E+02	0.E+00		00.46293E+u3
25 00.12749E+02 0.E+			00.10954E+02	0.E+00		00.39689£+53
27 00.675765+01 U.E+			00.78052E+01	0.E+00		00.46033L+u3
29 00.50571E+01 0.E+			00.44705E+01	0.E+00		00.43177E+63
31 00.31024E+01 G.E+			00.34648E+01	0.E+00		00.464561443
33 00.24904E+01 0.E+			00.55951E+01	0.E+0U		00.45111E+63
35 00.17157E+01 U.E+			00.18686E+01	0.E+00		00.47184E+63
37 00.145s3E+01 0.E+	00 00.14583E+01	00.47372E+03 38	00.135556+01	0.E+0U		Lu+16666.00
39 00.1105HE+01 0.E+	00.11068E+01	00.47327E+03 40	00.11795E+01	0.E+0U	CO.11795E+01	00.479956+63

THE ELASTIC ENERGY IS THE PLASTIC ENERGY IS THE TOTAL ENERGY IS THE APPLIED LOAD IS

00.678333E+02 0.E+00 00.67833E+02FOR A LUAD OF 00.153324E+05 THIS IS INCHEMENT 2 - 1 OF 2 15332-4346THE INC. LUAD IS 7186.9549

SCALED STEP

TABLE VI. - Continued. SAMPLE PROBLEM (3) - OUTPUT

					111000			. (0)			
STATE MAP	STEP 2		2								
3 2	1 1		1	1	1 1	1					
1 1	i		i	i	i i	i					
3 2 1 1	l i	-	ļ	1	1 1	1					
	•	1 1		•		TOTAL	DISPLACEMENTS				
0.00943130	0.000000		0.008		0.0000000	0.0074132	0.00000000	0.00664729	0.00000000	0.00611606	0.00000000
3.0056830A° 0.00467217	0.00000		0.005		0.0000000 0000037			0.00493007 0.00738938	0.00000000	0.00477695	0.00000000
1.00609711	00000		0.005		0000859			0.00511845	00008118	0.00667268	000004309
5.00477840	00009		0.004		0000898	E166600 0	00016604	0.00036542	00014135	0.007-0934	00016427
0.30664046 0.00442258	00016		0.006		0001702			0.00536556	00017596	0.00510748	00017900
	******					INCREMENTAL	DISPLACEMENTS	•			
6.00078739	0.00000			61843	0.0000000			0.00049001	0.00300000	0.000~4829	0.00000000
0.00041379 0.00033411	0.00000			38893 78739	0.0000000			0.00035391 0.00055350	0.00000000 00000330	0.0003+226 0.000+9410	0.00000000 00000366
3.00044692	00000		0.000		0000051	0 0.0003673		0.00036020	00000576	0.00035241	00000007
_0.00034143	000000		0.000		0000057		0.0000929	0.00061836	0.00000425	0.00054943	00000769
0.00048472 0.00035217	00000		0.000	33994	0000043			0.00038765	0001000	0.00036678	000,01147
			•			INCREMENTAL	FORCES				
154.0		2.2		-0.0	lo.			0.0	12.0	-0.0	-3.3
-0.0 00.0	-12	2.7		0.00	1. 00.			-0.0 -0.0	01.0 00.0	-0.0 00.0	-2.3 -0.0
-0.0	-00	.0		-0.0	-0.	0	00.0	-0.0	-0.0	00.0	00.0
00.0		0		00.0	00. -0.			-0.0 00.0	-0.0	00.0	-0.0
0.0		.0		00.0	00.			00.0		00.0	00.0
						TOTAL	FORCES				
3756.0	-4	3.2 .4		-0.0	125.			00.0	14.3	-0.0	-9.6
00.0		.5	8	925.0	-0.			-0.0	00.0	00.0	-0.0
	0 (	0.0		-0.0	-0.	0 ` 00.	00.0	-0.0	-0.0"	-0.0	00.0
-0.0		0.0		00.0	<del>-</del> 0.			-0.0 00.0	-0.0 -0.0	-0.0	0.Ò.
00.0		).0		00.0	00.			00.0	-0.0	00.0	00.0
						NODAL	COORDINATES ""				
1.009931 2.005683	0.0000			08375 05372`	0.00000			1.606647 2.604930	0.000000	- 1.806117 - 2.804779	0.000000
3.004672	0.0000			09931	00.19991			1.407389	00.199919	1.605673	JO.199917
1.806097	00.1999			05692	00.19991			2.405118	00.199910	2.60+920	00.199909
2.804778	00.1999			04663 06111	00 <u>.</u> 19991 00.39983			1.208365 2.205366	00.399859 00.399824	1.407409 2.405107	00.399836 00.399821
2.604923	00.399			04769	1866.00						
							00.377020				
SAMPLE PROB					K WALL TUB	٤			STEP	2 2 OF	2
						٤	EMENT DATA		STEP	2 - "- 2 OF	2
SAMPLE PROB	HEM 4 6	XPANSI	ON OF	A THIC	K ∉ALL TUB	E STRESS EI	EMENT DATA				
			ON OF			٤	EMENT DATA	TS SIGE		2 - 2 OF	73
NEL IRV	SR SR	ST	ON OF	A THIC	SRZ	STRESS EI	EMENT DATA		δ <u> </u>	Jz	J3
NEL IRV	SR	ST S50E+0	ON OF	SZ 46E+02	SRZ	STRESS EI	SI2	 E+040.00 0.101	Q 5 5E+05 0.4883E+0	J2 	U.1449E+11
NEL IRV  1 3-0.514 2 2-0.546	SR	ST	ON OF	SZ 46E+02 30E+03	SRZ 0.E+00 0.2230E+0	STRESS EI  S1 5/  0.6446E+02-0.53-0.1437E+03-0.6	SI2 149E+04 0.2607E 472E+04 0.2664E	E+040.00 0.101 E+040.04 0.101	0 5 5E+05 0.4883E+0 0E+05 0.1871E+0	JZ 3 0.34352+0d 3 0.3395E+0d	U.1449E+11 U.1151E+11
NEL IRV  1 3-0.514 2 2-0.546 3 1-0.339 4 1-0.339	SR 3E+04 0.6 7E+04 0.6 1E+04 0.4 1E+04 0.4	ST -550E+0 -177E+0 -774E+0 -209E+0	4 0.544 4-0.15 4 0.127	SZ 46E+02 30E+03 04E+02 64E+02	SRZ 0.E+00 0.2230E+0 -0.4591E+0	STRESS EI  0.6446E+02-0.5 3-0.1437E+03-0.2 20.1267E+02-0.3 3-0.3664E+02-0.3	SI2  149F+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1969E		55-05 0.4883E-03 0E-05 0.4883E-03 7E-04 0.4684E-03 5E-04 0.4480E-03	J2 3 0.34352+0d 3 0.33952+0d 3 0.16722+0d 3 0.20652+0d	0.1449E+11 0.1151E+11 0.754E+10 0.5589E+10
NEL IHV  1 3-0.514 2 2-0.546 3 1-0.339 4 1-0.339 5 1-0.256	SR	ST -550E+0 -177E+0 -774E+0 -204E+0	4 0.644 4-0.15 4 0.124 4 0.276 4 0.505	5Z 46E+02 30E+03 64E+02 55E+02	SRZ 0.E+00 0.2230E+0 -0.4541E+0 -0.4581E+0 -0.4589E+0	STRESS EI  0.6446E+02-0.5 3-0.1437E+03-0.5 2.0.1267E+02-0.3 3.0.3664E+02-0.2 2.0.5135E+02-0.2	SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1949E 587E+04 0.1319E	1-040.00 0.101 1-040.04 0.101 1-040.01 0.709 1-040.05 0.791 1-040.02 0.584	0 5 55+05 0.48835+0: 06+05 0.18716+0: 76+04 0.46866+0: 56+04 0.44806+0: 16+04 0.52406+0:	J2 3 0.3435£+0d 3 0.3395£+0d 3 0.167££+0d 3 0.2065£+0d 3 0.1137£+08	0.1449E+11 0.1151E+11 0.71504E+10 0.5089E+10 0.5277E+10
NEL INV  1 3-0.514 2 2-0.564 3 1-0.339 4 1-0.339 5 1-0.236 6 1-0.247	SR  SR	ST 	4 0.544 4-0.15 4 0.12( 4 0.274 4 0.50 4-0.34	A THIC 5Z 45E+02 45E+03 64E+02 55E+02 78E+02	SRZ 0.E+00 0.2230E+0 -0.4591E+0 0.1881E+0 0.4589E+0	STRESS EI  0.6446E+02-0.5 3-0.1637E+03-0.2 0.1267E+02-0.3 0.3664E+02-0.2 2.5135E+02-0.2 2-0.3394E+02-0.2	SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1969E 587E+04 0.1314E	-040.00 0.101 -040.04 0.101 -040.01 0.709 -040.05 0.791 -040.02 0.584 -040.02 0.584	0 55E+05 0.4483E+0: 0E+05 0.1871E+0. 7E+04 0.4686E+0. 5E+04 0.4480E+0. 1E+04 0.5240E+0. 7E+04 0.414E+0.	J2 3 0.34355+0d 3 0.3355+0d 3 0.16725+0d 3 0.20655+0d 3 0.11375-0d	0.1449E+11 0.1151E+11 0.1504E+10 0.5089E+10 0.5089E+10 0.5089E+10
NEL INV  1 3-0.514 2 2-0.546 3 1-0.336 4 1-0.336 6 1-0.247 7 1-0.173 6 1-0.147	SR  #E+04 0.6 #E+04 0.6 #E+04 0.4 #E+04 0.4 #E+04 0.4 #E+04 0.4	ST 550E+0 177E+0 774E+0 1209E+0 104E+0 1140E+0 1321E+0	4 0.544 4-0.154 4-0.154 4-0.154 4-0.344 4-0.176	A THIC 5Z 46E+02 30E+03 64E+02 64E+02 78E+02 78E+02 78E+02	SRZ  0.E+00 0.2230E+0 -0.4591E+0 -0.1681E+0 0.4522E+0 -0.4552E+0 -0.3765E+0 0.4456E+0	STRESS EI  0.6446E+02-0.5  0.1637E+03-0.5  0.1267E+02-0.5  0.3664E+02-0.6  2.0.5135E+02-0.6  2-0.3394E+02-0.6  2-0.1503E+02-0.6  2.0.1699F+02-0.7	SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1969E 587E+04 0.1319E 475E+04 0.1221E 731E+04 0.8574E	*040.00 0.101 *040.04 0.101 *040.01 0.709 *040.05 0.791 *040.02 0.584 *040.02 0.542 *030.02 0.424 *030.02 0.424	9 5 5E+05 0.4883E+0: 0E+05 0.1871E+0. 7E+04 0.4684E+0. 5E+04 0.488UE+0. 1E+04 0.524UE+0. 7E+04 0.4114E+0. 1E+04 0.4813E+0.	J2 3 0.3435E+0d 3 0.3395E+0d 3 0.167dE+0d 3 0.1137E+08 3 0.1137E+08 3 0.9815E+07 4 0.5995E+07	0.1449E+11 0.1151E+11 0.1504E+10 0.5049E+10 0.5277E+10 0.4241E+10 0.2594E+10
NEL INV 1 3-0.514 2 2-0.566 3 1-0.336 4 1-0.349 5 1-0.267 7 1-0.173 6 1-0.167 9 1-0.132	SR  #E+04 0.6 #E+04 0.4 #E+04 0.4 #E+04 0.7 #E+04 0.7 #E+04 0.7 #E+04 0.7	ST   S50E+0   177E+0   177E+0   108E+0   108E+0   108E+0   132E+0	4 0.644 4-0.15 4 0.124 4 0.505 4 0.34 4-0.15 4 0.17 4 0.17	A THIC 52 46E+02 30E+03 64E+02 55E+02 78E+02 19E+02	0.E+00 0.2230E+0 0.2230E+0 0.1691E+0 0.1691E+0 0.4522E+0 0.4522E+0 0.4752E+0 0.4456E+0 0.4456E+0	STRESS EI  0.6446E+02-0.5 3-0.1647E+03-0.2 0.1267E+02-0.3 0.3664E+02-0.2 2.5135E+02-0.2 2-0.3394E+02-0.2 2-0.3194E+02-0.2 2-0.1194E+02-0.3 0.1124E+02-0.3	EMENT DATA  SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1959E 587E+04 0.1319E 475E+04 0.1221E 731E+04 0.8574E 860E+04 0.990E 365E+04 0.990E	*040.00 0.101 *040.04 0.101 *040.01 0.709 *040.05 0.791 *040.02 0.584 *040.02 0.542 *030.02 0.424 *030.02 0.455 *030.03 0.364	0 5E-05 0.4883E-0: 0E-05 0.1871E-0: 7E-04 0.4684E-0: 5E-04 0.4480E-0: 1E-04 0.5240E-0: 7E-04 0.4513E-0: 0E-04 0.4513E-0: 0E-04 0.4803E-0: 5E-04 0.4970E-0:	J2 3 0.3435E+0d 3 0.3355E+0d 3 0.1676E+0d 3 0.1205E+0d 3 0.1137E+0d 3 0.4915E+07 3 0.595E+07 3 0.595E+07 3 0.692E+07	0.1449E+11 0.1151E+11 0.1564E+10 0.568E+10 0.568E+10 0.4271E+10 0.4294E+10 0.3294E+10 0.3146E+10
NEL INV  1 3-0.514 2 2-0.546 3 1-0.339 4 1-0.339 5 1-0.236 6 1-0.427 7 1-0.173 6 1-0.102 10 1-0.124	SR  SR	ST	4 0.644 4-0.154 4 0.127 4 0.127 4 0.503 4-0.34 4-0.174 4 0.101 4 0.101	A THIC 52 46E+02 30E+03 64E+02 55E+02 78E+02 19E+02 67E+02	SRZ  0.E+00  0.2230E+0  0.4541E+0  0.1841E+0  -0.4589E+0  -0.452E+0  0.4456E+0  -0.3765E+0  0.1451E+0	STRESS EI  0.6446E+02-0.5  0.1637E+03-0.5  0.1267E+02-0.5  0.3664E+02-0.6  2.0.5135E+02-0.6  2-0.3394E+02-0.6  2-0.1503E+02-0.6  2.0.1699F+02-0.7	EMENT DATA  SI2  149F.04 0.2607E 472E.04 0.2664E 382E.04 0.1969E 987E.04 0.1319E 475E.04 0.1221E 731E.04 0.8579E 880E.04 0.9490E 342E.04 0.0512E	**************************************	9 5 55 + 05 0.4883 E + 0: 05 + 05 0.187 I E + 0: 75 + 04 0.4684 E + 0: 55 + 04 0.480 E + 0: 16 + 04 0.480 E + 0: 17 + 05 E + 0: 18 +	J2 3 0.3435E+08 3 0.3355E+08 3 0.167:E+08 3 0.167:E+08 3 0.4137E+08 3 0.4815E+07 3 0.5955E+07 4 0.692-E+07 3 0.4427E+07 3 0.4427E+07	0.1449E+11 0.1151E+11 0.7564E+10 0.5689E+10 0.567E+10 0.4291E+10 0.209E+10 0.209E+10 0.2020E+10 0.1756E+10
NEL IHV  1 3-0.514 2 2-0.566 3 1-0.338 4 1-0.349 5 1-0.257 7 1-0.173 6 1-0.147 9 1-0.132 10 1-0.124 11 1-0.541	SR	ST	4 0.644 4-0.15; 4 0.12; 4 0.13; 4 0.34; 4-0.13; 4-0.17; 4 0.10; 4-0.17; 4-0.13; 4-0.13; 4-0.17;	A THIC 5Z 46E+02 30E+03 64E+02 55E+02 78E+02 78E+02 19E+02 42E+02 50E+01	0.E+00 0.2230E+0 0.2230E+0 0.1691E+0 0.459E+0 0.452E+0 0.455E+0 0.455E+0 0.455E+0 0.145E+0 0.145E+0 0.1256+2+0	STRESS EI  0.6446E+02-0.5 3-0.1437E+03-0.2 3-0.1267E+02-0.3 3-0.3664E+02-0.2 2-0.3394E+02-0.2 2-0.3394E+02-0.2 2-0.1503E+02-0.3 2-0.1750E+02-0.3 2-0.1750E+02-0.2 2-0.1750E+02-0.2 2-0.185E+02-0.3 2-0.185E+02-0.3 2-0.185E+01-0.3	EMENT DATA  SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1969E 587E+04 0.1319E 475E+04 0.122E 73E+04 0.9574E 860E+04 0.96774E 860E+04 0.9672E 242E+04 0.0122E 723E+03 0.4248E 415E+03 0.4248E	**************************************	0 5 55E+05 0.4883E+01 06+05 0.1871E+01 76+04 0.4664E+01 55E+04 0.4480L+01 16+04 0.5240E+01 76+04 0.414E+01 16+04 0.4803E+01 55E+04 0.4950E+01 06E+04 0.470EE+01 9E+04 0.470EE+01	J2 3 0.3435E+08 3 0.3395E+08 3 0.1676E+08 3 0.1676E+08 3 0.1137E+08 3 0.79815E+07 3 0.5995E+07 3 0.692FE+07 3 0.492FE+07 3 0.392FE+07 3 0.2685E+07	0.1449E+11 0.1151E+11 0.1564E+10 0.568E+10 0.568E+10 0.277E+10 0.2491E+10 0.3146E+10 0.1756E+10 0.1187E+10
NEL INV  1 3-0.514 2 2-0.546 3 1-0.336 4 1-0.336 6 1-0.247 7 1-0.173 6 1-0.147 9 1-0.132 11 1-0.871 12 1-0.941 13 1-0.540	SR SR VE+04 0.6 VE+04 0.6 VE+04 0.4 UE+04 0.4 DE+04 0.7 VE+04 0.7 VE+04 0.7 VE+04 0.7 VE+03 0.7 SE+03 0.7 SE+03 0.7 SE+03 0.7 SE+03 0.7	ST	4 0.644 4-0.154 4 0.164 4 0.174 4 0.174 4-0.174 4 0.174 4 0.114 4 0.174 4 0.174 4 0.174 4 0.174 4 0.174 4 0.174 4 0.174 4 0.184 6 0.184 6 0.184 6 0.184	A THIC 52 46E+02 30E+03 64E+02 64E+02 65E+02 19E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67E+02 67	0.E+00 0.2230E+0 0.4591E+0 0.4591E+0 0.4552E+0 0.455E+0 0.455E+0 0.455E+0 0.455E+0 0.1431E+0 0.1431E+0 0.1431E+0	STRESS EI  0.6446E+02-0.5	SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1319E 475E+04 0.1221E 731E+04 0.8574E 800E+04 0.9490E 325E+04 0.9470E 325E+04 0.9470E 475E+03 0.4274E 415E+03 0.4274E	**************************************	95 55+05 0.4883E+00 05+05 0.1871E+00 05+05 0.1871E+00 05+04 0.46406+00 55+04 0.4513E+00 16+04 0.4513E+00 16+04 0.4513E+00 16+04 0.4513E+00 16+04 0.470E+00 19+04 0.470E+00 19+04 0.470E+00 19+04 0.470E+00 19+04 0.470E+00	J2 3 0.3435E+08 5 0.3395E+08 5 0.3395E+08 6 0.1676E+08 6 0.1137E+08 6 0.1137E+08 7 0.5995E+07 7 0.3921E+07 7 0.3921E+07 7 0.2997E+07 7 0.2997E+07 7 0.2997E+07	0.1449E+11 0.1151E+11 0.756+E+10 0.5277E+10 0.5277E+10 0.4241E+10 0.2049E+10 0.3146E+10 0.4020E+10 0.1756E+10 0.1145E+10 0.1345E+10 0.1345E+10
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NEL INV  1 3-0.514 2 2-0.56 3 1-0.336 4 1-0.37 5 1-0.25 6 1-0.247 7 1-0.173 6 1-0.17 9 1-0.132 10 1-0.50 11 1-0.50 12 1-0.50 13 1-0.50 15 1-0.372 16 1-0.414 17 1-0.25 18 1-0.17 19 1-0.52 20 1-0.85 21 3-0.54 23 1-0.334 24 1-0.337 25 1-0.26 26 1-0.27 27 1-0.17 29 1-0.13 30 1-0.14 31 1-0.50 32 1-0.94 33 1-0.54 33 1-0.54 31 1-0.54 33 1-0.54 33 1-0.54	SR  SR	ST   S50E+0   1776E+0   17	4 0.644 4 0.644 4 0.15; 4 0.15; 4 0.27; 4 0.15; 4 0.15; 4 0.15; 4 0.16; 4 0	A THIC  SZ  46E+032  46E+032  578E+022	0.E+00 0.2230E+0 0.4230E+0 0.4591E+0 0.4592E+0 0.4552E+0 0.4151E+0 0.2569E+0 0.415E+0 0.415E+0 0.4175E+0 0.11716E+0 0.1474E+0	STRESS EI  ST ST ST  0.6446E+02-0.5  2-0.1637E+03-0.5  2-0.1637E+02-0.5  3-0.3394E+02-0.6  2-0.3394E+02-0.6  2-0.1503E+02-0.6  2-0.1724E+02-0.6  2-0.1726E+02-0.6  2-0.1726E+02-0.6  2-0.1726E+02-0.6  2-0.1726E+01-0.6  1-0.144E+02-0.6  2-0.870SE+01-0.6  1-0.3467E+01-0.6  1-0.3467E+01-0.6  2-0.870SE+01-0.6  1-0.3465E+02-0.6  2-0.870SE+01-0.6  1-0.3465E+02-0.6  2-0.870SE+01-0.6  1-0.3465E+02-0.6  2-0.3152E+02-0.6  2-0.3152E+01-0.6  2-0.3152E+01-0.6	### ST2  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1319E 475E+04 0.1221E 731E+04 0.8574E 813E+04 0.9490E 325E+04 0.9490E 415E+03 0.4294E 415E+03 0.4744E 413E+03 0.4744E 413E+03 0.4744E 413E+03 0.4744E 413E+03 0.40744E 413E+03 0.40744E 413E+03 0.40744E 413E+03 0.40744E 413E+03 0.40744E 413E+04 0.2673E 334E+04 0.2673E 348E+04 0.2673E 348E+04 0.2673E 337E+04 0.1621E 476E+04 0.1621E	100 0 0 101 1 1 1 1 1 1 1 1 1 1 1 1 1 1	95  55  56  50  50  60  60  60  60  60  6	J2  3 0.3435E+08 3 0.3355E+08 3 0.1676E+08 3 0.1676E+08 3 0.1137E+08 3 0.595E+07 3 0.692+E+07 3 0.3921E+07 3 0.3921E+07 3 0.295E+07 3 0.1916E+07 3 0.1105E+07	0.1449E+11 0.1151E+11 0.7564E+10 0.5689E+10 0.5277E+10 0.4249E+10 0.3277E+10 0.4249E+10 0.1756E+10 0.1756E+10 0.1756E+10 0.1756E+10 0.1756E+10 0.1245E+09 0.5256E+09 0.5256E+10
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NEL INV  1 3-0.514 2 2-0.566 3 1-0.338 4 1-0.379 5 1-0.256 6 1-0.247 7 1-0.173 8 1-0.127 10 1-0.132 10 1-0.132 10 1-0.132 11 1-0.640 11 1-0.571 12 1-0.521 13 1-0.640 14 1-0.592 15 1-0.372 16 1-0.144 17 1-0.255 18 1-0.177 19 1-0.529 20 1-0.845 21 3-0.521 22 2-0.544 23 1-0.373 24 1-0.373 25 1-0.261 26 1-0.277 27 1-0.172 28 1-0.177 29 1-0.133 30 1-0.124 31 1-0.549 32 1-0.941 33 1-0.644 33 1-0.644 34 1-0.593 35 1-0.414 37 1-0.293 38 1-0.414 37 1-0.293	SR  SR	550E+0 177E+0 177E+0 177E+0 177E+0 177E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704E+0 1704	4 0 . 644 4 0 . 644 4 0 . 15; 4 0 . 17; 4 0 . 12; 4 0 . 12; 4 0 . 12; 4 0 . 13; 4 0 . 14; 4 0 . 14;	A THIC 23 46 E + 03 22 46 E + 04 22 22 46 E + 04 22 22 24 26 E + 04 22 22 24 26 E + 04 22 24 26 26 26 26 26 26 26 26 26 26 26 26 26	0.E+00 0.2230E+0 0.2230E+0 0.4522E+0 0.1881E+0 0.4545E+0 0.4545E+0 0.455E+0 0.455E+0 0.3765E+0 0.3765E+0 0.3765E+0 0.1431E+0 0.0.2569E+0 0.3931E+0 0.1959E+0 0.3931E+0 0.1716E+0 0.4475E+0	STRESS EI  ST	EMENT DATA  SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1319E 475E+04 0.8574E 880E+04 0.9490E 325E+04 0.9490E 325E+04 0.9712E 472E+03 0.4294E 415E+03 0.494E 415E+03 0.497E 426E+04 0.621E 426E+04 0.132E 426E+03 0.427E	*** **** **** **** **** **** **** **** ****	95  55  56  50  50  50  50  50  50  50  5	J2  3 0.3435E+0d 3 0.3395E+0d 3 0.3395E+0d 3 0.1676250d 3 0.11376+08 3 0.9415E+07 4 0.5995E+07 5 0.3442E+07 5 0.3442E+07 6 0.2645E+07 7 0.2645E+07 7 0.155E+07 7 0.345E+07 7 0.345E+07 7 0.345E+07 7 0.345E+07 7 0.4435E+07 7 0.4435E+	0.1449E+11 0.1151E+11 0.7064E+10 0.5089E+10 0.2772+10 0.4291E+10 0.2772+10 0.429E+10 0.1756E+10 0.1756E+10 0.1756E+10 0.1343E+10 0.1343E+10 0.1243E+09 0.5082E+09
NEL INV  1 3-0.514 2 2-0.566 3 1-0.339 4 1-0.349 5 1-0.256 6 1-0.247 7 1-0.173 6 1-0.174 11 1-0.871 12 1-0.971 13 1-0.500 14 1-0.590 15 1-0.372 20 1-0.855 21 3-0.521 22 2-0.564 23 1-0.372 25 1-0.27 27 1-0.172 28 1-0.27 27 1-0.172 28 1-0.27 27 1-0.172 28 1-0.27 27 1-0.173 30 1-0.147 29 1-0.133 30 1-0.147 31 1-0.4648 32 1-0.590 35 1-0.371 31 1-0.590 35 1-0.371 31 1-0.590 35 1-0.371 37 1-0.177 39 1-0.177 39 1-0.177 39 1-0.593 31 1-0.590 35 1-0.371 37 1-0.237 38 1-0.590 38 1-0.590 39 1-0.592	SR	ST	4 0 - 644 4 - 0 - 154 4 - 0 - 157 4 - 0 - 157 5 - 0 -	A THIC 23 C	0.E+00 0.2230E+0 0.2230E+0 0.4552E+0 0.4552E+0 0.4552E+0 0.3765E+0 0.4556E+0 0.3765E+0 0.4456E+0 0.4556E+0 0.3765E+0 0.143E+0 0.143E+0 0.1456E+0 0.2569E+0 0.3765E+0 0.1656E+0 0.1766E+0 0.1766E+0 0.1766E+0 0.1766E+0 0.1766E+0 0.176E+0 0.1776E+0 0.1776E+0 0.1776E+0 0.1779E+0 0.	STRESS EI  0.6446E+02-0.5 3-0.1637E+03-0.2 0.1267E+02-0.3 0.3664E+02-0.2 2.0.1267E+02-0.2 2.0.1265E+02-0.2 2.0.1265E+02-0.2 2.0.1750E+02-0.2 2.0.1750E+02-0.3 2.0.165E+02-0.3	EMENT DATA  SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1319E 475E+04 0.1319E 475E+04 0.1319E 475E+04 0.6712E 242E+04 0.6714E 242E+04 0.162E 242E 242E+04 0.162E 242E+04 0.1	6.040.00 0.101 6.040.04 0.101 6.040.04 0.101 6.040.05 0.791 6.040.05 0.791 6.040.05 0.542 6.030.02 0.425 6.030.03 0.364 6.030.02 0.425 6.030.03 0.364 6.030.01 0.343 6.030.02 0.495 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203	0 5  55 - 05 0.4883E - 03  05 - 05 0.4883E - 03  05 - 05 0.4881E - 03  05 - 04 0.4801E - 03  05 - 04 0.4950E - 03  05 - 04 0.504E - 03  05 - 04 0.490E - 03  06 - 04 0.490	J2  3 0.3435E+08 3 0.335E+08 3 0.1676E+08 3 0.205E+08 3 0.1137E+08 3 0.595E+07 3 0.692-E+07 3 0.3921E+07 3 0.2685E+07 3 0.2947E+07 3 0.211-E+07 3 0.195E+07 3 0.195E+07 3 0.195E+07 3 0.195E+07 3 0.195E+08 3 0.3455E+08 3 0.345E+08 3 0.346E+08 3 0.34	0.1449E+11 0.1151E+11 0.7564E+10 0.5649E+10 0.2549E+10 0.4241E+10 0.2549E+10 0.1756E+10
NEL INV  1 3-0.514 2 2-0.566 3 1-0.339 4 1-0.349 5 1-0.256 6 1-0.247 7 1-0.173 6 1-0.174 11 1-0.871 12 1-0.971 13 1-0.500 14 1-0.590 15 1-0.372 20 1-0.855 21 3-0.521 22 2-0.564 23 1-0.372 25 1-0.27 27 1-0.172 28 1-0.27 27 1-0.172 28 1-0.27 27 1-0.172 28 1-0.27 27 1-0.173 30 1-0.147 29 1-0.133 30 1-0.147 31 1-0.4648 32 1-0.590 35 1-0.371 31 1-0.590 35 1-0.371 31 1-0.590 35 1-0.371 37 1-0.177 39 1-0.177 39 1-0.177 39 1-0.593 31 1-0.590 35 1-0.371 37 1-0.237 38 1-0.590 38 1-0.590 39 1-0.592	SR	ST	4 0 - 644 4 - 0 - 154 4 - 0 - 157 4 - 0 - 157 5 - 0 -	A THIC 23 C	0.E+00 0.2230E+0 0.2230E+0 0.4552E+0 0.4552E+0 0.4552E+0 0.3765E+0 0.4556E+0 0.3765E+0 0.4456E+0 0.4556E+0 0.3765E+0 0.143E+0 0.143E+0 0.1456E+0 0.2569E+0 0.3765E+0 0.1656E+0 0.1766E+0 0.1766E+0 0.1766E+0 0.1766E+0 0.1766E+0 0.176E+0 0.1776E+0 0.1776E+0 0.1776E+0 0.1779E+0 0.	STRESS EI  ST	EMENT DATA  SIZ  149E+04 0.2607E 472E+04 0.2664E 382E+04 0.1697E 902E+04 0.1319E 475E+04 0.1319E 475E+04 0.1319E 475E+04 0.6712E 242E+04 0.6714E 242E+04 0.162E 242E 242E+04 0.162E 242E+04 0.1	6.040.00 0.101 6.040.04 0.101 6.040.04 0.101 6.040.05 0.791 6.040.05 0.791 6.040.05 0.542 6.030.02 0.425 6.030.03 0.364 6.030.02 0.425 6.030.03 0.364 6.030.01 0.343 6.030.02 0.495 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.215 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203 6.030.01 0.203	0 5  55 - 05 0.4883E - 03  05 - 05 0.4883E - 03  05 - 05 0.4881E - 03  05 - 04 0.4801E - 03  05 - 04 0.4950E - 03  05 - 04 0.504E - 03  05 - 04 0.490E - 03  06 - 04 0.490	J2  3 0.3435E+08 3 0.335E+08 3 0.1676E+08 3 0.205E+08 3 0.1137E+08 3 0.595E+07 3 0.692-E+07 3 0.3921E+07 3 0.2685E+07 3 0.2947E+07 3 0.211-E+07 3 0.195E+07 3 0.195E+07 3 0.195E+07 3 0.195E+07 3 0.195E+08 3 0.3455E+08 3 0.345E+08 3 0.346E+08 3 0.34	0.1449E+11 0.1151E+11 0.7564E+10 0.5649E+10 0.2549E+10 0.4241E+10 0.2549E+10 0.1756E+10

TABLE VI. - Continued. SAMPLE PROBLEM (3) - OUTPUT

SAHP	PLE PROBLEM	3 ЕХРА	NSION OF A	THICK W	ALL TUBE	STR	AIN ELEM	ENT DAT	A			STEP	2 -	S 01	F 2	
NEL	нс	ŞC	ER	ετ	€Z	ERZ	LR	LZ	LT	LI	L2	ŤL	TS	TH	EPEQ	NEL
1	1.07008		-0.00787	0.00471	-0.00042	0.0000	0.9922	0.4496	1.0088	0.9996	0.9922	0.00	-0.00	00.00	0.30082	1
S	1.14226		-0.00733		-0.00037							0.00	00.00		0.30000	2
) 4	1.34106		-0.00485		-0.00041							3.13	-0.00		0.00000	3
5.	-1.47342		-0.00385		-0.00037							0.00 3.12	-u.00		0.00000	- 5
6	1.540/4		0.003n0		-0.00042							0.00	00.00		0.10000	6
7	1.73962		-0.00206		-0.00043							3.12	-0.00		0.00000	7
8	1.67314	HSEE1.00	-0.00284		-0.00042							0.00	00.00		0.0000	8
9	1.87253	00.05664	-0.00217	0.00318	~0.00043	-0.00009	0.9978	0.4946	1.0032	0.9996	0.9978	3.11	-0.00	10.00	0.30000	4
10	1.93916		-0.00203		-0.00043							0.00	00.00		0.00000	10
11	2.13880		-0.00156		-0.00044							3.11	-0.00		0.30000	11
12	2.07224		-0.00167		-0.00043							0.00	00.00		0.0000	12
14	2.27145 2.33853		-0.00129		-0.00044							3.10 0.00	-0.00		0.10100	13
15	2.53832		-0.00043		-0.00045							3.09	-0.00		0.00000	15
16	2.41112		-0.00044		-0.00045							0.00	00.00		0.00000	16
17	2.67154	30.06664	-0.00076		-0.00045							3.06	-0.00			17
18	2.73816		-0.00071		-0.00046							3.13	-0.00	00.00	0.30000	18
19	2.93804		-0.00053		-0.00045							2.90	-0.00		0.30000	14
20	2.471+1		-0.00056		-0.00046							0.00	00.00		0.30000	20
21	1.07598		-0.00742		-0.00041							0.00	00.00		0.10085	
22 23	1.1-226		-0.00733		-0.00034							3.10 3.14	-0.00		0.10000	. 23
24	1.27475		-0.00550		-0.00034							3.08	-0.00		0.30000	24
25	1.473-1		-0.00387		-0.00042							0.00	00.00		0.30000	25
26	1.54023		-0.00360		-0.00041							3.11	-0.00		0.10000	26
27	1.73902	00.33319	-0.00266		-0.00042							0.00	00.00		0-10000	27
28	1.67314		-0.00289		-0.00041							3.11	-0.00	00.00	0.30000	28
29	1.67263		-0.0021H		-0.00042							0.00	00.00		0.10000	29
30	1.93915		-0.00203		-0.00043							3.11	-0.00		0.10000	30
35	2.13850" 2.07224		-0.00155		-0.00044							0.00	00.00		0.10000	31
<u>—35</u>	2.27144		-0.00124		-0.00044			0.9996				3.11	-0.00		0.10000	32
34	2.33053		-0.00120		-0.00045							3.10	-0.00		0.00000	34
35-	2-53832		-0.00093		-0.00045			0.9996				3.00	00.00		0.10000	35
36	2.47172		-0.00099		-0.00045							3.09	-0.00		0.10000	36
37	2.67154		-0.00077	0.00182	-0.00045	0.00000	0.9992	0.9996	1.0018	0.9996	0.9992	0.00	00.00	60.00	0.30000	37
_ 38_		00.26655			-0.00046							3.05	-0.00		0.10000	38
39	2.938)3		-0.00053		-0.00046							0.00	00.00		0.00000	39
40	2.87140	00.20055	-0.00058	0.00165	-0.00046	-0.0000	0.9994	0.9995	1.0017	0.9995	0.9994	2.98	-0.00	60.00	0.30000	40

1 00.44803E+02 00.48217E+01 00.53045E+02 00.44832E+03 2 00.44225E+02 0.E+00 00.44225E+02 00.18710E+03 3 00.71555+02 00.64635E+03 4 00.27266E+02 0.E+00 00.27266E+02 004611E+03 7 00.7154549E+02 0.E+00 00.79178E+01 00.45126E+03 6 00.1885E+02 00.E+00 00.945E+03 10.05503E+01 0.E+00 00.945E+01 00.47077E+03 12 00.4043IE+01 0.E+00 00.4043IE+01 00945E+03 12 00.4043IE+01 0.E+00 00.4043IE+01 00945E+03 12 00.4043IE+01 0.E+00 00.2043E+01 00945E+03 12 00.2043E+01 0.E+00 00.2043E+01 00945E+03 12 00.2043E+01 0.E+00 00.2043E+01 00.5043E+03 12 00.1885E+02 00.E+00 00.1885E+00 00.E+00 00.1885E+00 00.E+00 00.1885E+00 00.E+00 00.1885E+00 00	ELE EL. EN. DEN PLS EN. DEN TOT EN. DEN HYDRO. TENS.	ELE EL. EN. DEN PLS EN. DEN TOT EN. DEN HYURO. TENS.
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25 00.147165-02 0.E+00 00.14976E+02 00.50144E+03 26 00.12862E+02 0.E+00 00.12862E+02 001162E+03 27 00.73979E+01 0.E+00 00.78979E+01 00.45651E+03 28 00.91443E+01 0.E+00 00.9213E+01 003657E+03 30 00.5213E+01 0.E+00 00.5213E+01 003657E+03 31 00.36156E+01 0.E+00 00.36156E+01 00.47527E+03 32 00.40415E+01 0.E+00 00.6213E+01 003657E+03 32 00.40415E+01 0.E+00 00.6213E+01 003442E+03 33 00.27699E+01 0.E+00 00.28999E+01 00.49748E+03 34 00.26323E+01 0.E+00 00.26323E+01 003640E+03 35 00.19743E+01 0.E+00 00.12720E+01 00.50441E+03 36 00.21720E+01 0.E+00 00.21720E+01 00.50441E+03 37 00.16928E+01 0.E+00 00.16728E+01 00.5069E+03 38 00.15729E+01 0.E+00 00.15729E+01 00.50999E+03	21 00.45045E+02 00.82751E+01 00.53320E+02 00.45037E+03	22 00.44192E+02 0.E+00 ' 00.44192E+02 00.20775E+i3
27 00.739795+01 0.6+00 00.739795+01 00.456516+03 28 00.914436+01 0.6+00 00.914436+01 0036576+03 29 00.591606+01 0.6+00 00.5911000+01 00.490046+03 30 00.522136+01 0.6+00 00.522136+01 00365786+03 30 00.522136+01 0.6+00 00.522136+01 00365786+03 30 00.572136+01 0.6+00 00.404156+01 00365786+03 30 00.404156+01 00.6+00 00.404156+01 0034026+03 30 00.273996+01 0.6+00 00.2839976+01 00.497786+03 30 00.27206+01 0.6+00 00.2839876+01 00.497786+03 30 00.27206+01 0.6+00 00.277206+01 00.504416+03 37 00.163286+01 0.6+00 00.167296+01 00.506946+03 38 00.157296+01 0.6+00 00.157296+01 00.4999898+03	23 00.218335+02 0.6+00 00.218336+02 00.482746+03	24 00.27280E+02 0.E+00 00.27280E+02 006857E+03
29 00.59100E+01 0.E+00 00.59100E+01 00.49004E+03 30 00.52213E+01 0.E+00 00.52213E+01 005694E+03 31 00.36154E+01 0.E+00 00.36158E+01 00.47527E+03 32 00.4045E+01 0.E+00 00.4045E+01 009492E+03 33 00.26999E+01 0.E+00 00.2632E+01 009402E+03 34 00.26323E+01 0.E+00 00.2632E+01 0094060E+03 35 00.19943E+01 0.E+00 00.19943E+01 00.49428E+03 36 00.21720E+01 0.E+00 00.21720E+01 0.0.50441E+03 37 00.16928E+01 0.E+00 00.16928E+01 00.50694E+03 38 00.15729E+01 0.E+00 00.15729E+01 00.49899E+03	25 00.149765+02 0.5+00 00.149765+02 00.501445+03	26 00.12862E+02 0.E+00 00.12862E+02 00.41162E+03
31 00.36154E+01 0.E+00 00.36154E+01 00.47527E+03 32 00.40415E+01 0.E+00 00.40415E+01 009432E+03 33 00.26999E+01 0.E+00 00.28999E+01 00.49748E+03 34 00.26323E+01 0.E+00 00.28323E+01 008040E+03 35 00.19493E+01 0.E+00 00.19494E+03 36 00.21720E+01 0.E+00 00.21720E+01 0.E+00 37 00.16928E+01 00.50694E+03 38 00.15729E+01 0.E+00 00.15729E+01 00.59899E+03	27 00.789795+01 0.E+00 00.78979E+01 00.45651E+03	28 00.91443E+01 0.E+00 00.91443E+01 U03657E+63
33 00.28999E+01 0.E+00 · 00.28999E+01 00.4974HE+63 34 00.2832E+01 0.E+00 00.28323E+01 00.+000E+03 35 00.19943E+01 0.E+00 00.21726E+01 00.59441E+03 36 00.21726E+01 0.E+00 00.21726E+01 00.59441E+03 37 00.1692HE+01 0.E+00 00.15729E+01 0.E+00 00.25729E+01 0.E+00 00.2572	29 00.59100E+01 0.E+00 00.59100E+01 00.49004E+03	30 00.52213E+01 0.E+00 00.52213E+01 00.45644E+03
35 00.19943E+01 0.E+00 00.19943E+01 00.49283E+03 36 00.21720E+01 0.E+00 00.21720E+01 00.50441E+03 37 00.16928E+01 0.E+00 00.16928E+01 00.50694E+03 38 00.15729E+01 0.E+00 00.15729E+01 00.49899E+03	31 00.3615mE+01 0.E+00 00.3615bE+01 00.47527E+03	32 00.40415E+01 0.E+00 00.40415E+01 0094J2E+03
37 00.16928E+01 0.E+00 00.16928E+01 00.50694E+03 38 00.15729E+01 0.E+00 00.15729E+01 00.49899E+03	33 00.26999E+01 0.E+00 · 00.28999E+01 00.49748E+03	34 00.26323E+01 0.E+00 00.26323E+01 00d0d0E+63
	35 00.19943E+01	36 00.21720E+01 0.E+00 00.21720E+01 00.50441E+03
39 00.128316+01 0.6+00 00.128316+01 00.508846+03 40 00.136796+01 0.6+00 00.136796+01 00.515576+03	37 00.16928E+01 0.E+00 00.16928E+01 00.50694E+03	38 00.15729E+01 0.E+00 00.15729E+01 00.49899E+03
	39 00.128316+01 0.6+00 00.124316+01 00.508846+03	40 00.13679E+01 0.E+00 00.13679E+01 00.51557E+03

THE ELASTIC ENERGY IS THE PLASTIC ENERGY IS THE TOTAL ENERGY IS THE APPLIED LOAD IS

00.777548E+02 00.221512E+01 00.799709E+02F0R A LOAD OF 00.165074E+05 THIS IS INCHEMENT 2 2 OF 2 16507.4264THE INC. LUAD IS 1174.9918

SCALED STEP

TABLE VI. - Continued. SAMPLE PROBLEM (3) - OUTPUT

	STEP 2 -	. 3							
3 3 1 1 3 3	1 1 1 1 1 1	1 1 1 1 1 1	1 1 1	1 1 1					
1 1 0.0100000 0.00571697 0.0046944 0.00613369 0.00480632 0.0068084 0.00495138	1 1 0.00000000 0.00000000 0.00000000000916100016176	0.00540 0.01000 0.00572 0.00469	7699 0.00000000 3372 0.00000000 100000008244 260300008737 104400017099 178700017099 169400018352	0.00570950 0.005334023 0.00534023 0.00570950	0.00000000 00007260 00008867 00016338 00017463	0.00666744 0.00495902 0.00743441 0.00518457 0.00541744	0.00000000 0.00000000 00004117 00009004 00013955 00017684	0.00615337 0.00480694 0.00671305 0.00494071 0.00745512 0.00513748	0.0000000 0.0000000 0000334 00004132 00016437
0.00006870 0.00003389 0.00002732 0.00002658 0.00002742 0.00002880	0.09000000 0.00000000 0.0000000 00000050 00000067	0.00003 0.00006 0.00003 0.00002 0.00003	0.00000000 0.00000000 0.00000132 0.0000045 0.0000046 0.0000046 0.0000076 0.0000100	0.00004526 0.00003015 0.00005271 0.00003170 0.00006870 0.00003379	0.00000000 0.00000000 0.00000084 00000045 0.00000266 00000085	0.00004014 0.00002895 0.00004503 0.00003012 0.00005207 0.00003173	0.00303000 0.00000000 00000001 00000047 0.00000180 00000088	0.00003672 0.00002799 0.000000 0.0002885 0.00004578	0.0000000 0.0000000 00000031 00000049 00000010 000000093
19.4 -0.0 00.0 00.0 00.0 00.0	2.2 00.4 +1.1 00.0 -0.0 -0.0	4 4	0.0 2.0 0.0 0.3 5.0 00.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	-0.0 0.0 -0.0 -0.0 10.5 00.0	-3.5 00.2 -0.0 00.0 -0.0 -0.0	-0.0 -0.0 -0.0 00.0 -0.0 00.0	-0.7 00.1 00.0 -0.0 -0.0 -0.0	-0.0 -0.0 00.0 00.0 00.0	00.3 -0.2 -0.0 00.0 -0.0 00.0
3775.5 -0.0 00.0 00.0 -0.0 00.0	-41.0 1.8 -55.6 00.0 -0.0 -0.0	896	0.0 127.6 0.0 6.2 9.9 -0.0 0.0 -0.0 0.0 0.0 0.0 0.0	-0.0 -0.0 00.0 3843.0 00.0	-56.3 -56.3 -0.0 00.0 -0.0 -0.0 -0.0 00.0	00.0 -0.0 -0.0 -0.0 -0.0 00.0	13.6 5.5 00.0 -0.0 -0.0	-0.0 -0.0 00.0 -0.0 -0.0	1.7 -9.8 -0.0 00.0 -0.0
1.010000 2.005717 3.004699 1.606134 2.60496611 2.604951	0.000000 0.000000 0.000000 00.194903 00.194903	1.208 2.205 1.010 2.005 3.004	0.000000 404 0.000000 000 00.199918 726 00.199910 690 00.199910 148 00.399829	NODAL 1.407456 2.405145 1.206533 2.205390 1.010000	COORDINATES 0.000000 0.000000 00.199927 00.199911 00.399837	1.606687 2.604359 1.407434 2.405149 1.208417 2.205397	0.000000 0.199910 0.199910 0.399860 0.399860	1.806153 2.804807 1.606713 2.604949 1.407455 2.405137	0.000000 0.000000 00.159917 00.199909 00.399836
	30.337010	2.804	797 00.399816	3.004690	00.399817	2.203377			
NEL IRV	ILEM 3" EXP	ANSTON OF A	THICK WALL TUBE	3.004690		TS SIGEO	STEP	2 - 3 OF	2

TABLE VI. - Concluded. SAMPLE PROBLEM (3) - OUTPUT

SAMPL	E PHOBLEM	. З ЕХРА	NSION OF A	THICK W	ALL TUBE	STR	IN ELEM	ENT DAT	<b>A</b>			STER	· ' ¿ -	3 0	7 2	
NEL	⊀c	<b>2</b> C	EH	£Τ	εZ	ERZ	LR	LZ	LT	LI	. L?	TL	ts	TR	FhEO	NEL
1	1.07614		-0.00746		-0.000+1							0.00	-0.00	00.00	0.00089	1
5	1.14232		-0.00742		-0.00036							0.00	00.00		0.00007	2
3	1.3-111		-0.004ов		-0.000+1							3.13	-0.00		0.00000	
5	1.27440 1.473no		-0.00554 -0.00388		-0.00036							0.00	00.00		0.00000	4
6	1.54028		-0.00363		-0.00041							3.15	-0.00		0.00000	5
ž	1.73966		-0.003os		-0.00042							3.12 0.00	-0.00		0.00000	7
	1.6/318		-0.00241		-0.00042							0.03	00.00		0.00000	ė
9	1.87267		-0.00214		-0.00043							3.11	-0.00		0.00000	ij.
10	1.93919	HSEE1.00	-0.00204		-0.00044							0.00	00.00		0.00000	10
11	2.138#4	00.05664	-0.00157	0.00257	-0.00044	-0.00003	0.9984	0.9996	1.0026	0.4990	0.9984	3.11	-0.00	00.00	0.00000	11
12	2.07228		-0.0010H		-0.00044							0.00	00.00		0.00000	12
13	2.27178		-0.00130		-0.00044							3.10	-0.00		0.00000	٤1
14	2.33856		-0.00121		-0.00045							0.00	00.00		0.00000	14
15	2.53815		-0.0009.		-0.000-6							3.09	-0.00		0.00000	15
16	2.47175		0.00100_		-0.00045							0.00	00.00		0.00000	16
17	7:07157 2.73819		-0.0007n -0.00071		-0.00046							3.00 3.13	-0.00		0.00000	17 18
19	2.93817		-0.00054		-0.00045							2.40	-0.00		0.00000	19
20	2.87143		-0.00055		-0.00046							0.0ù	00.00		0.00000	20
21	1.07614		-0.00801		-0.00040							0.00	00.00		0.00000	21
22	1.14232		-0.00742		-0.00034							3.10	-0.00		0.00007	55
23	1.34110		-0.00485		-0.00042							3.1-	-0.00		0.00000	23
24	1.27450		-0.00554		-0.00034							3.00	-0.00		0.00000	24
25	1.47306	00.33320	-0.00349	0.00+87	-0.00042	0.0000	0.9961	0.9996	1.0049	0.9996	0.4961	0.00	00.00	00.00	0.00000	25
26	1.54028	J0.20656	-0.00363	0.00450	-0.00042	-0.0000	0.9964	0.9996	1.0045	0.4996	0.9964	3.11	-0.00	00.00	0.00000	26
27	1.73965		-0.00268		-0.00043							0.00	00.00	00.00	0.00000	27
28	1.67318		-0.00291		-0.00042							3.11	-0.00	00.00	0.00000	28
29~	1.87266		-0.00220		-0.00043							0.00	00.00		0.00000	24
30	1.93919		-0.00204		-0.00044							3.11	-0.00		0.00000	30
31	2.13853		-0.00156		-0.00044							0.00	00.00		0.00000	31
33	2.07228		-0.00156		-0.00044							3.11	-0.00		0.00000	32
34	2.33856		-0.00130 -0.00121		-0.00044							0.00	00.00		0.00000	33
-35			-0.00043									3.10	-0.00		0.00000	34 35
35	2.47174		-0.00100		-0.00045							0.06 3.09	-0.00		0.00000	35 36
37	2.67157		-0.00077		-0.00045							0.00	00.00		0.00000	37
38	2.73818		-0.00071		-0.00045							3.05	-0.00		0.00000	36
39	2.93806		-0.00053		-0.00046							0.00	00.00		0.00000	39
43	2.87143		-0.00058		-0.00046							2.98	-0.00		0.00000	40

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ELE EL. EN. DEN PLS EN. DEN TOT EN. DEN MYDPO. TENS.

1 00.446002-02 00.90134-01 00.53374E-02 00.47102E+03 2 0.4231E+02 00.69812E+00 00.44779E+02 00.16500E+03 3 00.22233E+02 0.E+00 00.22233E+02 00.4709E+03 4 00.27621E+02 0.E+00 00.27621E+02 00.6910E+03 5 00.15137E-02 0.E+00 00.15137E-02 00.52713E+03 4 00.27621E+02 0.E+00 00.27621E+02 00.49310E+03 7 00.86154E+01 0.E+00 00.15137E-02 0.E+00 00.15137E-02 0.E+00 00.15137E-02 0.E+00 00.15137E-03 8 00.42592E+01 0.E+00 00.92592E+01 0.0.4938E+03 10 0.59782E+01 0.E+00 00.59782E+01 0.E+00 00.59782E+01
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THE ELASTIC ENEMGY IS
THE PLASTIC ENEMGY IS
THE TOTAL EMEMGY IS
THIS TOTAL EMEMGY IS
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TAPE HESTART GENERATION ... STEP 2 - 1 OF 2

TABLE VII. - SAMPLE PROBLEM (4) - INPUT

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SAMPLE PRUBLEY 3 EXPANSION OF A THICK WALL TUBE
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           1 3-0.63925+04 0.57405+04+0.74465+02 0.E+00
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           1 3-0,5357-94 0.5140E-04-0.5336E-03 0.140E+03-0.524E-03-0.683E-04 0.3152E-040.03 0.1042E-05-0.720BE-03 0.365E-040-0.6763E-10 3 1-0,4366E-04 0.535E-04 0.535E-04 0.5743E-03 0.365E-04 0.5743E-03 0.365E-04 0.5743E-03 0.265FE-03 0.365E-04 0.5743E-03 0.265FE-03 0.365E-04 0.5743E-03 0.265FE-03 0.365E-03 0.265FE-03 0.365E-03 0.265FE-03 
           4 2-0.5639240 0.75406204 0.27056303 0.2054633 0.28455603-0.504464004 0.26556440.04 0.1004635 0.6125603 0.3355608 0.1120631

5 1-0.33276304 0.5157634 0.14226503-0.64756402 0.14346603-0.3324604 0.173565040.02 0.73384604 0.5573603 0.14565040 0.3424630

6 1-0.31766404 0.45606474-0.27386407-0.44356402-0.28226402-0.31766404 0.15746404010 0.65496404 0.4240603 0.15566403 0.35166404 0.5566403 0.35166404 0.55666403 0.35166404 0.55666403 0.35166404 0.55666403 0.35166404 0.55666403 0.35166404 0.55666403 0.35166404 0.55666403 0.35166404 0.55666403 0.35166404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.5566640404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666404 0.55666
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                    1-0.7777F+03 0.2540E+54-0.17HbE+02 0.15n/E+00-0.17HbF+02-0.7778E+03 0.3A00E+030.00 0.3011E+04 0.5a14E+03 0.3021E+0/ 0.1595E+10 1-0.4424E+03 0.2302E+0/ 0.1540E+02-0.3017E+02-0.1350E+02-0.4444E+03 0.2407E+030.06 0.2590E+04 0.5474E+03 0.2235E+0/ 0.1140E+10
                   01+3051.0 10+31625.0 60+31610.0 40+32015.0 00.060+3075.0 60+3046.0-10+3076.0 00-60+3066.0 10+3056.0 60+3066.0-1

+00+30704.0 10+31661.0 60+3566.0 40+35665.0 01.060+3661.0 60+36061.0 60+36506.0 10-30406.0 10-30406.0 40+3661.0 60+36661.0 60+36661.0 60+36660.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-30406.0 10-304
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                    1-0.4284F+04 0.6018E+04 0.4447E+07-0.447E+07 0.4613E+03-0.474E+04 0.7184E+040.02 0.8467E+04 0.6044E+04 0.2676E+040.02 0.8676E+04 0.6044E+04 0.276E+040.07 0.1010F+05 0.5566E+03 0.3358+080 0.1034E+11 1-0.3441F+04 0.570E+040.07 0.1010F+05 0.5566E+03 0.3358+080 0.1034E+11 1-0.3441F+04 0.570E+040.07 0.7440E+04 0.5758E+03 0.3868E+080 0.4447E+11 1-0.3441F+05 0.5104E+04 0.5758E+03 0.5658E+080 0.4447E+11 1-0.3441F+05 0.5104E+04 0.5758E+03 0.5058E+080 0.4447E+11 1-0.3441F+05 0.5768E+080 0.5758E+080 0.57
                    1-0.3181E •04 0.4676E •04-0.417ME •02-0.49M9E •02-0.3922E •02-0.3184E •04 0.1572E •040.03 0.6652E •04 0.4643E •03 0.1554E •04 0.6682E •10 1-0.2262E •04 0.3465E •04 0.4642E •04 0.4642E •04 0.4652E •0
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### TABLE VIII. - Continued. SAMPLE PROBLEM (4) - OUTPUT

NEL	RC.	Z¢	£≓	ŁT	ΕZ	EHZ	LH	LZ	LT	LI	15	TL	15	TH	FaFA	NEL
1	1.07874		-0.0115a		-0.00014							0.00	-0.00		0.03440	1
2	1.1-409		-0.01040		-0.00014		0.9894					0.00	00.00		0.01751	2
3	1.3-3.5	00.00664			-0.00041							3.13	-0.00		0.01000	3
5	1.27035	00.13324			-0.000+1		0.4479					0.00	-00.00		0.0000	5
	1.5+203	00.00004			-0.000+t		0.7751					3.15	-0.00		0.01000	
. 6	1.74121	00.13327			-0.00048							3.12	-0.00		0.01000	6 7
ક	1.67474		-0.00370		-0.00048	0.00007						0.00	00.00		0.03000	8
	1.87414	00.06663			-0.00052							3.11	-0.00		0.03000	y
10	1.9+0-2	00.11326			-0.00053	0.00002						0.00	00.00		0.03000	1 ó
11	2.14017	Fancy. VO.		0.00319	-0.00054	-0.00005	0.9940	0.9995	1.0032	0.4995	0.9980	3.11	-0.00	00.00	0.0:000	Ti Ti
12	2.07354	30.13326	-0.00214		-0.00053							0.00	00.00	00.00	0.01000	12
13	2.27325	10.05663			-0.00054							3.10	-0.00		0.01000	13
14.	2.33952	00.13326			-0.00055							0.00	00.00		0.03000	. 14
15	2,53956	00.00003			-0.00056							3.08	-0.00		0.0:000	15
16_	2.472-17	_00.13326			-0.00055							0.00	-0.00		0.0:000	10
17	2.67275	30.00663			-0.00056							3.04	-0.00		0.0000	17
16	2.73935 2.93920	00.13326			-0.00056							3.11	0.00		0.0000	18
23	2.87257		-0.0005H -0.00073		-0.00055							3.13	-0.00		0.0:000	20
21	1.07874		-0.00073		-0.00012							3.14	-0.00		0.01433	21
22	1.1-470		-0.01030		-0.00014							3.11	-0.00		0.0:322	22
23	1.3-306	00.33323			-0.00043							3.12	-0.00		0.0.00	23
24	1.27605	10005.00			-0.00014							3.07	-0.00		0.0000	24
25	1.475-5		-0.00502		-0.00043							0.00	00.00		0.0:000	25
_ 26	1.54200	00.25654	-0.00460	0.00561	-0.00049	-0.00012	0.4954	0.9945	1.0057	0.9995	0.9954	3.11	-0.00	00.06	0.00000	26
_` 27	1.74121	00.33317	-0.00343	0.00452	-0.00050	0.00003	0.9966	0.9995	1.0045	0.9995	0.9966	0.00	00.00	00.00	0.01000	27
28	1.67479	00.26654			-0.000-9							3.11	-0.00	00.00	0.0000	28
29	1.57413	00.33316			-0.00050							0.00	00.00		0.01000	29
30	_l.9+052_	00.26653			-0.00052							3.11	0.00		0.01000	30
31	2.14017	00.33316			-0.00053							0.00	00.00		0.01000	اد
32	2.07354	00.26653			-0.00052							3.10	-0.00		0.0:000	32
33	2.27326				-0.00053							0.00	00.00		0.0:000	33
3 <del>4</del>	2.53995	30.26652	0.00154_ 0.0011H		-0.00054							3.10_	0.00_		0.01000	34
36	2.472-6	00.26652			-0.00054							3.13	-0.00 -0.00		0.00000	
37	2.67274	00.33315			-0.00055							3.13	-0.00		0.00000	36 37
. 36	2.73934	90.26652			-0.00055							3.03	-0.00		0.00000	31 38
39	2.93914	00.33315			-0.00057							3.12	-0.00		0.0000	34
40	2.87257		-0.00073		-0.00056							2.97	-0.00		0.00000	40
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1 00.47899E+02 00.44619E+02 00.92509	E+02 -0.24237E+03	2 00.47370E+02 0	0.32455E+02 00.79825E	+02 -0.72383E+03
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5 00.23913E+02 0.E+00 00.23913	E+02 00.65728E+03			*02 00.49Z0ZE+03
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11 00.57127E+01 0.E+00 00.57127	E+01 00.50418E+03			+01 00.59270E+03
13 00.4554/E+01 0.E+00 00.4554	E+01 00.50947E+03			+01 00.581435+03
15 00.31215E+U1 0.E+00 00.3121e	E+01 00.59794E+03	16 00.33977E+01		+01 00.61>28E+03
17 00.27377E+01 0.E+00 00.26389	E+01 00.63525E+03	18 00.24501E+01		·01 00.61727E+03
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21 00.450436+02 00.446176+02 00.92111	E+02 -0.19628E+03	22 00.47303E+02 0		*92 -0.67230E+03
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	E+02 00.57579E+03			*U2 00.48~28E+U3
	E+02 00.52610E+03			+02 00.57536c+UJ
	E+01 00.57709E+03			+01 00.542562+03
31 00.55963E+01 C.E+00 00.55963	E+01 00.55946E+03			+01 00.59:012+03
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2.606764 SAMPLE PRO  1 3-0.77 2 3-0.77 3 2-0.96 5 1-0.33 6 1-0.35 7 1-0.22 9 1-0.19 10 1-0.11 11 1-0.12 12 1-0.11 13 1-0.8	90.3 16EE4 3 16EE4 3 16EE4 4 16EE4 4 1	99757 EXPAN 0.52599 0.44066 0.50077 0.7106 0.52018 0.42656 0.42508 0.36140 0.3150 0.3150 0.3150 0.7708	E+04-( E+04 ( E+04 ( E+04 ( E+04-( E+04-( E+04-( E+04-( E+04-( E+04-( E+04-( E+04-( E+04-(	2,86656 OF A TH 52 0,147456 0,147466 0,134766 0,21226 0,45116 0,45116 0,4516 0,4516 0,2454 0,2454 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2456 0,2566 0,2566 0,2566 0,2566 0,2566 0,2566 0,2566 0,2566 0,2566 0,2566 0,2566 0,2566	+03 0 +03 0	0.399754  **ALL TUHE  \$\text{F+00} \ \$\text{\$-2006\text{\$\text{\$\circ}\$} \ \$\text{\$\circ}\$ \ \$\$\	3.6 STHE SI -0.1479E+1 -0.539E+1 0.1117E+1 0.3604E+1 0.4051E+0 -0.4051E+0 0.4038E+0 0.4038E+0 0.7932E+0 -0.2196+1 0.21048E+0 -0.2136+1 -0.2136+1	33-0.70 33-0.70 33-0.70 33-0.50 33-0.50 33-0.37 11-0.35 02-0.27 11-0.13 02-0.18	00.39975 MENT DATA  S12  006+04 0.3 006+04 0.2 72E+04 0.2 72E+04 0.2 13E+04 0.1 13E+04 0.1 13E+04 0.1 13E+04 0.4 13E+04 0.9 13E+04 0.6 13E+04 0.6 13E+04 0.6 13E+04 0.6 13E+04 0.6	3467E+04 3382E+04 570E+04 940E+04 230E+04 1748E+11 230E+04 1727E+63 9437E+03 3335E+03	0.00 0 0.04 0 0.04 0 0.04 0 0.04 0 0.02 0 0.02 0 0.02 0 0.02 0 0.02 0 0.03 0	1071E+ 1059E+ 1010E+ 1021E+ 4258E+ 7547E+ 5942E+ 6388E+ 5101E+ 4000E+ 4000E+ 33965E+ 4191E+ 3340E+	\$15-0.65 05-0.107 05-0.107 05-0.402 05-0.402 05-0.402 04-0.570 04-0.570 04-0.640 04-0.640 04-0.640 04-0.640 04-0.640	72E+0.3 76E+0.3 76E+0.3 37E+0.3 99E+0.3 97E+0.3 17E+0.3 13E+0.3 17E+0.3 17E+0.3 17E+0.3	0.362 0.372 0.373 0.334 0.347 0.191 0.117 0.196 0.867 0.768 0.523 0.585 0.410 0.410	7E+08- 2E+00 2E+00 7E+00 7E+00 7E+00 7E+00 7E+00 7E+07 7E+07 7E+07 7E+07	J3  -0.1936E- 0.199E- 0.1959E- 0.1956E- 0.195E- 0.195E- 0.978E- 0.978E	11 11 11 11 11 10 10 10 10
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04-0.7405 04-0.7405 04-0.7405 04-0.7405 04-0.7405 04-0.7405 04-0.7405 04-0.7405	72E+0.3 76E+0.3 37E+0.3 37E+0.3 37E+0.3 37E+0.3 37E+0.3 31E+0.3 31E+0.3 31E+0.3 31E+0.3 32E+0.3 33E+0.3 35E+0.3	J2  0.382 0.373 0.347 0.347 0.191 0.117 0.1367 0.191 0.170 0.523 0.410 0.523 0.471 0.274 0.275 0.209 0.1640 0.216	7E+08- 2E+00- 2E	J3 -0.1y36E* 0.1599E* 0.1590E* 0.178E* 0.178E* 0.378E* 0.378E* 0.378E* 0.378E* 0.378E* 0.378E* 0.378E* 0.103E* 0.103E* 0.103E* 0.103E* 0.103E* 0.103E* 0.103E* 0.103E* 0.103E* 0.110E* 0.110E* 0.110E* 0.110E*	11 11 11 11 11 10 10 10 10 10 10 10 10 1
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1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0 1502E+0	15 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1071E+ 1071E+ 1019E+ 1021E+ 1021E+ 258E+ 7597E+ 5388E+ 5101E+ 3905E+ 4900E+ 3394E+ 3394E+ 2599E+ 2506E+ 221E+ 221E+ 221E+ 2105E+	STE  S  U5-0.657 U5-0.107 U5-0.107 U5-0.107 U5-0.107 U5-0.107 U5-0.107 U4-0.552 U4-0.552 U4-0.602 U4-0	72E+0.3 76E+0.4 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12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13 12-0.13	00.39975 MENT DATA  S12  B2E-04 0.3  002-04 0.3  002-04 0.3  29E-04 0.2  87E-04 0.2  87E-04 0.1  13E-04 0.1  13E-04 0.1  13E-04 0.1  14E-04 0.1  14E-0	57 3407E + 04 3382E + 04 570E + 06 570E + 06 2001E + 04 1748E + 14 236E + 06 3375E + 0 3375E + 0 3476E + 06 4476E + 06 4476	10.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1071E+ 1071E+ 1059E+ 1010E+ 1059E+ 258E+ 7587E+ 5388E+ 6388E+ 6388E+ 4000E+ 33905E+ 2394E+ 1071E+ 10	STE  S  U5-0.657 05-0.107 05-0.507 05-0.507 04-0.712 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 04-0.57 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### TABLE VIII. - Continued. SAMPLE PROBLEM (4) - OUTPUT

SAMPL	E PROBLEM	T EXPA	NSION OF A	THICK WA	ALL TURE	51HA	IN ELEM	ENT DAT	A			STE	3 -	e or	•	
NEL	#C	žC.	EH	Eſ	ΕZ	ERZ	LR	LZ	LT	LI	rs	ŤL	TS	TH	Łŕta	NEL
1 2	1.08024 1.14608	00.13335	-0.01385 -0.01270	0.01106	F0000*0	0.00000	0.9875	1.0000	1.0112	1.0000	0.9875	0.00	-0.00	00.00	0.0Co45 0.0C442	1 2
3 4 ~ 5	1.27832	00.13331	-0.00710 -0.00456 -0.00554	9.00644	£00003	0.00010 01000.0	0.4415	1.0000	1.0090	1.0000	0.4415	3.12 0.00 3.11	-0.00 -0.00	00.00	0.00000	3 4 5
6 7 H	1.54275	00.00063	-0.00504 -0.00360 -0.00416	0.36530	-0.00057	0.00001 -0.00007 0.00006	0.4402	0.4494	1.0050	0.9994	0.4462	0.00 3.12 0.00	_00.00 _0.00	00.00	0.00000	6 7 8
- 10 - 11	1.87445 1.44141 2.14041	00.05663	-0.00310 -1+500.0-	0.00441	-0.00057	0.00007	0.4469 0.4471	0.9944	1.0044	0.9494	0.9969	3.11	-0.00	00.00	0.00300	9 10
. 12 13	2.07-39 2.273-7	00.00663	-0.00240 -0.001d4	0.00372 1'600.0	-0.00057 -0.00059	0.00008	0.9976 0.9982	0.4994	1.0037	0.4944 0.4444	0.4476	3.11 0.00 3.10	-0.00 -0.00	00.00	0.00300 0.00300	11 12 13
14 15 16	2.3+057 2.5+022 2.4736+	00.05663 00.13325	-0.00172 -0.00132 -0.00142	0.00271	-0.00061	-0.00000 -0.00005 -0.00000	0.9987 0.9986	0.4994	1.0027	0.7974	0.4987	3.14 3.07 3.14	-0.00 -0.00 -0.00	00.00	0.00100 0.00100 0.00100	14 15 16
17 18 19	2.67334 2.73949 2.93942	00.13325 00.00663	-0.00107* -0.00100 -0.00075	0.00242	-0.00001	-0.00002	0.9992	0.9994	1.0024	0.9994	0.9990 9.9492	3.04 3.10 2.80	-0.00 -0.00 -0.00	00.00 00.00	0.00000 0.00000 0.00000	17 18 19
21 21 22	2.87320 1.05025 1.14634	00.3333d	-0.00381 -0.01367 -0.01270	0.01250	0.00015	-0.00001 -0.00011 -0.00056	0.9666	1.0002	1.0127	1.0002	0.9606 0.9675	3.10 3.11 3.11	-0.00 -0.00 -0.00	00.00	0.00000 0.00527 0.00494	20 21 22
23 24 25	1.34+17 1.275,3 1.47656	00.2555	-3.00704 -0.00856 -9.00574	0.30845	0.00010	-0.00017 -0.00067 0.00012	0.9915	1.0001	1.0090	1.0002	0.9915	3.00	-0.00 -0.00 00.00	00.00	0.00300 0.00133 0.00300	23 ° 24 25
26 27 28	1.54245 1.74256 1.67567	00.33315	-0.0050→ -0.00388 -0.06412	100001	-0.00052	-0.00012 0.00006 -0.00007	0.9961	0.9995	1.0050	3.4995	0.9961	3.11 6.00 3.12	-0.00 00.00 -0.00	00.00	0.00000 0.00000	26 27 26
- 30 - 31	1.941-1	13.20551	-0.0031H -0.00291 -0.00224	0.00415	-0.00057	0.00005 -0.00006 0.00001	0.4971	0.9994	1.0042	0.9994	0.9971	0.00 3.12 0.00	00.00 -0.00	00.00	0.0000 0.0000 0.00100	39 30 31
32 33 34	2.07439 2.27346 2.34051	00.26651 00.33314	-0.00186 -0.00172	0.00372	-0.00057 -0.00057	-0.00007 0.00001 -0.00005	0.9976 0.9981	0.9994	1.0037	0.9994	0.9976	3.09 3.11	-0.00 00.00 -0.00	00.00	0.00000	32 33 34
35 36 37	2.54021 2.47353 2.67335	00.33313 00.26651	-0.00132 -0.00142 -0.00110	0.00270	-0.00000	-0.00001 -0.00006 -0.00001	0.9987	0.9994	I.0027	0.9994	0.9987 0.9986	3.13 3.07 3.13	-0.00 -0.00	00.00	0.00300 0.00300 0.00300	35 36 37
38 39 40	2.73944 2.93940 2.47319	00.26650 00.33313	-0.00100 -0.00075 -0.00081	0.00242 0.00230	20000.0- 20000.0-	-0.00005	0.4490 0.4993	0.9994	1.0024	0.4944	0,9990 0,9993	3.02 3.10 2.96	-0.00 -0.00 -0.00	00.00	0.00000 0.0000 0.0000	36 39 40
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3 5	00.443+1F 00.29857E 00.15498E	+02 0.E+	0000	.44391E+0 .29557E+0	2 00.5634 2 00.7130 2 00.570	45E+03	·	6 00.	.45311E-	•02 00.		2 00.5842		.40370£	•03 •03	
. 11	00.115/3E 00.7035#E 00.55990E	*02 0.E**	00 00	.115235+0 .70358£+0	2 00.6404 1 00.6094 1 00.663	2/E+03 41E+03		10 00	.10191E .78573E	02 0.	E+00 E+00 E+00	00.1019	16+02 00 16+01 00	.58504E	د0+ د0+	
<u>15</u> -	00.33259E 00.3236TE 00.24445E	+01 0.E+	00 00	.35?69E+0 .323015+0	1 00.652 1 00.6784 1 00.7154	+>E+03		16.00.	41673E 29976E 26003E	•010.	E+00 E+00 E+00	-00.4167 -00.2997	3E+v1 00 6E+v1 00	.67175c	÷03	
21 23	00.500292 00.44252E 00.30440E	+02 00.544 +02 0.84+	5025+02 00 00 00	.11453E+U .44262E+O		31E+03 31E+03		22 00. 24 00.	.49207E	.00 SO.	50454E+0.	2 00.9966 2 00.5087	1E+J2 -0	.10121£	+04 +03	
·27	00.15723E 00.11655E 00.70214E	+02 0.E+	00 00 00 00	.15723E+0 .11655E+0	2 00.540 2 00.614	10E+03 536+03		26 GO	17947E- 10185E- 78530E-	•02 0.	E+00 E+00		76+02 00 156+02 00	.617405	د0• د0•	
33 35	00.56036E 00.35131E 00.32251E	•01 0.E+:	00 00. 00 00	.56036E+0 .3H131E+0	1 00.651 1 00.657 1 00.678	2vE+03 74E+03		34 00. 36 00.	50695E 41632E 29922E	·01 0.1	E+00 E+00 E+00	00.5069	5E+01 00 2E+01 00 2E+01 00	.63222£	£0+ £0+	•
	00.243556				1 00.695							00.2595				

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THE ELASTIC EMERGY IS 00.129221E+03
THE PLASTIC EMERGY IS 00.30043-E+02
THE TOTAL EMERGY IS 00.165865E+03F3H A LOAD OF 00.215174E+05
THIS IS INCREMENT 3 - 2 OF 4
THE APPLIED LOAD IS $21517.3791F4E INC. LOAD IS 1599.4475
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SCALED STEP

STATE MAP	STEP 1	-	3							
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iii	iii	•	; ;		i					
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4.00Allu33	J.00000000	o	0.00705047	0.00000000	0.00727143	0.00000000	0.00699926	0.00000000	0.00677879	0.00000000
:.30002354	0.0000000	S	0.01500000	0.00005944	0.01734644	0.00002246	0.01060767	00000000	0.00756456	00010419
2.30-71742	0u011n/	•	U.00m1203n	u0ul174l	0.00762667	00015004	0.00727215	00012251	0.006+7405	0001256Y
3.00677203	0031250	4	0.00000445	00012220	0.01500000	0.00010723	0.01550115	0.00005935	0.01072950	00014084
<b>(.00454644</b>	000/153	0	0.00~75066		0.00#U4640	00023401	0.00763576	00023741	0.00725186	00024435
0.30647450	030/449	6	0.00675264							
	•				INCHEMENTAL	DISPLACEMENTS	. ,			
2.00051,464	0.0000000		0.00038971				0.00027471	0.00000000	0.00025049	0.00000000
0.00023124	<b>ე.</b> ეაიიიეი		0.00021661			0.0000000	0.00014640	0.0000000	0.00018967	0.00000000
C.00018497	0.0000000		0.00051954		0.00040460	0.00001613	0.00031019	0.00000489	0.000277-6	00000058
0.0CU25UJn	0000027		0.00023151			00000546	0.00020458	cososo303 ·	0.00019531	00000324
C.3001 page	0000032		0.00018393			0.00003937	0.00034420	0.00:03328	_ 0.00035104	6.00001933
C.00327483	0000024		0.00025305			00000541	0.00021008	00000553	0.00020300	00000598
C.30019501	0000062	7	0.00018779		0.00016316 INCREMENTAL	00000624 FORCES		• •	• •	
100.5	5.	4	-0.0	20.5		-8.3	-0.0	-20.7	-0.0	1.8
-0.0	5.		-0.0			3.0	-0.0	1.2	-0.0	-1.0
00.0	-9.		224.3			-0.0	0.0	00.0	00.0	-0.0
00.0	o		-0.0			00.0		-0.0	00.0	00.0
-v.ū	-0.		00.0	00.0		-0.0	00.0	-0.0	-0.0	-0.0
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00.0	-0.	0	00.0	00.0	-0.0	00.0				
					TOTAL	FORCES				
5138.9	104.	6	-0.0			-285.1	-0.0	-112.6	-0.0	44.0
-0.0	37.	7	-0.0			23.5	-0.0	13.7	-0.0	-25.3
00.0	-14û.	6	11837.2	00.0		-0.0	-0.0	00.0	00.0	-0.0
00.0	00.		-0.0			00.0	-0.0	-0.0	-0.0	00.0
÷0.0	-ij .		00.0	00.0		-0.0	-0.0	-0.0	-0.0	-0.0
00.0	-u.		00.0			-0.0	00.0	-0.0	00.0	00.0
00.0	-0.	0	00.0	00.0		00.0				
					NODAL	COORDINATES				
1.015000	0.00000		1.212155			6.000000	1.609526	0.000000	1.808748	0.000000
2.008110	0.00000		2.207650			0.000000	2.606999	0.000000	2.806779	0.000000
3.006624	0.00000		1.015000	00.200060	1.212392	00.200022	1.410608	00.199932	1.609565	00.199596
1.608713	60.19948		2.004120	00.199883	2.207027	00.199880	2.407272	00.199877	2.605979	00.199874
2.006772	00.19947		3.006654	00.199578	1.015000	00.400107	1.212201	00.400059	1.410729	90.399659
1.609549	00.19978		1.808751			00.399766	2.207636	00.399763	2.407252	00.399756
2.606980	00.39975		2.806753		3.006599	00.379750			3 3 OF	
SAMPLE PHUS	SCHM 3 EX	MANS	IUN UF A IMI	CK WALL TUHE		EMENT DATA		STEP	3 - 3 OF	4
					31ME 33 ELE	LUCIAL DATA				
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\$12 NEL TRY 1 3-0.724% + 94 0.51596 + 94 + 9.1560 £ + 93 0. £ + 90 - 0.1560 £ + 93 - 0.7240 £ + 94 0.3542 £ + 94 0.00 0.1077 £ + 95 + 95 - 9.745 £ + 93 0.3870 £ + 98 + 93 - 0.262 £ + 11 2 3 - 0.755 £ + 94 0.4545 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 94 0.4575 £ + 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0,475%-04-0,54436%-04-0,3170%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-0,475%-04-25 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1-0.41718-03 0.24718-04-0.4588-01-0.7428-01-0.73498-01-0.45188-03-0.47188-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-03 0.2478-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4518-01-0.4 35 1-0,3703E+03 0-710E+04 0-775E+01-0,6865E+01 0-7876E+01-0,499E+03 0-15386E+030-0,25778+04 0-696E+03 0-740E+07 0-1346E+10 0-745E+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-73378+04 0-1-0.1457L-01 0.7799E-04 0.1141E-07-0.775E-07 0.1640E-07-0.1507E-03 0.8774E-020.18 0.2370E-04 0.7716E-03 0.1871E-07 0.7706E-09

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### TABLE VIII. - Continued. SAMPLE PROBLEM (4) - OUTPUT

SAMPLE PROBLEM & EXPANSION OF A THICK WALL TUBE

STRAIN ELEMENT DATA

STEP 3 -

NEL	нс	7C	ER	ET_	€Z	ERZ	LR	LZ	LT	LI	rs	ŤL.	rs_	TH	EPEQ	MEL
1	1.08072		-0.01453	0.01292								0.00	-0.00		0.00705	1
2	1.14652		-0.01330	0.01143	1.00011		0.9870					0.00	00.00		0.60544	. 2
3	1.34448		-0.00744		-0.00034							3.15	-0.00		0.00034	3
	1.27839		-0.00904	0.00415	0.00011							3.11-	0.00		0.00171	
5	1.476-4		-0.00579		-0.00052							0.00	00.00		0.0000	6 1
6.	1.54323		-0.00324		-0.0005E							3.12	-0.00		0.0000	7
8	1.67544		-0.00426		-0.00056							0.00	00.00		0.0000	ä
9	1.87519		-0.00320		-0.00058							3.11	-0.00		0.10000	ÿ .
15	1.44105		-0.00300		-0.00059							0.00	00.00		0.00000	10
11	2.14113		-0.00231	0.00363	-0.00060							3,11	-0.00	-03.00	0.0000	. 11
12	2.07452	00.13325	-0.00c4H		-0.00059							0.00	00.00		0.10000	
13	2.27418		-0.00140		-0.00000							3.10	-6.00		0.0000	
14	2.34072		-0.0017s		-0.000p1							3.14	-0.00		0.0000	
15	2.54042		-0.00136		-0.00063							3.07	-0.00		0.10000	
16	2,473:14		-0.001+7		-0.00051							3,13	-0.00		0.0000	
17	2.67379		-0.00110		-0.00063							3.04	-0.00		0.10000	
.18	2.74014		-0.00104		-0.00063							3.10	<del>-</del> G.00		0.0000	
19	2.94000		-0.0007a		-0.00063							3.11	-0.00		0.0000	
. 23	2.87339		-0.01429		0.00024							3.13	-0.00		0.0000	
22	1.14653		-0.01330		0.00018							3.10	-ú.00		0.0547	
23	1.34451		-0.60744	0.00028	-0.00036	-0.00030	0.4926	0.9990	1.0084	0.4446	0.9925	3.11	-0.00		0.60035	
24	1.278-0		-0.00905		0.00018							3.06	-6.00		0.00175	
25	1.470+6		-0.00596		-0.00036							C.00	00.00	00.03	0.0000	ීදු
26	1.54324		-0.00526		-0.00056							3.11	-0.00	03.00	0.0000	26
27	1.74234	00.33315	-0.00402		-0.00053							0.00	00.00		0.60000	
28	1.67594	26992.00	-0.00426		-0.00056							3.12	-ú.00		0.00000	
. 59	1.87519	00.33314	-0.00324		-0.00053							0.00	00.00		<b>0.6000</b>	
30	1.94154		-0.00300		-0.00058							3,12	0.00_		0.0000	
31		~30.3331			-0.00059							0.00	00.00		0.00000	
32	2.07451		-0.00248		-0.00058							3.11	0.00		0.00000	
33```	2.27417		-0.00193		-0.00059							0.00	00.00		0.0000	
34	2.34072		-0.00175		-0.00061							3.09	-0.00		0.0000	
35	2.54040		-0.00136		-0.00062							3.13	-0.00 -0.00		0.0000	
36 37	2,473.3		-0.00147		-0.00061							3.07	-0.00		0.13000	36 37
3 <i>1</i> 38	2.67357 2.74017		-0.00114		-0.00064							3.02	-0.00		0.63000	38
39	2.93999		-0.00077		-0.00064							3.09	-0.00		0.00000	30
40	2.87339		-0.00084		-0.00004							2.96	-0.00		0.63000	
70		30.20030					¥ • / / / L									

ELE EL. EN. DEN PLS EN. DEN	TOT EN. DEN HYDRO. TENS.
1 00.506416+02 00.725305+02	06.12322E+03 -0.74578E+03
3 00.44631E+02 00.34295E+01	00.45061E+02 00.47042E+03
5 00.31776E+02 C.E+40	00.31776K+02 00.74267E+03
7 00.16445E+02 0.E+00	00.164456+02 00.583766+03
9 00.122275.62 0.6.00	00.122276+02 00.654976+03
11 00.746195+01 0.6+00	00.746192+01 00.622936+03
	00.59351E+01 00.67902E+03
13 U0.59351E+01 G.E+00	
15 00.405 156 +01 0.8 +00	00.405356+01 00.669146+03
17 00.341.76.01 0.6.00	00.341976+01 00.717246+03
19 00.258736+01 0.6+00	10+3+645.00 10+367H25.00
21 00.506926+02 00.705976+02	00.12120E+03 -0.59432E+03
23 00.44563E+U2 00.34747E+01	00.474826+02 00.514166+03
25 00.32526E+02 0.E+00	00.385258+02 00.602168+03
27 00.157256+02 0.6+00	00.16726E+02 00.54685E+03
29 00.12339E+02 0.E+00	00.123886+02 00.625276+03
31 00.74497E+01 0.E+00	00.744976+01 00.627456+03
	00.59419£+01 00.66601E+03
33 00.594136+01 0.6+00	
35 00.403556+01 0.6+00	00.403852+01 00.674196+03
37 00.34156E+31 0.E+00	00.34150E+01 00.69610E+03
39 00.257158+01 0.6+00	00.257156+01 00.715216+03

ε	LE EL. EN. DI	EN PLS EN. DE	N TOT EN. JE	HYU-O. TENS.
	2 00.49922E+0	2 00.557746+02	00.1057UE+03	-0.11761E+04
	4 00.45640E+0	2 00.17345E+02	UU.62486E+02	00.314336+03
	6"00.26702E+0	U.E+00	UU.20702E+U2	U0.57dc5E+U5
	8 00.19050E+02	2 0.E+00	00.190506+05	00.65175と+0.3
ı	0 00.10816E+U	2 0.5+00	00.10816E+02	00.5inosE+03
1	2 00.833576+0	1 0.E+C0	10+37c6600	00.65467E+03
ì	4 00.53787E+0	1 0.E+00	00.53/6/6+01	00.6-665€+03
ì	6 00.44149E+0.	0.E+00	06.441492+01	00.0:3576.03
1	8 60.317326+6.	0.£+00	00.31/32E+01	00.610016.00
5	0 00.27518E+0.	0.E+00	00.275188+31	00.72/JaE+03
5	2 00.49809E+0		00.10563E+03	-0.11C53E+04
5	4 00.45809E+07		2C+30F+F0.00	00.3:3556:03
2	6 00.26742E+0		UU.25742E+02	00.55349E+03
S	B 00.19071E+0.		00.19071E+32	00.635216.03
3	0 00.104105.00		00.109105.15	00.5532/6.03
	2 00.83312E+0.		00.03315E+31	00.650196+03
	4 00.53731E+0.		00.53731E+01	00.6-/026-03
_	6 CO.44104E+U.		00.44104E+01	00.657056+43
	8 00.31n73E+0.		00.31673E+01	00.670056+03
4	0 00.27459E+0.	1 0.E+00	00.27459E+01	00.7<155E+03

THE ELASTIC ENERGY IS THE PLASTIC ENERGY IS THE TOTAL EMERGY IS THE APPLIED LOAD IS

00.134217E+03 00.41M10bE+02 00.176087E+03F0M 4 LUAU UF 00.219494E+05 THIS IS INCKEMENT 3 - 3 UF 4 21979,18961HE INC. LUAD IS 411.0105

					TABLE VIII.	- Continued.	AMPLE PROBLEM	f (4) - OUTPUT	ı		
STATE MAP	STEP			ı							
<b>VIAI</b> (	512.	•		•							
3 3		3	1	1 1		1					
1 1	1 3	l J	5	1 1	1 1	1			•		
i i	ī	ī	ī	i i	i i	1	Discourage Contract				
0.01775741	3.300	00000		0.01-2140-	0.00000000	1014L 10.012327	DISPLACEMENTS.	0.01097771	0.00000000	0.010073a0	0.0000000
0.00733171	0.000			0.00H79531		0.008353/ 0.01453/		0.00803598 0.01224738	0.00000000°°°	0.00777987/ 0.01103098	0.00000000
0.01004064	000	13061		0.00434320	00013178	0.000700	300013565	0.00835217	00013840	0.00H00AAT.	
0.00776401 0.011029+2	000			0.00757446		0.017757		0.01432056	0.0002+553 00026641	0.01243406	0000d214 00027578
6.00000872					00028729	0.007565	200028747				
0.00275741	0.000	00000		0.3020625		INCREMENTAL 0.001053	DISPLACEMENTS	0.00145122	0.00000000	0.00132546	0.0000000
0.00122135	0.000			0.00114490		0.001001	4 0.00000000	0.00103672 17920106.0	0.00000000	0.00100168	00000000
v:00132275	000	01432		0.0015558				0.00105071	00001507	0.00103000	00001703
0.0009969H 0.00148J43	000	01701 01212		0.00097003				0.00211745	0.00018619	0.00170456	0.00005870
C.00102922	000		•	0.0009409	00003431	0.000900	100003275	***************************************			
562.3		28.0		-0.0	110.2	INCHEMENTAL 0	FOMCES 0 -44.1	-0.0	-113.2	-0.0	10.3
-0.0 00.0		28.7		-0.0 1177.e	14.1		U 16.7	-0.0 -0.0	6.3 00.0	-0.0	-8.7 -0.0
00.0		-53.5		-0.0	-0.0	-0.	00.0	00.0	-0.0	00.0	00.0
		-0.0						00.0 00.0	-0.0 -0.0	00.0	-0.0
00.0		-0.0		00.0		00.	0 00.0	****			
5701.2		132.6		-0.0		TOTAL -0.		-0.0	-225.8	-0.0	54.9
-0.0		66.4		-0.0 13014.c		-0. -0.		-0.0	20.0	-0.0	-34.0
00.0		00.0		-0.0	-0.0		0.00	-0.0	-0.0	-0.0	00.0
-0.0		-0.0 -C.0		00.0		5374		-0.0	-0.0		-0.0
00.0		-0.0		00.0							
1.017757		00000		1.214216		1.4123	0.000000	1,610978	0.000000	1.810074	0.000000
3.007500		00000 00000		1.017757		2.4083		2.608036	0.000000	2.807760	0.000000 00.199893
1.810041	00.1	99869		2.009343	00.199868	2.2067	7 00.199864	2.408352	00.199862	S.608010.	00.199857
2.807769		99857 9 <b>9773</b>		3.007574	00.399756			1.214321 2.208777	00.400246	1.412434 2.408327	00.399918 00.399724
2.608009		99718	NC 1 A	2.807744	00.399713 CK WALL TUBE	3.0075	5 00.399718		STEP		<u>4</u>
3417 66 11100	Jec., 3	£ 7			O	STRESS E	LEMENT DATA		5,2,		·
NEL IRV	SR	S	T	SZ	SRZ		5 512	TS SIGE	Q S	J2	J3
	<del>:</del>			<del></del>		S1 S				· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
1 3-0.807	74E+04 9JE+04	0.4632	Ë+04 E+04	-0.1980E+0	3 0.E+00 3 0.2777£+03	S1 -0.1980E+03-0.	8074E+04 0.3938E 8400E+04 0.3785E	+040.00 0.111 +040.04 0.109	1E+05-0,1213E+03E+05-0,1099E+	0.4113E+08	-0.4072E+11 -0.3343E+11
1 3-0.807 2 3-0.839 3 3-0.599	74E+04 9JE+04 54E+04	0.4632 0.4134 0.5959	E+04 E+04	-0.1980E+0 -0.8412E+0 -0.7809E+0	3 0.E+00 3 0.2777£+03 2-0.1255£+03	\$1 -0.1980E+03-0. -0.8310E+03-0. -0.7541E+02-0	8074E+04 0.3938E	+040.00 0.111 +040.04 0.109 +040.02 0.103	1E+05-0.1213E+0 3E+05-0.1649E+ 3E+05-0.2601E+	04_0.4113E+08 04_0.3976E+08 02_0.3552E+08	-0.4072E+11 -0.3343E+11 0.1849E+10
1 3-0.807 2 3-0.839 3 3-0.599 4 3-0.646 5 1-0.438	74E+04 99E+04 54E+04 67E+04 81E+04	0.4632 0.4134 0.5959 0.5618 0.6821	E+04 E+04 E+04 E+04	-0.1980E+0 -0.8412E+0 -0.7809E+0 -0.3022E+0	3 0.E+00 3 0.2777£+03 3 0.2777£+03 3 0.2241£+03 3-0.1551£+03	51 -0.1980E+03-0 -0.8310E+03-0 -0.7561E+02-0 0.8473E+03-0 0.4733E+03-0	8074E+04 0.3938E 8400E+04 0.3785E 5962E+04 0.2943E 0469E+04 0.3419E 4586E+04 0.2529E	+040.00 0.111 +040.04 0.105 +040.02 0.105 +040.03 0.105 +040.03 0.945	1E+05-0.1213E+0 33E+05-0.1699E+1 32E+05-0.2601E+1 50E+05-0.1606E+1 9E+04-0.9028E+1	0.4113E+08 04 0.4113E+08 04 0.3976E+08 02 0.3552E+08 03 0.3669E+08	-0.4072E+11 -0.3344E+11 0.1849E+10 -0.1703E+11 0.1409E+11
1 3-0.807 2 3-0.836 3 3-0.599 4 3-0.646 5 1-0.436 6 1-0.426 7 1-0.306	74E+04 99E+04 54E+04 67E+04 81E+04 33E+04 37E+04	0.4632 0.4134 0.5959 0.5616 0.6821 0.6169	E+04 E+04 E+04 E+04 E+04	-0.1980E+0 -0.4412E+0 -0.7809E+0 0.3022E+0 0.4485E+0 0.4422E+0	3 0.E+00 3 0.2777£+03 2-0.1255E+03 3 0.2241E+03 3-0.1551E+03 2-0.2516E+02 2-0.63+3E+02	\$1 -0.1980E+03-0. -0.8510E+03-0. 0.3695E+03-0. 0.4733E+03-0. 0.4437E+02-0.	8074E+04 0.3938E 8400E+04 0.37d5E 5902E+04 0.2943E 0469E+04 0.2529E 4580E+04 0.2529E 4233E+04 0.213yE	+040.00 0.111 +040.04 0.109 +040.02 0.103 +040.03 0.105 +040.03 0.949 +040.01 0.905 +040.01 0.905 +040.02 0.703	11E+US-0.1213E+U 13E+US-0.1699E+U 13E+US-0.2601E+U 10E+US-U.1606E+U 10E+US-U.1606E+U 10E+US-U.1606E+U 10E+US-US-US-US-US-US-US-US-US-US-US-US-US-U	04 0.4113E+08 04 0.3976E+08 02 0.3552E+08 03 0.3669E+08 03 0.273E+08 03 0.273E+08	-0.4072E+11 -0.3344E+11 0.1849E+10 -0.1409E+11 0.1609E+11 0.1609E+11 0.1137E+11
1 3-0.807 2 3-0.836 3 3-0.599 4 3-0.646 5 1-0.426 7 1-0.306 8 1-0.336	74E+04 90E+04 54E+04 67E+04 81E+04 33E+04 30E+04	0.4632 0.4134 0.5959 0.5616 0.6821 0.6169 0.5041 0.5435	E+04 E+04 E+04 E+04 E+04 E+04	-0.1980E+0 -0.412E+0 -0.780YE+0 -0.302ZE+0 -0.408SE+0 -0.503E+0 -0.104ZE+0	3 0.E+00 3 0.E+00 3 0.2777£+03 2-0.1255E+03 3 0.2241E+03 3-0.1551E+03 2-0.6343E+02 2-0.6343E+02 3 0.5747E+02	\$1 -0.1960E+03-0 -0.8310E+03-0 -0.7541E+02-0 0.3095E+03-0 0.4733E+03-0 0.443E+03-0 0.465E+02-0 0.1651E+03-0	8074E+04 0.3938E 8400E+04 0.3785E 5962E+04 0.2943E 0.469E+04 0.3117E 4586E+04 0.2523E 4233E+04 0.2134E 33032E+04 0.1142E 3301E+04 0.1763	*040.00 0.111 *040.04 0.109 *040.02 0.105 *040.03 0.405 *040.01 0.409 *040.02 0.707 *040.02 0.707	11E+05-0.1213E+03E+05-0.1213E+03E+05-0.1049E+04026E+04026E+040633E+040633E+040633E+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+04068+0	04 0.4113E+08 04 0.3976E+08 02 0.3552E+08 03 0.3669E+08 03 0.3264E+08 03 0.2733E+08 03 0.1666E+08	-0.4072E+11 -0.334dE+11 -0.1849E+10 -0.1903E+11 -0.1609E+11 -0.1600E+11 -0.1137E+11
1 3-0.807 2 3-0.807 2 3-0.809 3 3-0.606 5 1-0.402 7 1-0.30 8 1-0.33 9 1-0.235	74E+04 99E+04 54E+04 67E+04 81E+04 33E+04 00E+04 67E+04 31E+04	0.4632 0.4134 0.5959 0.5618 0.6821 0.6169 0.5041 0.5435 0.4543	E+044 E+044 E+044 E+044 E+044 E+044 E+044	-0.1980E+0 -0.412E+0 -0.780YE+0 -0.302ZE+0 -0.468E+0 -0.462ZE+0 -0.5003E+0 -0.4170E+0 -0.5120E+0	3 0.E+00 3 0.2777E-03 2-0.1255E+03 3 0.2241E+03 3-0.1551E+03 2-0.2515E+02 2-0.6343E+02 3 0.5747E+02 2 0.1441E+02	\$1 -0.1980E+03-0 -0.8310E+03-0 -0.7541E+02-0 0.3695E+03-0 0.4732E+03-0 0.4856E+02-0 0.1051E+03-0 0.5907E+01-0	8074E+04 0.3938E 8440E+04 0.3785E 5962E+04 0.2943E 0469E+04 0.3414E 4586E+04 0.2523E 4233E+04 0.2134E 3302E+04 0.1144E 3301E+04 0.1146E 2234E+04 0.1160E	*040.00 0.111 *040.04 0.100 *040.02 0.101 *040.03 0.105 *040.01 0.905 *040.02 0.700 *040.02 0.700 *040.02 0.700 *040.03 0.600 *040.03 0.600	11E+05-0.1213E+0 32E+05-0.1049E+0 32E+05-0.2001E+1 32E+05-0.1006E+1 32E+04-0.4024E+1 32E+04-0.5034E+1 32E+04-0.7034E+1 32E+04-0.7034E+1 32E+04-0.7034E+1 32E+04-0.7034E+1	04 0.4113E+08 04 0.3552E+08 03 0.3669E+08 03 0.3664E+08 03 0.2733E+08 03 0.193E+08 03 0.1228E+08 03 0.1228E+08	-0.4072E+11 -0.3343E+11 -0.1847E+10 -0.1903E+11 0.1409E+11 0.1608E+11 0.157E+11 0.159E+11 0.1592E+10 0.7375E+10
1 3-0.807 2 3-0.843 3 3-0.599 4 3-0.645 5 1-0.426 7 1-0.303 8 1-0.333 9 1-0.235 10 1-0.226 11 1-0.152	74E+04 99E+04 54E+04 54E+04 81E+04 33E+04 30E+04 54E+04 54E+04 81E+04 81E+04	0.4632 0.4134 0.5959 0.5618 0.6821 0.6169 0.5435 0.4543 0.4543 0.4543	E+044 E+044 E+044 E+044 E+044 E+044 E+044 E+044	-0.1980E+0 -0.4412E+0 -0.7307E+1 0.4685E+0 0.462E+0 -0.5003E+0 0.4176E+0 -0.5120E+0 -0.176E+0 -0.555E+0	3 0.E+00 3 0.2777E-03 3 0.2241E+03 3 0.2241E+03 3-0.1551E+03 2-0.2510E+02 2-0.63+3E+02 3 0.5747E+02 2 0.1441E+02 2 0.1554E+02 1 0.1470E+02	51 -0.1960E+03-0 -0.4510E+03-0 -0.7541E+02-0 0.3695E+03-0 0.4733E+03-0 0.4437E+02-0 -0.4866E+02-0 0.5907E+01-0 -0.5907E+01-0 -0.3978E+02-0	8074E+04 0.3938E 8440E+04 0.37455 5962E+04 0.2943E 0469E+04 0.33414 4586E+04 0.25294 4233E+04 0.21394 3032E+04 0.11492 3301E+04 0.11703 2231E+04 0.1090E 1547E+04 0.7736E	*040.00 0.11i *040.04 0.10i *040.02 0.10i *040.03 0.10i *040.03 0.90i *040.01 0.40i *040.01 0.40i *040.01 0.57i *040.01 0.57i *040.03 0.60i	11E+05-0.1213E+03E+03E+05-0.1213E+03E+05-0.2001E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.500E+05-0.50	04 0.4113E+08 04 0.3976E+08 02 0.3552E+08 03 0.3669E+08 03 0.3233E+08 03 0.3233E+08 03 0.1658E+08 03 0.1228E+08 03 0.1228E+08 04 0.1228E+08 05 0.7407E+07 06 0.7407E+07	-0.4072E+11 -0.3343E+10 -0.1849E+10 -0.1849E+11 0.1849E+11 0.1869E+11 0.1869E+11 0.1219E+11 0.855E+10 0.557E+10 0.567E+10
1 3-0.807 2 3-0.893 3 3-0.599 4 3-0.699 5 1-0.492 7 1-0.303 9 1-0.233 9 1-0.233 11 1-0.152 12 1-0.171	74E • 04 99E + 04 54E + 04 54E + 04 81E + 04 31E + 04 52E + 04 52E + 04 17E + 04 74E + 04	0.4632 0.4134 0.5959 0.5821 0.6169 0.5041 0.5435 0.4257 0.4257 0.3902	E+044 E+044 E+044 E+044 E+044 E+044 E+044 E+044 E+044	-0.1980E+0 -0.4612E+0 -0.7607E+0 0.302E+0 0.4642E+0 -0.503E+0 0.4176E+0 -0.5176E+0 -0.5176E+0 -0.5176E+0 -0.5176E+0	3 0.E+00 3 0.E+00 3 0.2777E+03 3 0.2241E+03 3 0.2241E+03 2-0.6343E+02 2-0.6343E+02 1-0.6389E+02 2 0.1941E+02 2-0.5558E+02 1 0.1470E+02 1 0.1470E+02 1 0.1470E+02	\$1  -0.1980E+03-0 -0.8310E+03-0 -0.7541E+02-0 0.3695E+03-0 0.4733E+03-0 0.4733E+02-0 0.1051E+03-0 0.5907E+01-0 -0.5102E+02-0 -0.3978E+02-0 -0.3438E+01-0 0.852E+01-0	80746+04 0.39386 84006+04 0.37355 59026+04 0.29438 04696+04 0.3252+ 42336+04 0.21345 42336+04 0.11426 30316+04 0.1763 23346+04 0.1160 23346+04 0.1160 15476+04 0.77366 17176+04 0.85696	*040.00 0.111 *040.04 0.105 *040.02 0.103 *040.03 0.105 *040.03 0.9d5 *040.01 0.905 *040.02 0.706 *040.03 0.606 *040.03 0.606 *040.03 0.606 *040.03 0.606 *040.03 0.606	11E+05-0.1213E+035E+035E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.1201E+05-0.120	04 0.4113E-08 04 0.4976E-08 02 0.3552E-08 03 0.3669E-03 03 0.366E-03 03 0.2733E-03 03 0.1238E-03 03 0.1238E-03 03 0.7407E-07 03 0.2796E-07	-0.4072E-11 -0.3349E-11 -0.3349E-10 -0.1403E-11 -0.1403E-11 0.1608E-11 0.1608E-11 0.1219E-11 0.8552E-10 0.7376E-10 0.5049E-10 0.5071E-10
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109E+04 0.5926E 109E+04 0.5926E 109E+04 0.5926E 109E+04 0.3747E 7404E+03 0.3937E 7404E+03 0.3937E 7404E+04 0.3747E	*040.00 0.111 *040.04 0.101 *040.04 0.102 *040.03 0.102 *040.03 0.903 *040.02 0.702 *040.03 0.607 *040.03 0.607 *040.03 0.607 *040.03 0.607 *040.03 0.607 *040.03 0.607 *040.03 0.607 *040.03 0.607 *030.04 0.412 *030.01 0.392 *030.07 0.346 *030.01 0.308 *030.07 0.346 *030.01 0.308 *030.07 0.346 *030.01 0.308 *030.06 0.292 *020.27 0.266 *020.27 0.266 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.04 0.103 *040.05 0.304 *040.06 0.504 *040.07 0.305 *040.07 0.335 *040.07 0.335 *040.07 0.335	11E+05-0.1213E+03E+05-0.1213E+03E+05-0.1213E+05E+05-0.2001E+05E+05E+06-0.2001E+05E+05E+06-0.200E+05E+06-06-06-06-06-06-06-06-06-06-06-06-06-0	04 0.4113E-08 04 0.4113E-08 06 0.4976E-08 07 0.4976E-08 08 0.4976E-08 09 0.352E-08 09 0.264E-08 09 0.1264E-08 09 0	-0.4072E+11 -0.3343E+11 -0.3343E+11 -0.1849E+10 -0.1409E+11 -0.1609E+11 -0.1609E+11 -0.1509E+10 -0.552E+10 -0.552E+10 -0.5539E+10 -0.535E+10 -0.151E+10 -0.151E+10 -0.151E+10 -0.151E+10 -0.151E+10 -0.151E+10 -0.151E+10 -0.151E+10 -0.151E+10 -0.201E+11 -0.153E+11

1-0.34515+0.3 0.2746F-04-0.12875+03-0.4946+02-0.6366E+01-0.3916E+03 0.1976E+030.13 0.2964E+04 0.7027E+03 0.2926E+07 0.1624E+10 1-0.1209E+03 0.2564E+07 0.673E+03 0.2926E+07 0.1624E+10 1-0.1209E+03 0.2564E+04 0.7173E+03 0.2234E+04 0.7173E+03 0.2234E+03 0.123E+10 1-0.1787F+03 0.2673E+04 0.7173E+03 0.2465E+07 0.1465E+10 1-0.1787F+03 0.2720E+04 0.730E+03 0.2465E+07 0.1465E+10 0.703E+03 0.2465E+07 0.787E+03 0.2465E+07 0.2465E+0

### TABLE VIII. - Continued. SAMPLE PROBLEM (4) - OUTPUT

SAMPLE PROBLEM 3 EXPANSION OF A THICK WALL TUBE

STRAIN ELEMENT DATA

STEP 4 - LOF

NEL	HC .	_/C	ER	ΕŤ	εz	ERZ	LR	LZ	LT		rs	TL	75	TR	EPEQ	_NE
. 1	1.08324	00 06673	-0.01818	0 01519	. 0.00035	0.0000	1 A. GA23	1.0009	170155	1.0009	0.9823	0.00	-0.00		0.01039	·- 1
	1.14804		-0.01050		0.00056							0.00	00.00		0.00033	
	1.34676	00.06665	-0.00959		-0.00020							3,12	-0.00		0.00225	
	1.240.13		-0.01165	0.01062	0.00056	0.0004	3 0.9886	1.0006	1.0108	1.0000	0.9886	0.00_	00.00		0.00+13	_ :
	T.47852		-0.00682		-0.00020							3.11	-0.00		0.0000	_ :
	1.544/5		-0.00014		-0.00054							. 3.14 3.12	-0.00		0.0000	!
	1.677.35		-0.00-94		-0.00054							0.00	00.00		0.00000	
	1.87648		-0.00373		-0.00065							3.11	-0.00		0.00000	
10	1.44241		-0.00351	0.00441	-0.00066	0.0000	3 0.9965	0.4493	1.0050	0.4993	0.9965	0.00	00.00		0.00000	10
	5.1.510		_0.00500		-0.00068							3.11	-0.00		.0.0000	1
	2.075+1		-0.00540		-0.00000							0.00	_ 00.00		0.00000	1
13	2.27531 2.34142		-0.00223	0.00379	-0.00068	-0.0000	0.4478	0.9993	1.0038	0.9993	6.9978	3.09	-0.00		0.0000	1
	2.54147		-0.00154	0.00362	-0.00071	-0.0000	7 0.34n4	0.9993	1.003	0.4943	0.9984	3.07	-0.00		0.00000	i
16	2.47441		-0.00172	0.00332	-0.00069	-0.0000	0.9983	0.9993	1.0033	0.4993	0.9983	3.13	-0.00		0.00000	ī
	2.67401		-0.00124		-0.00071							3.03	-0.00	00.00	0.00000	_1
ls	2.74119	00.1332+	-0.00121		-0.00072							3.08	-0.00		0.00000	. 1
	2.94098		-0.00090		-0.00069							2.67	-0.00		0.00000	1
	2.87437		-0.00097		-0.00072							- 3.09	-0.00		0.0000	- 2
	1.08328		-0.01764		0.00071 0.00066							3.13	-0.00		0.00993	2
	1.14847		_0.01650 _0.00957	0.01343	-0.00021	-0.0007	0.9906	0.9994	1.009#	0.9998	0.9906	3.10	-0.00		0.00231	_5
24	1.28037		-0.01105	0.01064	0.00005	-0.00094	0.9866	1.0007	1.0106	1.0007	0.9885	3.07	-0.00		0.00419	2
	1.47857		-0.00710	0.00402	-0.00021	11000.0	0.4430	0.9998	1.0001	0.4948	0.9930	0.00	00.00		0.00000	ě
	1.54477		-0.00014		-0.00060							3.11	-0.00		0.00000	2
27	1.74372		-0.00474		-0.00057							0.00	00.00		0.00000	5
	1.67737		-0.00499		-0.00060							3.13	-0.00		0.00000	- 2
	1.87648		-0.00386	0.00522	-0.00057	0.0000	0.9961	0.9994	1.0053	0.9994	0.9961	0.00	-0.00		0.0000	2
	2.14229		-0.00351 -0.00271	0.00491	-0.00065 -0.00065	0.00000	6.4473	0.9993	1.0047	0.9993	0.9973	- 3.12	00.00		0.00000	نڌ 3
	2.075#1		-0.60290	0.00439	-0.00065	-0.00000	0.9971	0.9993	1.0044	0.9993	0.9971	3.11	-0.00		0.00000	3
	2.27529		-0.00226	0.00378	-0.00065	0.00000	0.9977	0.9993	1.0038	0.9993	0.9977	0.00	60.00		0.00000	د ``
14	2.34142	00.26648	-0.0020H	0.00362	-0.00069	-0.00007	0.9979	0.9993	1.0036	0.9993	0.9979	3.09	0.00_		0.00000	_3
35	2.54145	00.33310	-0.00154	0.00319	-0.00070	-0.00002	0.9964	0.9993	1.0032	0.9993	0.9984	3,12	-0.00		0.00000	_3
.36	2.47440	00.26648	-0.00172	0.00335	-0.00069	-0.00007	0.9983	0.9993	1.0033	0.4993	0.9983	_ 3.07	-0.00		0.00000	3
	2.67459	00.33310	-0.00133	0.00296	-0.00070	-0.00000	0.9987	0.9993	1.0020	0.9993	0.9987	3.12	-0.00		0.00000	3
	2.74117		-0.00099	0.00286	-0.00072	-0.00000	0.9491	0.9993	1.0025	0.9993	0.9991	3.07	-0.00		0.00000	٠ 3
	2.87436		-0.00097	0.00257	-0.00072	-0.0000	0.4940	0.9993	1.0027	0.4943	0.9990	2.95	-0.00		0.0000	4
1 0 3 0 5 0 11 0 13 0 15 0 17 0 21 0 23 0 25 0 27 0 29 0 31 0 33 0	00.543-4E 00.461-2F 00.219186 00.19186 00.921-66 00.737-4E 00.535-96 00.34070E 00.538-7E 00.538-7E 00.444-01E 00.22561E 00.927-4E	02 00.10 02 00.27 02 0.54 02 0.54 03 0.54 04 0.54 05 0.54 06 0.54 07 0.54 08 0.54 09 0.54 0	000 000 000 000 000 000 000 000 000 00	1.16289E+( 1.6289E+( 1.6293E+( 1.16293E+( 1.16293E+( 1.78744E+( 1.78744E+( 1.78744E+( 1.78744E+( 1.78744E+( 1.16744E+( 1.1674E+( 1.2661E+( 1.2661E+( 1.274E+( 1.78961E+( 1.78961E+( 1.78961E+( 1.78961E+(	3 -0.121 2 -0.260 2 00.902 2 00.903 2 00.731 11 00.653 11 00.752 11 00.754 11 00.816 13 -0.935 2 00.316 2 00.579 2 00.670 10 0.694 11 00.694	33E+04 10E+02 34E+03 54E+03 64E+03 47E+03 07E+03 26E+03 41E+03 97E+03 97E+03 97E+03 26E+02 17E+03 26E+03 26E+03 27E+03		2 00 4 00 8 00 10 00 12 00 14 00 16 00 20 00 22 00 24 00 28 00 30 00 32 00 32 00 33 00 34 00	.53525E .47772E .35794E .25537E .14429E .11100E .58414E .41835E .36226E .33311E .47925E .35884E .25587E .11095E .71247E	02 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	E+00 E+00	00.140 00.899 00.255 00.144 00.111 00.713 00.418 00.462 00.407 00.368 00.907 00.358 00.255	35E+03 - 34E+02 - 34E+02 - 34E+02 - 34E+02 - 34E+01 - 35E+01 - 35E+01 - 35E+01 - 35E+01 - 35E+01 - 35E+02 - 35E+02 - 35E+02 - 36E+02 - 36E	-0.109926 -0.109573 00.05993 00.746546 00.767146 00.723266 00.775716 00.775716 -0.15926 -0.15926 00.71936 00.71936 00.71936	+ ( 4	
35 (	0.533h7E			.53.367E+(					.58345E		E+00			00.77701		
				).45058E+(					.41740E		E+00			00.732651		
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37 0 39 0 THE EL	0.3301 <u>36</u>	ERGY IS	00 2374		•02'									·- ; / ·		

"SCALED STEP

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                                                          | 51<br>-0.19<br>-0.64<br>-0.11<br>-0.37<br>-0.50<br>-0.46<br>-0.10<br>-0.10<br>-0.52<br>-0.40<br>-0.32<br>-0.32<br>-0.32                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      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|    | 2.66 SAMPLI TO THE TO T | 08155<br>E PRO<br>0.8150<br>-0.650<br>-0.650<br>-0.650<br>-0.600<br>-0.334<br>-0.246<br>-0.324<br>-0.1670<br>-0.171<br>-0.171                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           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3.007<br>STRESS<br>34E+03-(<br>59E+03-(<br>17E+03-(<br>31E+02-(<br>46E+02-(<br>44E+01-(<br>34E+02-(<br>77E+02-(<br>60E+02-(<br>66E+02-(<br>66E+02-(<br>66E+02-(<br>66E+02-(<br>66E+02-(<br>66E+02-(<br>66E+02-(                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 702<br>ELE<br>0.81<br>0.60<br>0.45<br>0.46<br>0.43<br>0.30<br>0.30<br>0.33<br>0.30<br>0.33<br>0.30<br>0.33<br>0.30<br>0.33<br>0.30<br>0.33                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                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                                                                                                                                                                                                                                                                                                                 | 713<br>A<br>2<br>3999E<br>3432E<br>2981E<br>25894E<br>21525<br>1743E<br>11525<br>17417E<br>5400<br>5440E                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              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|    | 2.66 SAMPLI TO THE TO T | 08155<br>2 PRO<br>0.81<br>0.650<br>0.650<br>0.40<br>0.22<br>0.22<br>0.21<br>0.21<br>0.21<br>0.71<br>0.74<br>0.74<br>0.74                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                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|    | 2.66 SAMPL  1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 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                        | 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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 0.4360; 0.4360; 0.4370; 0.4370; 0.4170; 0.1437; 0.1276; 0.770; 0.770; 0.3740; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 0.4775; 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SAMPLE PROBLEM 3 EXPANSION OF A THICK WALL TUBE

STRAIN ELEMENT DATA

STEP 4 - 2 OF

NEL	RC	ZC	ER	ET	ΕZ	ERZ	LR	LZ	LT	LI	L2	TL.	TS	TR	EPEQ	NEL
1			-0.01875									0.00	-0.00		0.01088	. 1
	1.14913		46410.0-			0.00000						0.00	00.00		0.0075	2
3	1.34652	00.06665				0.00043						3.12	-0.00		0.0252	3 4
	1.47875	00.13336	-0.01207									0.00 3.11	-0.00		0.0000	
6	1.54447	00.13329				-0.000071						3,13	-0.00		0.0000	6.
· · · · · · · · · · · · · · · · · · ·	1.74349	00.06662				-0.00004						3.12	-0.00		0.0000	. 7
ė	1.67755	00.13325				0.00000						0.00	00.00		0.(0000	ė
·	1.87007	00.00662				-0.00009						3,11	-0.00		0.:0000	٠ ټ
10	1.94308	00.13324				0.00003						0.00	00.00		0.10000	10
$\neg \Gamma$	2.1-245	500n0.0u	-0.00275	0.00425	-0.00069	-0.00007	0.9973	0.9993	1.0043	0.9493	0.9973	3,11		-00.00	0.4000	_11_
12	2.07548					0.00002						0.00	00.00		0.0000	12
13	2.275+n	20000.00				-0.00007						3,09	-0.00		0,0000	13
_14	_2.34178	00.13324				-0.00001						3,13	-0.00		00000	14
15	2.54162		-0.00162									3.07	-0.00		0.0000	15
<u> 16</u>	2.47516	00.13324				-0.00001						3,13	-0.00		0.0000	10
77	2.67475	20900.00				-0.00007						3,03	-0.00		J. :0000	17
. 18	_2.741.33					-0.00003						3.08	-0.00		0.00000	19 
19 20	2.94[12		-0.00042			-0.00007						2.87	~0.00		0.0000	
-21	_ 2.47451_					-0.00052						- 3.13			0.1000	
55	1.04365	00.26687	-0.01511			-0.00076						3.10	-0.00 -0.00		0.(0079	22
23	1.34660	00.31339				-0.00036						3,10	-0.00		0.10258	23
24		30.26679		0.01087		-0.00097						3.07	-0.00		0.00453	
-25	1.47660		-0.00735									0.00	-00.00		0.10022	
26		00.26654				-0.00014						3,11	-0.00		0.10000	
-27	1.74342	00.33313				0.00004						0.00	00.00		0.0000	
28	1.67757	00.26651				-0.00007						3.13	-6.00		0.0000	28
29	1.87657	00.33312	-0.00395			0.00007						0.00	00.00	00.00	0.0000	29
30	1.943.8	00.25649	-J.0035H	0.00500	-0.00066	-0.00007	0.9964	0.9993	1.0050	0.9993	0.9964	3.12	-0.00	00.00	0.60000	30
- 31	~2.14245	T00.33311	-0.00277	0.00425	-0.00066		0.9972	0.9993	1.0043	0.4993	0.9972	0.00	00.00	00.00	0.60000	~31 °°
32	2.0/578	00.25649				-0.0000A						3,11	-0.00		0.60000	32
33		00.33310				0.00000						0.00	00.00		0.0000	33
34	2.341 77	U0.26648				-0.00007						3.09	-0.00		0.60000	_ 34
35	2.54150	10.33310				-0.00002						3,12	-0.00		0.0000	35
36	2.475.5	00.26648				-0.00004						3.0/	-0.00		0.10000	.36
37	2.67473	00.33309				-0.00002						3.11	-0.00		0.0000	37
38	2.741.52					-0.00067						3.01	-0.00		0.0000	38
39	2.94110	00.33309				-0.00001						3.07	-0.00		0.0000	39
40	E.8/457	00.26647	-0.00099	0.002/2	-0.00073	-0.00005	0.4440	0.9993	1.0027	0.9993	0.9990_	2.95	-0.00	00.00	0.0000	40

ELE EL. EN. DEN PLS EN. DEN TOT EN. DEN HYDRO. TENS.	ELE EL. EN. DEN PLS EN. DEN TOT EN. DEN HYDRO. TENS.
1 00.54922E+02 00.11400E+03 00.16892E+03 -U.12767E+04	2 00.54057E+02 00.91082E+02 00.14514E+03 -0.1765+E+04
3 00.464352+02 00.25526E+02 00.71461E+02 -0.102842+03	4 00.48095E+02 00.45708E+02 00.93804E+02 -0.22853E+03
5 00.447155+02 0.5+00 00.447156+02 00.923856+03	6 00.37250E+02 0.E+00 00.37250E+02 00.65327E+03
7 00.227775+92 0.6+00 00.227775+00 00.662326+03	8 00.265562+02 0.2+00 00.265562+02 00.755442+03
9 00.169305+02 0.6+00 00.169306+02 00.742116+03	10 00.14994E+02 0.E+00 100.14994E+02 00.65594E+03
11 00.10304E+02 0.E+00 00.10304E+02 00.70281E+03	12 00.11530E+02 0.E+00 00.11530E+02 00.73699E+03
13 00.817418+01 6.8+00 00.817418+01 00.773548+03	14 00.740408+01 0.8+00 00.740408+01 00.733698+03
15 00.55594E+01 C.E+00 00.55594E+01 00.76593E+03	16 00.60607E+01 0,E+00 00.60607E+01 00.75775E+02
17 00.467%92+91 0.8+00 00.467898+01 00.830262+03	18 00.433d1E+01 0.E+00 00.433d1E+01 00.e040+E+03
19 00.353238+01 0.6+00 00.353236+01 00.862496+03	20 00.37559E+01 0.E+00 00.3/559E+01 00.6~558E+03
21 00.342786.02 00.108/56.03 00.163056.03 -0.966196.03	22 00.53823E+02 00.91504E+02 00.14533E+03 -0.15513E+04
23 00.453236.02 00.261176.02 00.724406.02 -0.162446.02	24 00.482432+02 00.463992+02 00.946422+02 -0.1133-2+03
25 00.446365+02 00.217545+01 00.463115+02 00.659696+03	26 00.373466.02 0.6.00 00.373466.02 00.614696.03
27 00.23434E+02 0.E+00 UC.23438E+02 00.55779E+03	28 00.26608E+02 0.E+00 00.26608E+02 00.75608E+03
29 00.173y0£+02 C.E+00 00.1730UE+02 00.68665E+03	30 00.14985E+02 0.E+00 00.14985E+02 00.658/7E+03
31 00.1039mE+02 0.E+00 00.103mE+02 00.703m+E+03	32 00.11524E+02 0.E+00 00.11524E+02 00.73395E+03
33 00.81971E+01 0.E+00 00.81971E+01 00.75382E+03	34 00.73946E+01 0.E+00 00.73946E+01 00.73483E+03
35 00.553596+01 0.6+00 00.553596+01 00.772316+03	36 00.605346+01 0.6+00 00.605346+01 00.754056+03
37 00.467285+01 0.E+00 00.46728E+01 00.79950E+03	38 00.432806.01 0.6.00 00.432806.01 00.795496.03
39 00.35044E+01 0.E+00 00.35048E+01 00.83167E+03	40 00.37459E+01 0.E+00 00.37459E+01 00.83721E+03

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THE ELASTIC ENEMGY IS 00.167480E+03

THE PLASTIC ENEMGY IS 00.794769E+02

THE TOTAL EXERGY IS 00.246696E+03FOH A LUAD OF 00.243707E+05

THIS IS INCPEMENT 4 - 2 OF 4

THE APPLIED LOAD IS 24370.7071THE INC. LUAD IS 279.8538
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SCALED STEP

STATE MAP STEP 4 - 3

3 3	3 3	3 2 1	1 1 1						
	——; · ; · ·	- 13 21	-ii;-i						
1 1	1 1	1 1	1 1						
0.31996290	0.00000000	0.01586090	0.0000000	TOTAL	DISPLACEMENTS 0.00000000	0.01208390	0.0000000	0.01104845	0.00000000
0.31026pHp	_0.00000000	0.00467110	-0.00000000	0.00917974	~~0.0000000 ~~~~	~~0.00da2723	0.00000000	0.00B5+3+0	~0.00000000
0.00834343	0.00000000	0.01996290	0.00031732	0.01625096	0.00020932	0.01353981		0.01216911	00010599
0.01105953 0.00452840	00014170 00015578	0.0102±14A 0.00431340	0001415d <sup></sup>	0,00963852	00014691 0.00054019	0.00917718		0.00879627	00015543 00000a78
0.01215469	00023277	0.01111275	00026015	0.01025127	00028133	0.00964949		0.00914723	00029868
0.00874356	00030633	0.00849833	00031289	0.00430040	00030671			•	
0.00179977	0.00000000	0.00134462	0.00000000	NCREMENTAL 0.00104059	*DISPLACEMENTS** 0.0000000	0.00089776	0.0000000	0.00082495	0.00000000
0.00076103	0.00000000	0.00071290	0.00000000	0.00007292	0.00000000	0.00064426		0.00005103	0.00000000
0.00000595	0.00000000	0.00179977	0.00010615	0.00139748	0.00007871	0.00105538	0.00002698	0.00092777	0.00000092
0.00082978	00000406	0.00076406	00000810	0.00071006	00000930	0.00067177		650÷9000•0	00001036
3.00061872	00001032 00000306	0.00060164	00000919	0.00179977	0.00017332 00001557	0.00140104		0.0011+013 0.00066817	0.00006142 00001868
	00001989	0.00061450	00002084	0.00059898	00001972	*************		•••••••	***************************************
				NCREMENTAL	FORCES	–			
299.9	-12.5 37.5		86.5	-0.0	-1.7	-0.0	-81.9	-0.0	-12.8 -5.6
-0.0	-38.0	640.0	00.0	-0.0	14.1	-0.0 -0.0	00.0	-0.0	-0.0
00.0	00.0	-0.0	-0.0	-0.0	00.0	+0.0	-0.0	-0.0	0.0
00.0	-6.0	00.0	00.0	210.7	-0.0	-0.0	-0.0	-0.0	-0.0
00.0	-0.0	00.0	-0.0	00.0	00.0	00.0	-0.0	00.0	00.0
				TOTAL	FORCES				
6081.1	117.0	-0.0	510.2	-0.0	-325-1	-0.0	-311.9	-0.0	40.6
-0.0	106.0	-0.0	63.5	=0.0	-0.0	-0.0	25.1	-0.0	-41.2
00.0	-240.7	13808.6	-0.0	-0.0	-0.U	-0.0	-0.0	-0.0	-0.0
-0.0	-0.0	00.0	00.0	5631.3	-0.0	-0.0	-0.0	-0.0	-0.0
00.0	-0.0	00.0	-0.0	00.0	-0.0	.00.0	-0.0	00.0	00.0
00.0	-0.0	00.0	00.0	NODAL OU.O	00.0 COORDINATES			<u> </u>	
1.019963	0.000000	1.215861	0.000000	1.413656	0.000000	1.612084	0.000000	1.8110#8	0.000000
2.010267	0.000000	2.209671	0.00000	2.409180	0.000000	2.608827	0.00000	2.803543	0.000000
3.008344	0.000000	1.019463	00.200317	1.219521	00.200209	1.413540	00.199990	1.612169	60.199893
2.608529	00.199359	2.010281	00.199858 00.199851	5.508034	00.199853	2.409177	00.199850	2.608790	(0.199845
1.612160	00.199344	1.011113	00.197651	2.010251	00.399719	2.209649	00.399713	2.409147	C0.399991 C0.399701
2.608794	00.399594	2.808498	00.399687	3.008301	00.399693				
SAMPLE PROB	JLEM 3 EXPA	ANSTON OF A THIC	K WALL TUBE				STEP	4 - 3 OF	4
				CTUESS ELS	MENT BATA		316		
				STRESS ELE	MENT DATA				
NEL INV	SA S	sr sz	SRZ	STRESS ELE	MENT DATA	YS SIGE		JZ	J3
NEL IRV	sa s	57 52		51 52	\$12		o s	JZ	J3
1 3-0.862	25E+04 0.4304	+E+04-0.1749E+03	3 0.E+00 -	51 52 0.1749E+03-0.86	512 525E+04 0.4225E	+0+0.00 0.113	0 S 17E+05-0.1499E+04	J2 0.4311E+08	J3 -0.5476£+11
1 3-0.866	25E+04 0.4304	+E+04-0.1749E+03 9E+04-0.9149E+03	0.2821E+03-	51 52 0.1749E+03-0.86 0.9050E+03-0.89	\$1Z 525E+04 0.4225E 69E+04 0.4032E	+0+0.00 0.113 +040.04 0.111	0 5 17E+05-0.1499E+04 6E+05-0.2035E+04	JZ 0.4311E+08 0.4144E+08	J3 -0.54765+11 -0.45015+11
1 3-0.866 2 3-0.899 3 3-0.699	25E+04 0.4304 54E+04 0.3769 52E+04 0.561	+E+04-0.1749E+03 9E+04-0.9149E+03 7E+04-0.1727E+03	3 0.E+00 - 3 0.2821E+03- 3-0.1755E+03-	51 52 0.1749E+03-0.86 0.9050E+03-0.69 0.1677E+03-0.64	512 525E+04 0.4226E 69E+04 0.4032E 67E+04 0.3150E	+0+0.00 0.113 +040.04 0.111 +040.03 0.104	0 5 17E+05-0.1499E+04 6E+05-0.2035E+04 7E+05-0.3392E+03	JZ 0.4311E+08 0.4144E+08 0.3656E+08	J3 -0.54765+11 -0.45015+11 -0.50745+10
1 3-0.866 2 3-0.895 3 3-0.646 4 3-0.703 5 3-0.495	26E+04 0.4304 59E+04 0.3769 62E+04 0.5616 92E+04 0.5147 67E+04 0.6796	6E+04-0.1749E+03 9E+04-0.9149E+03 7E+04-0.1727E+03 7E+04-0.3539E+03	3 0.E+00 = - 3 0.2821E+03= 3-0.1755E+03= 3 0.1932E+03	51 52 0.1749E+03-0.86 0.9050E+03-0.69 0.1677E+03-0.70 0.3669E+03-0.70	512 526E+04 0.4226E 69E+04 0.4032E 67E+04 0.3150E 97E+04 0.3736E 65E+04 0.2766E	+0+0.00 0.113 +0+0.04 0.111 +0+0.03 0.104 +0+0.03 0.106 +0+0.04 0.101	0 17E+05-0.1+99E+0+ 6E+05-0.2035E+0+ 7E+05-0.339ZE+03 9E+05-0.5270EF03 9E+05-0.799UE+03	0.4311E+08 0.4144E+08 0.3650E+08 0.3805E+08 0.3855E+08	-0.54765+11 -0.45016+11 -0.45016+11 -0.40146+11 0.43146+11 0.43154+10
1 3-0.866 2 3-0.899 3 3-0.696 4 3-0.700 5 3-0.495 6 2-0.45	26E+04 0.4304 59E+04 0.3769 62E+04 0.561 92E+04 0.5147 67E+04 0.6796 37E+04 0.6749	0-E+04-0.1749E+03 9-E+04-0.9149E+03 7-E+04-0.1727E+03 7-E+04-0.1727E+03 7-E+04-0.5587E+03 8-E+04-0.3662E+02	3 0.E+00 = 3 0.2821E+03= 3 0.2821E+03= 3 0.193E+03= 3 0.193E+03 3 0.2047E+03 2 0.2239E+02	51 52 0.1749E+03-0.86 0.1677E+03-0.66 0.1677E+03-0.70 0.3669E+03-0.70 0.3661E+03-0.45	\$12 526E+04 0.4226E 669E+04 0.4032E 67E+04 0.3150E 97E+04 0.3733E 65E+04 0.2766E 37E+04 0.2438E	+0+0.00 0.113 +040.04 0.111 +040.03 0.104 +040.03 0.104 +040.04 0.101 +040.00 0.100	0 5 17E+05-0.1499E+04 6E+05-0.2035E+04 7E+05-0.3392E+03 9E+05-0.5270E+03 8E+05-0.6502E+03 8E+05-0.6502E+03	0.4311E+08 0.4144E+08 0.3650E+08 0.3805E+08 0.3455+04 0.345E+00	-0.54765+11 -0.5015+11' -0.50745+10 -0.30195+11 0.53135+10 0.50465+11
1 3-0.864 2 3-0.895 3 3-0.646 4 3-0.705 5 3-0.495 6 2-0.45 7 1-0.33	25E+04 0.4304 5-E+04 0.3765 6-E+04 0.5616 5-E+04 0.5147 6-7E+04 0.6796 37E+04 0.6746	%E+04-0.1749E+03 %E+04-0.9149E+03 7E+04-0.1727E+03 7E+04-0.1727E+03 7E+04-0.3539E+03 8E+04-0.4034E+02 8E+04-0.4034E+02	3 0.E+00 3 0.2821E+03= 3-0.1755E+03= 3-0.1932E+03= 3-0.2047E+03= 2-0.239E+02= 2-0.534E+02=	51 52 0.1749E+03-0.86 0.9050E+03-0.60 0.1677E+03-0.60 0.3669E+03-0.40 0.3872E+02-0.46	\$12 \$26E * 0 * 0.4226E \$69E * 0 * 0.4032E \$67E * 0 * 0.3150E \$97E * 0 * 0.3733E \$65E * 0 * 0.2766E \$37E * 0 * 0.2438E \$35E * 0 * 0.4648E	+0+0.00 0.113 +040.04 0.111 +040.03 0.104 +040.03 0.106 +0+0.04 0.101 +040.00 0.100 +040.02 0.778	0 5  7E+05-0.1+99E+0+6E+05-0.2035E+04 7E+05-0.3392E+03 9E+05-0.5270E+03 9E+05-0.7520E+03 9E+05-0.502E+03 2E+04-0.7203E+03	0.4311E+08 0.4414E+08 0.3650E+08 0.3805E+08 0.3805E+08 0.388=E+08 0.2015E+08	J3  -0.5476E+11 -0.5012+11 -0.5012+11 -0.5013514 0.50132+10 0.5046E+11 0.15042+11
1 3-0.864 2 3-0.894 3 3-0.644 4 3-0.704 5 3-0.494 7 1-0.333 8 1-0.375	25E+04 0.4304 5+E+04 0.3765 52E+04 0.5616 57E+04 0.5147 57E+04 0.6746 37E+04 0.6746 34E+04 0.555	%E.04-0.1749E.03 9E.04-0.9149E.03 7E.04-0.1727E.03 7E.04-0.3539E.03 9E.04-0.3582E.03 9E.04-0.4038E.02	3 0.E+00 3 0.2821E+03= 3-0.1755E+03= 3-0.1932E+03 3-0.2047E+03 2-0.2239E+02 2-0.534E+02= 1 0.9863E+02	51 52 0.1749E+03-0.86 0.9050E+03-0.69 0.1677E+03-0.70 0.3669E+03-0.70 0.5661E+03-0.49 0.3872E+02-0.49 0.1369E+03-0.43 0.1369E+03-0.43	512 0266-04 0.42266 0696-04 0.40326 0676-04 0.31506 0576-04 0.27666 0376-04 0.27666 0376-04 0.24386 0376-04 0.14356	+0+0.00 0.113 +040.04 0.111 +040.03 0.104 +040.03 0.106 +0+0.04 0.101 +040.00 0.100 +040.02 0.778 +040.03 0.845	0 5 17E+05-0.1499E+04 6E+05-0.2035E+04 7E+05-0.3392E+03 9E+05-0.5270E+03 8E+05-0.6502E+03 8E+05-0.6502E+03	0.4311E+08 0.4144E+08 0.3650E+08 0.385E+08 0.385E+08 0.338E+00 0.2015E+00	-0.54765+11 -0.5012+11 -0.5012+11 -0.503192+11 0.53192+11 0.5036465+11 0.15305+11
1 3-0.86.6 2 3-0.89.3 3 3-0.64.4 4 3-0.70.5 5 3-0.49.6 6 2-0.45.7 1-0.33.8 1-0.37.9 1-0.26.10 1-0.26.10	26E+04 0.4304 5-E-04 0.561 5-E-04 0.561 5-E-04 0.5167 5-E-04 0.6764 3-E-04 0.6764 3-E-04 0.555 31E-04 0.4962 1-E-04 0.4962	*E+04-0.1749E+03 *E+04-0.9149E+03 *E+04-0.1727E+03 *E+04-0.3539E+03 *E+04-0.3559EE+03 *E+04-0.3662E+02 *E+04-0.4634E+03 *E+04-0.4634E+03 *E+04-0.6454E+03 *E+04-0.6454E+03	3 0.E+00 3 0.Z82IE-03- -0.175E-03- 3 0.1932E-03- 3 0.1932E-03- -0.239E-02- -0.5534E-02- 1 0.9843E-02- -0.5540E-02- 0.2747E-02-	51 52 0.1749E+03-0.86 0.9050E+03-0.86 0.1677E+03-0.66 0.3669E+03-0.70 0.3661E+03-0.86 0.3943F+02-0.86 0.3943F+02-0.37 0.1369E+03-0.86	\$12 \$266.04 0.42266 \$696.04 0.40326 \$676.04 0.31506 \$976.04 0.37336 \$656.04 0.27666 \$376.04 0.24366 \$356.04 0.10356 \$366.04 0.10356 \$176.04 0.1276	+0+0.00 0.113 +0+0.04 0.114 +0+0.03 0.104 +0+0.03 0.106 +0+0.04 0.101 +0+0.00 0.100 +0+0.03 0.405 +0+0.03 0.405 +0+0.03 0.405 +0+0.01 0.652	0 5  17E+05-0.1+99E+0+6E+05-0.2035E-04  7E+05-0.3392E+03  9E+05-0.7990E+03  8E+05-0.502E+03  2E+04-0.7263E+03  5E+04-0.736E+03  5E+04-0.736E+03	J2 0.4311E+08 0.4144E+08 0.3654E+08 0.3852E+08 0.3455E+08 0.2012E+08 0.2012E+08 0.1453E+08 0.1453E+08	J3  -0.54765+11 -0.45012+11 -0.45012+11 -0.50745+10 -0.5132+10 -0.5145+11 -0.1502+11 -0.1502+11 -0.1506+11 -0.1506+1 -0.1045+10 -0.5065+10
1 3-0.86/ 2 3-0.89/ 3 3-0.69/ 4 3-0.70/ 5 3-0.49/ 6 2-0.49/ 7 1-0.33/ 8 1-0.37/ 9 1-0.26/ 10 1-0.25/ 11 1-0.17/	26E+04 0.4304 55E+04 0.3766 55E+04 0.516 57E+04 0.516 57E+04 0.6796 37E+04 0.6796 37E+04 0.4993 15E+04 0.4993 17E+04 0.4993 17E+04 0.4045	0.000000000000000000000000000000000000	3 0.E+00 3 0.E+00 3-0.175E+03- 3 0.193E+03 1-0.2239E+02 1-0.5534E+02- 1-0.5540E+02- 1-0.5540E+02- 1-0.5540E+02- 1-0.6241E+02- 1-0.6241E+02-	51 52 0.1749E+03-0.86 0.1057E+03-0.69 0.1057E+03-0.70 0.3669E+03-0.70 0.3661E+03-0.46 0.3972E+02-0.46 0.1369E+01-0.30 0.1369E+01-0.30 0.4034E+01-0.26	\$12 \$26E+04 0.4226E \$69E+04 0.4032E \$67E+04 0.3150E \$97E+04 0.3750E \$37E+04 0.2766E \$37E+04 0.2438E \$37E+04 0.1435E \$16E+04 0.1312E \$16E+04 0.127E \$80E+04 0.6668E	+0+0.00 0.113 +040.04 0.111 +040.03 0.104 +040.03 0.106 +040.04 0.101 +040.02 0.100 +040.02 0.845 +040.03 0.845 +040.03 0.845 +040.03 0.845 +040.03 0.845	0 5   7E+05-0.1+99E+04  6E+05-0.2035E+04  7E+05-0.3392E+03  9E+05-0.5270E+03  8E+05-0.502E+03  8E+05-0.502E+03  8E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03	0.4311E+08 0.4314E+08 0.4650E+08 0.3650E+08 0.34550+08 0.338+c+08 0.201EE+08 0.230EE+08 0.1332E+08 0.1332E+08	-0.54765+11 -0.5012+11 -0.5012+11 -0.5012+11 -0.5012+11 0.5012+11 0.1502+11 0.1502+11 0.1502+11 0.1502+11 0.1505+11 0.1505+11 0.1505+11
1 3-0.866 2 3-0.896 3 3-0.696 4 3-0.703 5 3-0.496 6 2-0.493 7 1-0.333 8 1-0.377 9 1-0.261 10 1-0.261 11 1-0.177 12 1-0.197	26E+04 0.4304 55F+04 0.376 55F+04 0.561 67E+04 0.518 67E+04 0.676 34E+04 0.555 11E+04 0.499 77E+04 0.466 78E+04 0.467	6E+04-0.1749E+03 4E+04-0.9149E+03 7E+04-0.1777E+03 7E+04-0.1777E+03 7E+04-0.3539E+03 7E+04-0.368E+03 3E+04-0.403ME+02 3E+04-0.403ME+03 3E+04-0.6051E+01 3E+04-0.6051E+01 3E+04-0.6051E+02 3E+04-0.6054E+03	3 0.E+00 3 0.E2EEE3 3 0.E2EE63 3 0.1932E-03 3 0.1932E-03 3 0.1932E-03 4 0.294E-02-1 4 0.9943E-02 6 0.2747E-02-1 6 0.1744E-02-1 0.1744E-02-1	51 52 0.1749E+03-0.86 0.9050E+03-0.60 0.1677E+03-0.46 0.3669E+03-0.46 0.3872E+02-0.46 0.3943F+02-0.33 0.1369E+03-0.37 0.6394E+01-0.26 0.6393E+01-0.27 0.6393E+01-0.17	\$12 \$26E+04 0.4226E \$69E+04 0.4032E \$67E+04 0.3150E \$97E+04 0.3733E \$65E+04 0.2766E \$37E+04 0.1648E \$34E+04 0.193E \$16E+04 0.1312E \$17E+04 0.1227E \$34E+04 0.4668E \$34E+04 0.4668E	+0+0.00 0.113 +0+0.04 3.111 +0+0.03 0.104 +0+0.03 0.106 +0+0.04 0.10 +0+0.02 0.778 +0+0.03 0.445 +0+0.01 0.632 +0+0.01 0.632 +030.04 0.15	0 5  7E+05-0.1+99E+0+6E+05-0.2035E+0+7E+05-0.3392E+03 9E+05-0.5270E+03 9E+05-0.592E+03 9E+05-0.592E+03 5E+04-0.7ca5E+03 5E+04-0.7ca5E+03 5E+04-0.7ca5E+03 5E+04-0.7ca5E+03 5E+04-0.7ca5E+03	JZ  0.4311E+08 0.4144E+08 0.45542+08 0.3552408 0.338+c+08 0.2012+08 0.2012+08 0.14532+08 0.13322+08 0.19322-08 0.19322-08	J3  -0.3476E+11 -0.45012+11 -0.45012+11 -0.30174E+10 -0.3132+10 -0.3132+10 -0.5046E+11 -0.1530E+11 -0.1530E+11 -0.1530E+11 -0.1550E+11 -0.764E+10 -7445E+10
1 3-0.866 2 3-0.894 3 3-0.604 4 3-0.706 5 3-0.494 6 2-0.495 7 1-0.337 9 1-0.267 10 1-0.257 11 1-0.177	26E+04 0.4304 525-04 0.561 575-04 0.516 575-04 0.516 575-04 0.576 375-04 0.576 375-04 0.576 315-04 0.576 115-04 0.496 745-04 0.497 745-04 0.497 745-04 0.497	6E • 04 - 0 . 1749E • 03 6E • 04 - 0 . 9149E • 03 7E • 04 - 0 . 11727E • 03 7E • 04 - 0 . 13639E • 03 7E • 04 - 0 . 3639E • 03 7E • 04 - 0 . 3662E • 02 7E • 04 - 0 . 0362E • 02 7E • 04 - 0 . 0362E • 02 7E • 04 - 0 . 0362E • 03 7E • 04 - 0 . 0473E • 03	3 0.E+00 3 0.E+00 3 0.175E+03 3 0.193E+03 3 0.193E+03 9 0.2239E+02 9 0.5546E+02 9 0.5540E+02 9 0.724TE+02 0.1794E+02 0.1794E+02	51 52 0.1749E+03-0.86 0.1077E+03-0.69 0.1677E+03-0.70 0.3669E+03-0.70 0.3661E+03-0.40 0.3943F+02-0.30 0.6938E+01-0.25 0.6938E+02-0.25	512 526E+04 0.4226E 69E+04 0.4032E 69E+04 0.3150E 69E+04 0.2766E 137E+04 0.2766E 137E+04 0.123E 16E+04 0.1935E 16E+04 0.123E 16E+04 0.1266E 18E+04 0.4666E 18E+04 0.4669E	**************************************	0 5   7E+05-0.1+99E+04  6E+05-0.2035E+04  7E+05-0.3392E+03  9E+05-0.5270E+03  8E+05-0.502E+03  8E+05-0.502E+03  8E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03  4E+04-0.7046E+03	0.4311E+08 0.4144E+08 0.4650E+08 0.3855E+08 0.385E+08 0.385E+08 0.201EE+06 0.1332E+08 0.1932E+07 0.101E+07 0.101E+07	J3  -0.5012-11 -0.5012-11 -0.5012-11 -0.3192-11 0.3132-10 0.204-65-11 0.15032-11 0.1532-11 0.1532-11 0.1532-11 0.1532-11 0.1532-11 0.1532-11 0.1542-10 0.5057E-10 0.5057E-10 0.505E-10
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### TABLE VIII. - Continued. SAMPLE PROBLEM (4) - OUTPUT

SAMPLE PROBLEM & EXPANSION OF A THICK WALL TUBE

STRAIN ELEMENT DATA

STEP 4 - 3 OF

NEL	RC	ΣC	ER	ET	EZ	ERZ	LR	LZ	LT	L1	rs	TL	TS	TR	EPEQ	NEL
1	1.08526	00.06677	-0.02116	0.01649	0.00158	0.00000	0.9795	1.0016	1.0174	1-0016	.0.9795***	0.00	-0.00	00-00	0101303"	<sub>1</sub> .
ē	1.15069	00.13351	-0.01404	0.01497	0.00104	0.00074	0.9814	1.0010	1.0153	1.0010	0.9814	0.00	00.00		0.01061	ż
. 3	1.34769		-0.01121			-0.00030						3.11	-0.00		0.00370	3-
	"1.47976"		-0.013d3 -0.00796		-0.00005	0.00045 0.00030	0.9921	1,0000	1.0089	1.0000	0.7864	3.10-	-0.00		0.00005	
6	1.54543	00.13384	-0.00647	0.00415	-0.00054	-0.00003	0.9931	0,4995	1.0082	0.9995	0.9931	3.14	-0.00		0.00000	6
7	1.74474		-0.00501			-0.00007						3.12	-0.00		0.00000	7
8	1.67844		-0.00559 -0.00413	0.00699	-0.00054	-0.00013	0.9945	0.9995	1.0071	0.9995	0.9945	3.12	-0.00	00.00	0.00000	b.
10	1.94367		-0.00391			0.00004						0.00	00.00		0.00000	10
11	_5.1+3/14_		-0.00244	0.00459	-0.00074	-0.00008	0.4470	0,4493	1.0046	0.4493	0.9970	3.11	-0.00	00.00	0.00000	-11-
13	2.07673		-0.00323			-0.0000A						_0.00	00.00		0.00000	15
14	2.34267		-0.00231			-0.00001						3.09	-0.00		0.0000	13. 14
15	2.54227	00.06661	~0.00177	0.00351	-0.00078	-0.00008	0.9982	0.9992	1.0035	0.9992	0.9982	3.06	-0.00	00.00	0.00000	15
16	2.47572	_00.13323	-0.00191	0.00365	-0.00075	-0.00002	0.9481	0,9992	1.0037	0.9943	0.9981	3.12	-0.00	00.00	0.00000	10_
17	2.675.19		-0.00142 -0.00134	0.00325	-0.00078 -0.00078	-0.00008	0.9986	0.9992	1.0032	0.9992	0.9986	3.02	-0.00		0.00000 0.00000	17 15
19	2.9-173	00.06662	-0.00130	0.00245	-0.00075	-0.00008	0.9990	0.9993	1.0029	0.9993	0.9990	2.87	-0.00		0.00000	19"
20	2,87513	00.13323	-0.0010a	0.00244	-0.00078	-0.00002	0.9989	0.9992	1.0030	0.9992	0.9989	. 3.08	-0.00	00.00	0.00000	50
25	1.05532	00.33377	~0.02022 ~0.01909	0.01704	0.00111	-0.00025 -0.00083	0.9804	1.0011	1.0175	1.0011	0.9804	3.13 3.10	-0.00		0.01231	. 22 . 22
23	1.34750		-0.01128	0.01068	_0.00001	-0.00040	0.9590	1.0000	1.0109	1.0000	0.9890	- 3.11-	-0.00	00:00.	0.00379	-55-
24	1.28194	88005.00	-0.01364	0.01185	0.00116	-0.00110 0.00019 -0.00027	0.9864	1.0012	1.0121	1.0012	0.9864	3.07	-0.00	00.00	\$1000.0	24
25	1.47784		-0.00d46 -0.00642	0.00886	0.00001	0.00018	0.9916	1.0000	1.0090	1.0000	0.9916	0.00	00.00	00.00	0.00122	25
- 26 - 27 · · ·	1.74478	00.20055	-0.00524	0.00654	-0.00060	0.00007	0.9948	0.9994	1.0066	0.9994	U-9948 -	-3.10 0.00-	-0.00	00.00	0.00000	. 26 - 27
28	1.67846		-0.00554	0.00700	-0.00063	-0.00011	0.9945	0.9994	10071	0.9994	0.9944	3.12	-0.00	00.00	0.00000	28
29	1.87747		-0.00434	0.00574	-0.00060	0.00008	0.9957	0.9994	1.0058	0.9994	0.9957	0.00	00.00		0.00000	29
-31	2.14313		-0.00303	0.00540	-0.00070	-0.0000H	0.9961	0.9993	1.0054	0.4993	0.9961	3.12	-0.00		0.00000	30
35	2.07672		-0.00323	0.00483	-0.00070	-0.00009	0.9968	0.9993	1.0049	0.9993	0.9968	3.11	~0.00	00.00	0.60000	35
33	2.27615	u0.3330+	-0.00252	0.00416	-0.00070	-0.00000	0.9975	0.9993	1.0042	0.9993	0.9975	3.14	-0.00	00.00	0.00000	33
34	2.34265		-0.00231	0.00397	-0.00074	-0.00008	0.9977	0.9993	1.0040	0.9993	0.9977	3.09	-0.00		0.00000	34
36	2.54225		-0.00177			-0.00003 -0.00009						3.12	-0.00		0.00000	35
···37	2.67536	00.33309	-0.00148	0.00325	-0.00076	-0.00002	0.9985	0.9992	1.0033	0.9992	0.9985	3.11	-0.00	00.00	0.00000	37
38	2.74174		-0.00134			-0.00008						3.00	-0.00		0.00000	34
39 40	2.94170 2.87511		-0.00099		-0.00079	-0.00002	0.9990	0.9992	1.0029	0.9992	0.9990	3.06 2.95	-0.00		0.00000	39 40
1 3 5 7	00.57392E 00.47562E 00.45339E 00.26561E	+02 00.13 +02 00.37 +02 00.92 +02 0.E+	800E+03 0  742E+02 0  245E+01"0	TOT EN. DE 10.19539E+ 10.85303E+ 10.54613E+ 10.26561E+ 10.19797E+	)3 -0.149 )2 -0.339 )2"00.799	91E+04 20E+03 01E+03		2 00 4 00 6 00	.56461E .49679E .44243E	.02 00. .02 00.	E+00	00.168 00.111 00.442 00.313	03E+03 + 98E+03 + 93E+02 ( 98E+02 (	-0.20350  -0.52704  00.65013  00.70865	-04 -03 -03 -03	
. 9	00.197475	+02 0.E+				57E+03		10 00	.17605E	•02 0.	E+00 E+00			00.694021 00.770021		
	00.12043E			10.12045E+0		62E+03		- 12 00 14 00	.43311E	·01 · 0.	E+00			)0.77794l		·
15	00.64810E	+01 0.E+	00 0	0.6481UE+	1 00.817			16 00	.70700E	·01 0.	E+00	00.707	30E+01 (	00.839548	د0÷.	
	00.54452E	*01 0.E+	00 0	10.544626+1	11 00 840	89F+07					E+00	00.504	59E+01 (	00.861608	:+03	
21	00.41040E	+01 U.E+	034F+63 D	0.41080E+	13 -0-109	205+03 59F+04		50 00	.430/46 .56133F	.02 00.	11510E+03 11510E+03	00.430	23F+03 -	)0.96424( -0.14417:	.+U3 .+U4	***
23	00.474445	+02 00.34	640E+05 0	10.86144E+	2 -0.227	32E+03		24 00	.49740E	.02 00.	63179E+02	00.112	₹7E+63 •	14EF8E.0-	2+03	
				0.57736E+				26 00	.44410E	•02 0.	£+00			0.555316	.+03	
	00.27560E 30.20352E		00	10.27560E+0	12 00.619 12 60.721	51E+U3 80F+03		28 00 30 00	.31427E	.02 0.	E+00 E+00			)0.722818 )0.699468		
31	00.12073€	+02 U.E+	00 0	0.12073E+	2 00.743	66E+03		32 00	.13506E	•02 0.	E+00	00.135	16E+02 (	0.752198	.+03	
33	00.958798	+01 0.E+	00 0	0.95879E+	11 00.799	05E+03		34 00	.86385E	·01 0.	E+00	00.8638	5E÷01 (	0.77776	د 0 •	
	00.645268			0.645262+1					.70609E		E+00 E+00			)0.841586 )0.841586		
	00.54459E			10.54409E+1					.43545E					0.899408		
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THE E	LASTIC EN	ERGY IS		00.145552												
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				TC TC T. AL	DEMENT '-		ΛE .	—								
THE A	IPPLIED LO	AD IS	25571.2	346 THE IN	. LUAD I	S	150.527	5								

SCALED STEP

STATE MAP	STEP	4 -		•										
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3 3	3	3	3	3	1	ı	ı	ı						
1 1	ı	1	1	ı	1	ı	ı	1						
				:					TOTAL	DISPLACEMENTS				
.02000000	0.000		_		88884		00000		0.01367886	0.00000000	0.01210218	0.00000000	0.01110511	0.00000000
.01028215	0.000				968541		00000		0.00919324	0.0000000	0.00684016	0.00000000	0.00855586	0.00000000
.03835604		00000			000000		00314		0.01624015	0.00051045	0.01356226	00000901	0.01213110	00010081
.01107615		14131			19967		00141		0.00965277	00014710	0.00919065	00015021	0.00880910	00015564
.00454130		15599			132545		00144		0.02000000	0.00054372	0.01606704	0.00044629	0.01385515	00000726
.01217847		73245			112967		130590		0.01020001	00028164	0.00966378	00028756	0.00916064	00029405
.00440634	000	30672		0.00	H51064	0	100313		0.00831279 REMENTAL	00030710 DISPLACEMENTS				
	3 664						00000						0.000014	
.00003710		00000			002794 001431		00000		0.00002268		85910000.0 Se510000.0	0.00000000	0.00001666 0.00001247	0.00000000
.00001215		00000			001431		100002		0.00001350		0.00001245	0.00000000	0.00001247	0.00000000
.00001213		00001			003713		00000		0.00007419	00000019	0.00002245	000000019	0.00001284	000000018
.00001240	000				001502		00000		0.00001425	0.00000353	0.00001348	0.00000019	0.00001284	0.000000151
.00001240		00020			001693		00000		0.00003710	000000333	0.00001429	00000033	"-0.00002364 "-0.00001341	~.00000037
.00001281		00039			001231		00000		0.00001234	00000039	0.00001424	000000033	0.00001341	000000037
.00001261	000	00039		0.000	001231	0			REMENTAL	FORCES			- •	
5.3		-0.1			-0.0		00	. 6	00.0	00.2	-0.0	-0.2	-0.0	-0.6
-0.0		00.2			-0.0		0.0	. 3	-0.0	00.3	-0.0	00.1	-0.0	-0.1
00.0		-0.8			10.8		00	. 0	-0.0	-0.0	-0.0	00.0	-0.0	-0.0
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00.0		-0.0			00.0		0.0	.0	00.0	00.0				
			•						TOTAL	FORCES				
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00.0		106.3			3819.7						-0.0		00.0	
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-0.0		00.0			00.0			.0	5634.9	~0.0	-0.0	-0.0 -0.0	-0.0	~0.0
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00.0		-0.0			00.0			.0	00.0	00.0	00.0	-0.0	00.0	00.0
								•	- NODAL	COORDINATES -				
1.020000	0.0	00000		1.2	215889	Λ	.0000	0.0	1.413679	0.000000	1.612102	0.000000	1.911105	0.000000
2.010232		00000			209685		.0000		· 2.409193	0.00000	2.608840	. 0.000000	Z.808556	0.000000
3.008356		00000			020000		.2003		1.216280	00.200211	1.413562	00.199991	1.012108	00.199893
1.811076		99359	*		010297		1998		2.209653	00.199853	2.409191	00.199850	- 2.608809	00.199844
2.808541		99544			008325		1998		1.020000	00.400544	1.216067	00.400446	1.413855	00.399993
1.612178		99769"			311134		3997		2.010267	00.399718	2.209664	00.399712	2.409161	00.399701
2.608805		99693			308511		. 3996		3.008313	00.399693	2.22.20			
AMPLE PHO			120						STRESS EL			STEP	4 OF	4

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EL	RC	zc	ER	ET	EZ	ERZ	LR	LZ	LT	LI	FS	TL	TS	TR	EPEQ	NE
. <sub>1</sub> -	1.08530	00.06677	-0.02121	0.01702	0.00159	0.00000	0.9794	1.0016	1.0175	1.0016	0.9794	0.00	-0.00	00.00	0.01307	1
5	1.15072	00.13351	-0.01913			0.00074						0.00	00.00		0.01065	2
3 -	1.34771		-0.01124			-0.00030						3.11	-0.00		0.00372	3
<del>- 5 -</del> .	_1.2d1+1 _1.47978	00.13340	-0.01387 -0.00798	_0.00885. _0.0118%	-0.00005 -0.00105	0.00045	0.9864	1.0011	1.0120	1.0000	0.9864 0.9821"	3.16-	00.00		0.00063	
6	1.54575	00.13329	-0.00094	0.00613	-0.00003	-0.00003	0.9931	0.4945	1.0082	1.9995	0.9931	3.14	-0.00		0.00002	-
<sup>-</sup> 7	1.74476	20000.00	-0.00502			-0.00007						3.12	-0.00		0.00000	
8	1.67846	00.13325	-0.00560			-0.00013						0.00 3.12	-0.00		0.00000	
10	1.877-9	30.13324	-0.00414			0.00004						0.00	00.00		0.30000	
ii—	2.14321	5000 Johos	-0.00300	0.00400	-0.00074	-0.00000	0.7770	0.9943	1.0046	0.4943	0.9970	3.ii-	-0.00		-0.30000	
12	2.07674		-0.00324	0.00484	-0.00071	0.00002	0.9968	0.9993	1.0049	0.9993	0.9968	0.00	00.00		0.00000	
13 14	2.2761H 2.34258	00.00062	-0.00247	0.00417	-0.00074	-0.00008	0.9975	0.9993	1.0042	0.9993	0.9975	3.09	-0.00		0.0000	
15	2.54248	00.06661	-0.00177			-0.00008						3.06	-0.00		0.00000	15
16	2.475/3	00.13323	-0.00191	0.00355	-0.00075	-0.00002	0.9981	0.9992	1.0037	0.9992	0.9981	3.12	-0.00	00.00	0.0000	10
17	2.67540		-0.00142			-0.00008 -0.00004						3.02	-0.00		0.0000	
18	.2.74197 .2.94175		-0.00134	0.00314	-0.00078	-0.00008	0.9990	0.9993	1.0029	0.9993	0.9990	3.08 2.87	0.00		0.0000	10
ŽÓ	2.87514	00.13323	-0.0010a	0.00294	-0.00078	-0.00002	0.4989	0.9992	1.0030	0.9992	0.9989	08.د	-0.00	00.00	0.0000	20
21	1.08536	00.33377	-0.07026			-0.00025						3.13	-0.00	00.00	0.01234	
22 23	1.15078	00.25549	-0.01913 -0.01124	0.01505	0.00117	-0.00083	0.9814	1.0002	1.0154	1.0012	0.9814	3.10	-0.00		0.01070	
24	1.28197	30.26688	-0.01387		0.00117	-0.00110	0.9864	1.0012	1.0121	1.0013	0.9863	3.07	-0.00		0.10615	
25	1.47957	00.33325	-0.00849	0.00888	0.00001	0.00018	0.9916	1.0000	1.0090	1.0000	0.9916	0.00	00.00	00.00	0.00124	25
26 27	1.54596	00.26655	-0.00529	0.00614	L0000.0-	0.00027	0.9931	0.9994	1.0082	1.9994	0.9931	3.10 0.00	-0.00		0.0000	
2a	1.74479	00.35312	-0.00560	0.00701	-0.00063	-0.00011	0.9944	0.9994	1.0071	0.9994	0.9944	3,12	-0.00		0.00000	2
29	1.57749	00.33311	-0.00434	0.00575	-0.00060	0.00008	0.9957	0.9994	1.005h	0.4994	0.9957	0.00	00.00	00.00	0.00000	54
30	1.94356	00.25648	-0.00392		-0.00070	-0.00008	0.9961	0.9993	1.0055	0.9993	0.9961	3,12_	-0.60		0.0000	30
31 32	~2.14319~ 2.07674		-0.00303			-0.00001						3.11	00.00 0.00÷		0.0000	31 32
33	~2.27616"	"00.33369	-0.00253			-0.00000						3.14	-0.00	00.00	0.0000	- 33
34	2.34257	00.26647	-0.00232			-0.0000B						3.09	-0.00		0.00000	34
35**** 36	2.54226	00.33398	-0.00178 -0.00191	0.00350	-0.00076	-0.00003	0.9982	0.9992	1.0035	0.9992	0.9982	3.12	-0.00	00.00	00000	35 36
37 "	2.67538	00.233307	-0.00145			-0.00002						3,11	-0.00	00.00	0.00000	37
38	2.741+5	00.26645	-0.00134	0.00314	-0.00079	-0.00008	0.9987	0.9992	1.0032	0.9992	0.9987	3.00	-0.00	00.00	0.0000	36
39 °	2.94172		-0.00099			-0.00002						3.06 2.95	-0.00		0.0000	39 40
	2.87513	00.20040	-0100108	0.00274	-0.00017	-0.00000	0.7202	0.7772	1.0050	007772	V.,,,,,,	2.,,3	-0.00		***************************************	
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23	00.47473E	·02 00.38	144E+02 00	.8542ZE+0	2 -0.2313	32E+03		24 00.	49820E+	02 00.6	3504E+02	00.113	32E+03	-0.393586	+03	
25	00.45410E	+02 00.129	553E+02 00	.57463E+0	2 00.4588	116+03		26 00.	,444216+	05 00.1	1020F+00	00.4459	45-15	00.000406	+03	•
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33	00.961715	+01 P.E+0	00 00	.46171E+0	1 00.799	57E+03		34 00	86645E+	01 U.E	+00	00.8064	5E+31	00.783666	د0+.	
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### Lewis Research Center,

TAPE RESTART GENERATION ... STEP 4 - ""1"OF 4

National Aeronautics and Space Administration, Cleveland, Ohio, November 19, 1973, 501-21.

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